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Jones



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Standard Steel Construction

A MANUAL FOR
Architects, Engineers and Contractors

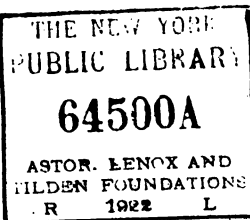
RELATING TO THE
USE OF

Structural Steel

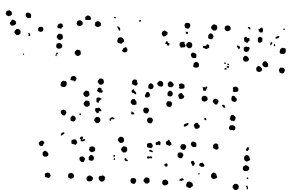
SEVENTH EDITION
1916



MANUFACTURED BY
Jones & Laughlin Steel Company
AMERICAN IRON AND STEEL WORKS
Pittsburgh



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PRICE \$1.50

Preface

Seventh Edition

In order that Standard Steel Construction may present the latest development in the manufacture of steel shapes and their use in such constructional work as buildings, bridges, cars, ships and barges, the text has been completely rewritten for this edition.

The diagrams and tables include only the sections best suited for these types of steel construction. A complete list of all the sections that we roll, with diagrams and weight tables, is shown in our Shape Book.

Much new data in the way of general information useful to architects, engineers and contractors has been added.

In determining the arrangement and classification of data the natural sequence has been followed as nearly as practicable without losing sight of convenience in locating the subject sought. For this reason the several specifications for material and fabrication are placed at the end of the book.

Offices

General Offices

Pittsburgh

Branch Office and Warehouse

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St. Louis

Pierce Building

Plants

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South Side Works

Soho Furnace and Works

Keystone Works

Aliquippa Works

J & L Products

Billets Blooms Slabs Skelp
Sheet Bars

Beams Channels Angles
Tees Zees Plates
Sheet Piling

Rounds Squares Flats Hexagons
Ovals Hoops Bands

Special Shapes
Agricultural Shapes
Tie Plates

Bars for Concrete Reinforcement
Light Rails and Connections
Steel Mine Ties

STRUCTURAL WORK

Columns Girders Trusses
Plate Work
Steel Barges

J & L Products

Wire Wire Nails Wire Products

Tin Plate Black Sheets
(Tin Mill Sizes)

Railroad Spikes Rivets Boat Spikes

Chain

Power Transmission Machinery

COLD ROLLED

Shafting Axles Shapes
Finger Bars

COLD DRAWN

Hexagons Flats
Squares Rounds

FORGINGS

Suggestions in Reference to Ordering Material

In the Standard specifications of the American Society for Testing Materials will be noted what are termed the permissible variations in the rolling of plates, shapes and bars, and provision should be made in the design to care for such variations. A design which does not permit of this variation is frequently the cause of serious difficulties. Ample clearances tend toward ease and economy in fabrication and greater facility in the erection of any structure.

All the profiles and tables of sections in this book give the theoretical dimensions, to which we endeavor to work, but, owing to wear of rolls and other contingencies, we cannot guarantee that these profiles will be exactly reproduced in the sections. Wherever a profile applies to more than one weight of a section the dimensions given are for the minimum weight only.

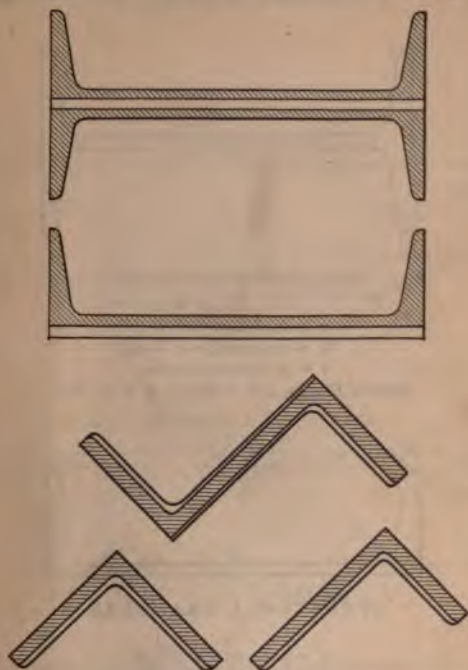
All weights, with the exception of rails, are given in pounds per lineal foot. The weights of rails are given in pounds per lineal yard. Where but one weight is specified for a section that weight only can be rolled.

Beams, channels, sheet piling, tees and zeos should be ordered to weight per lineal foot. Angles should be ordered either to weight per foot or to thickness, but never both. For universal mill plates, there should be specified the width and the thickness, both in inches, the length being given in feet and inches. Sheared plates, on the other hand, should have all dimensions specified in inches. For round and square rods, also bars, the width and the thickness should be specified in inches, the length in feet and inches. For the sizes of rails that we make, it is sufficient to specify weight per yard. For miscellaneous sections always specify the section number.

The association of American Steel Manufacturers recommend that certain sections of angles be considered as standard for general building construction, ship, car and bridge work. These angles have been indicated by printing their index numbers in bold-faced type in the tables on the profile pages and it is generally to the advantage of the customer to specify these standard sizes wherever possible.

In ordering material to specified lengths, the usual allowances for over or under length vary from $\frac{1}{4}$ " to $\frac{1}{2}$ " either way, and this should not be lost sight of in determining the lengths to order. *When more exact cutting is required special arrangements are necessary.*

Method of Increasing Sectional Areas



The above figures show the method of increasing the sectional areas and weights of structural shapes. Cross hatched portions represent the minimum sections and the blank portions the added areas.

In the case of Channels and I-Beams, the enlargement of the section adds an equal amount to the thickness of the web and the width of the flanges. In the case of Angles and Zees, the effect of spreading the rolls is slightly to increase the length of the legs. Many of the sizes, however, are rolled in finishing passes whereby the exact dimensions are maintained for different thicknesses.

Inasmuch, however, as these passes are modified in the wear of the rolls, it is impracticable to state what the exact dimensions will be, except in the case of the minimum weight sections. Designers and detailers of structural work should, therefore, arrange for ample clearances.

Common Dimensions of Beams and Channels



STRUCTURAL BEAMS

n = minimum web = t
 R = minimum web + 0.10
 r = $\frac{1}{8}$ minimum web

Slope of Flange, 1:6 = $16\frac{2}{3}\%$ = $9^\circ 27' 42''$



STRUCTURAL CHANNELS

n = minimum web = t
 R = minimum web + 0.10
 r = $\frac{1}{8}$ minimum web

Slope of Flange, 1:6 = $16\frac{2}{3}\%$ = $9^\circ 27' 42''$

All dimensions are in inches and apply only to the minimum weight Beams or Channels.

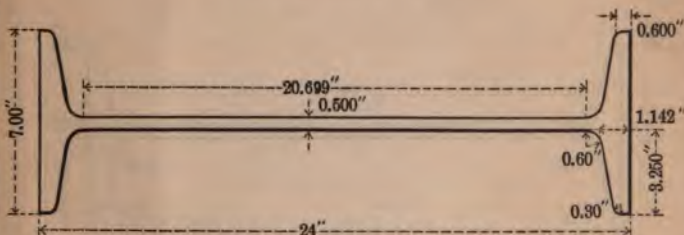
Dimensions given for Structural Beams are those adopted in 1896 by the Association of American Steel Manufacturers and apply to all Beam Sections shown on the pages which follow, except Beam Sections B0 to B7, B12 to B16, and B20 to B26.

Dimensions shown for structural Channels are those adopted by the Association of American Steel Manufacturers and apply to all Structural Channel Sections except C12 to C19.

Structural Beams



B-0 to B-2 115, 110 and 105 lbs.

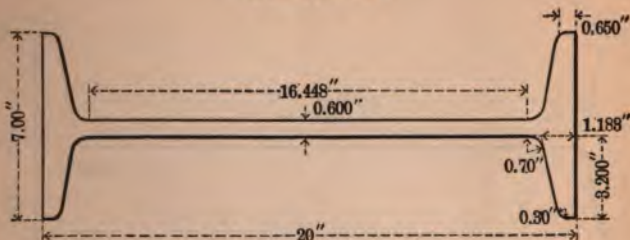


B-3 to B-7 100, 95, 90, 85 and 80 lbs.

Section Index	Depth of Beam, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
B-0	24	115.0	8.000	8	0.750	$\frac{3}{4}$	47
B-1		110.0	7.938	$7\frac{15}{16}$	0.688	$\frac{11}{16}$	49
B-2		105.0	7.875	$7\frac{7}{8}$	0.625	$\frac{5}{8}$	52
B-3	24	100.0	7.254	$7\frac{1}{4}$	0.754	$\frac{3}{4}$	54
B-4		95.0	7.193	$7\frac{1}{8}$	0.693	$\frac{11}{16}$	57
B-5		90.0	7.131	$7\frac{1}{8}$	0.631	$\frac{5}{8}$	60
B-6		85.0	7.070	$7\frac{1}{8}$	0.570	$\frac{9}{16}$	64
B-7		80.0	7.000	7	0.500	$\frac{1}{2}$	60

Structural Beams

Continued



B-12-B-16 100, 95, 90, 85 and 80 lbs.

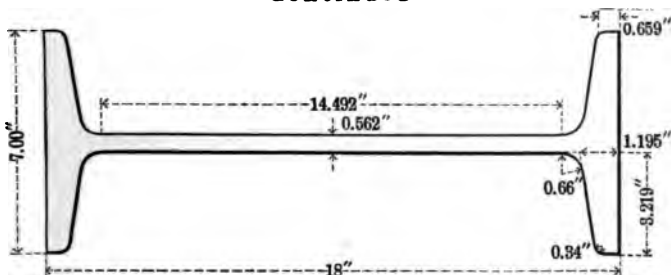


B-20-B-22 75, 70 and 65 lbs.

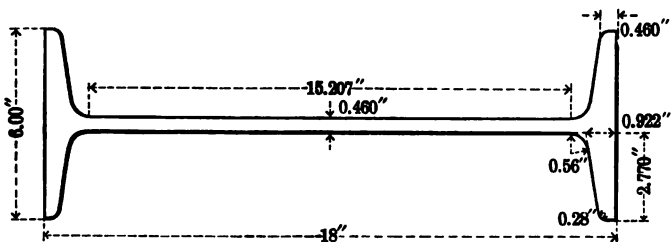
Section Index	Depth of Beam, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
B-12	20	100.0	7.284	$7\frac{9}{32}$	0.884	$\frac{57}{64}$	46
B-13		95.0	7.210	$7\frac{13}{64}$	0.810	$\frac{13}{16}$	49
B-14		90.0	7.137	$7\frac{9}{64}$	0.737	$\frac{47}{64}$	52
B-15		85.0	7.063	$7\frac{1}{16}$	0.663	$\frac{21}{32}$	55
B-16		80.0	7.000	7	0.600	$\frac{19}{32}$	57
B-20	20	75.0	6.399	$6\frac{13}{32}$	0.649	$\frac{21}{32}$	61
B-21		70.0	6.325	$6\frac{21}{64}$	0.575	$\frac{37}{64}$	66
B-22		65.0	6.250	$6\frac{1}{4}$	0.500	$\frac{1}{2}$	72

Structural Beams

Continued



*B-23 to B-26 90, 85, 80 and 75 lbs.



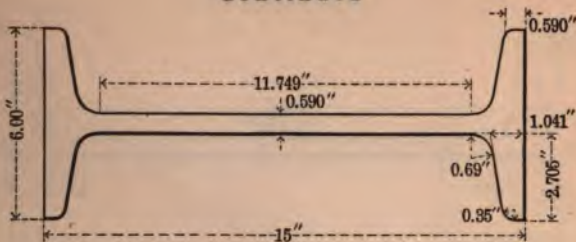
B-27 to B-30 70, 65, 60 and 55 lbs.

Section Index	Depth of Beam, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
*B-23	18	90.0	7.245	7 $\frac{1}{4}$	0.807	$\frac{13}{16}$	51
*B-24		85.0	7.163	7 $\frac{5}{8}$	0.725	$\frac{3}{4}$	54
*B-25		80.0	7.082	7 $\frac{5}{8}$	0.644	$\frac{3}{4}$	57
*B-26		75.0	7.000	7	0.562	$\frac{9}{16}$	61
B-27	18	70.0	6.259	6 $\frac{1}{4}$	0.719	$\frac{3}{4}$	66
B-28		65.0	6.177	6 $\frac{1}{4}$	0.637	$\frac{3}{4}$	71
B-29		60.0	6.095	6 $\frac{1}{4}$	0.555	$\frac{9}{16}$	77
B-30		55.0	6.000	6	0.460	$\frac{3}{4}$	85

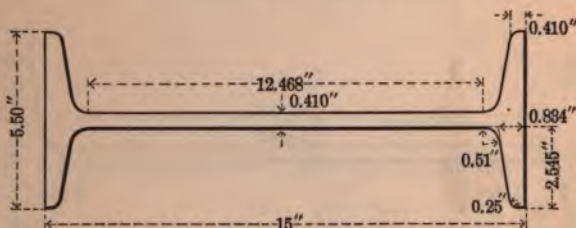
*Proposed Sections—Inserted for reference only.

Structural Beams

Continued



B-44—B-47 75, 70, 65 and 60 lbs.

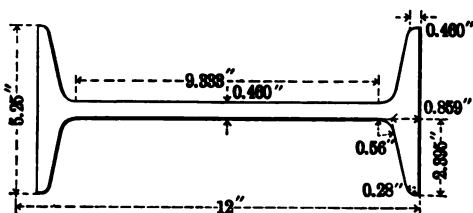


B-52—B-55 55, 50, 45 and 42 lbs.

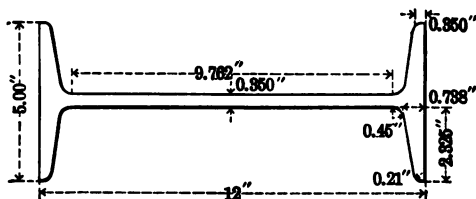
Section Index	Depth of Beam, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
B-44	15	75.0	6.292	$6\frac{19}{64}$	0.882	$\frac{7}{8}$	55
B-45		70.0	6.194	$6\frac{3}{16}$	0.784	$\frac{25}{32}$	59
B-46		65.0	6.096	$6\frac{3}{32}$	0.686	$\frac{11}{16}$	63
B-47		60.0	6.000	6	0.590	$\frac{19}{32}$	69
B-52	15	55.0	5.746	$5\frac{3}{4}$	0.656	$\frac{21}{32}$	76
B-53		50.0	5.648	$5\frac{41}{64}$	0.558	$\frac{9}{16}$	84
B-54		45.0	5.550	$5\frac{35}{64}$	0.460	$\frac{29}{64}$	93
B-55		42.0	5.500	$5\frac{1}{2}$	0.410	$\frac{13}{32}$	95

Structural Beams

Continued



B-60-B-63 55, 50, 45 and 40 lbs.

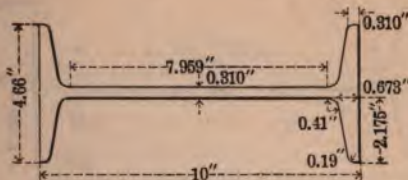


B-68-B-69 35 and 31.5 lbs.

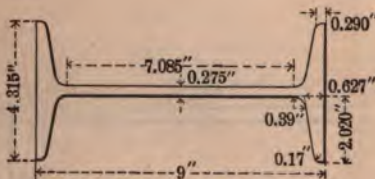
Section Index	Depth of Beam, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
B-60	12	55.0	5.611	5 $\frac{11}{16}$	0.821	$\frac{11}{16}$	54
B-61		50.0	5.489	5 $\frac{11}{16}$	0.699	$\frac{11}{16}$	60
B-62		45.0	5.366	5 $\frac{11}{16}$	0.576	$\frac{11}{16}$	64
B-63		40.0	5.250	5 $\frac{1}{4}$	0.460	$\frac{11}{16}$	73
B-68	12	35.0	5.086	5 $\frac{3}{16}$	0.436	$\frac{7}{16}$	84
B-69		31.5	5.000	5	0.350	$\frac{11}{16}$	94

Structural Beams

Continued



B-74-B-77 40, 35, 30 and 25 lbs.

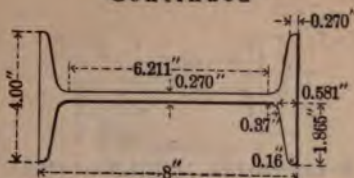


B-82-B-85 35, 30, 25 and 21 lbs.

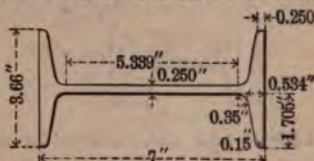
Section Index	Depth of Beam, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
B-74	10	40.0	5.099	$5\frac{3}{32}$	0.749	$\frac{3}{4}$	80
B-75		35.0	4.952	$4\frac{11}{16}$	0.602	$\frac{3}{8}$	90
B-76		30.0	4.805	$4\frac{13}{16}$	0.455	$\frac{29}{64}$	100
B-77		25.0	4.660	$4\frac{1}{2}$	0.310	$\frac{5}{16}$	100
B-82	9	35.0	4.772	$4\frac{49}{64}$	0.732	$\frac{47}{64}$	90
B-83		30.0	4.609	$4\frac{39}{64}$	0.569	$\frac{9}{16}$	100
B-84		25.0	4.446	$4\frac{29}{64}$	0.406	$\frac{13}{32}$	100
B-85		21.0	4.315	$4\frac{5}{16}$	0.275	$\frac{9}{32}$	100

Structural Beams

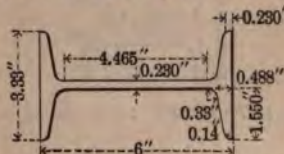
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B-90-B-93 25.5, 23, 20.5 and 18 lbs.



B-98-B-100 20, 17.5 and 15 lbs.

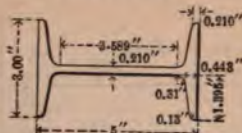


B-105-B-107 17.25, 14.75 and 12.25 lbs.

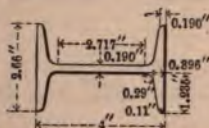
Section Index	Depth of Beam, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
B-90	8	25.5	4.271	$4\frac{11}{64}$	0.541	$\frac{35}{64}$	90
B-91		23.0	4.179	$4\frac{11}{64}$	0.449	$\frac{29}{64}$	100
B-92		20.5	4.087	$4\frac{3}{32}$	0.357	$\frac{23}{64}$	100
B-93		18.0	4.000	4	0.270	$\frac{11}{64}$	100
B-98	7	20	3.868	$3\frac{7}{8}$	0.458	$\frac{29}{64}$	90
B-99		17.5	3.763	$3\frac{43}{64}$	0.353	$\frac{23}{64}$	100
B-100		15.0	3.660	$3\frac{21}{32}$	0.250	$\frac{1}{4}$	100
B-105	6	17.25	3.575	$3\frac{21}{64}$	0.475	$\frac{15}{32}$	90
B-106		14.75	3.452	$3\frac{29}{64}$	0.352	$\frac{23}{64}$	100
B-107		12.25	3.330	$3\frac{33}{64}$	0.230	$\frac{15}{64}$	100

Structural Beams

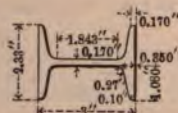
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B-112-B-114 14.75, 12.25 and 9.75 lbs.



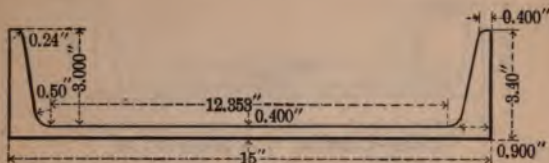
B-119-B-122 10.5, 9.5, 8.5 and 7.5 lbs.



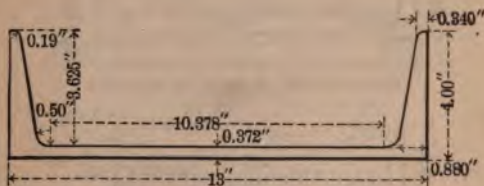
B-127-B-129 7.5, 6.5 and 5.5 lbs.

Section Index	Depth of Beam, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
B-112	5	14.75	3.294	$3\frac{19}{64}$	0.504	$\frac{1}{2}$	90
B-113		12.25	3.147	$3\frac{9}{64}$	0.357	$\frac{23}{64}$	100
B-114		9.75	3.000	3	0.210	$\frac{5}{24}$	100
B-119	4	10.5	2.880	$2\frac{7}{8}$	0.410	$\frac{13}{32}$	50
B-120		9.5	2.807	$2\frac{13}{16}$	0.337	$\frac{11}{32}$	55
B-121		8.5	2.733	$2\frac{7}{8}$	0.263	$\frac{17}{64}$	65
B-122		7.5	2.660	$2\frac{33}{64}$	0.190	$\frac{3}{16}$	65
B-127	3	7.5	2.521	$2\frac{33}{64}$	0.361	$\frac{23}{64}$	33
B-128		6.5	2.423	$2\frac{17}{32}$	0.263	$\frac{17}{64}$	38
B-129		5.5	2.330	$2\frac{11}{16}$	0.170	$\frac{11}{64}$	45

Structural Channels



C-3-C-8 55, 50, 45, 40, 35 and 33 lbs.

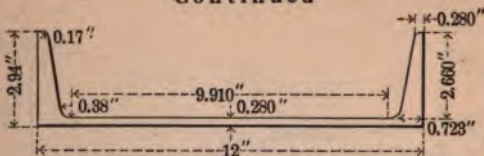


C-12-C-19 52.5, 50, 45, 40, 37.5, 35, 32 and 31.5 lbs.

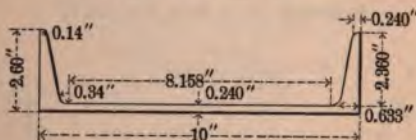
Section Index	Depth of Channel, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
C-3	15	55.0	3.818	$3\frac{13}{16}$	0.818	$\frac{13}{16}$	75
C-4		50.0	3.720	$3\frac{23}{32}$	0.720	$\frac{23}{32}$	84
C-5		45.0	3.622	$3\frac{5}{8}$	0.622	$\frac{5}{8}$	95
C-6		40.0	3.524	$3\frac{17}{32}$	0.524	$\frac{17}{32}$	95
C-7		35.0	3.426	$3\frac{27}{64}$	0.426	$\frac{27}{64}$	95
C-8		33.0	3.400	$3\frac{1}{2}$	0.400	$\frac{1}{2}$	95
C-12	13	52.5	4.473	$4\frac{15}{32}$	0.848	$\frac{27}{32}$	61
C-13		50.0	4.416	$4\frac{27}{64}$	0.791	$\frac{51}{64}$	64
C-14		45.0	4.303	$4\frac{3}{4}$	0.678	$\frac{3}{4}$	72
C-15		40.0	4.190	$4\frac{9}{16}$	0.565	$\frac{9}{16}$	80
C-16		37.5	4.134	$4\frac{3}{8}$	0.509	$\frac{33}{64}$	86
C-17		35.0	4.077	$4\frac{5}{8}$	0.452	$\frac{29}{64}$	93
C-18		32.0	4.009	$4\frac{1}{4}$	0.384	$\frac{25}{64}$	95
C-19		31.5	3.997	4	0.372	$\frac{3}{8}$	95

Structural Channels

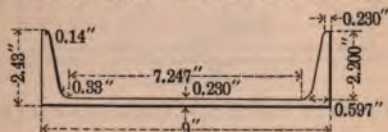
Continued



C-23-C-27 40, 35, 30, 25 and 20.5 lbs.



C-32-C-36 35, 30, 25, 20 and 15 lbs.

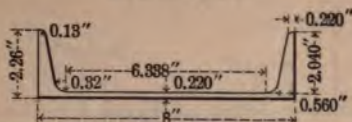


C-41-C-44 25, 20, 15 and 13.25 lbs.

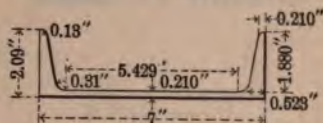
Section Index	Depth of Channel, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
C-23	12	40.0	3.418	$\frac{327}{64}$	0.758	$\frac{49}{64}$	80
C-24		35.0	3.296	$\frac{319}{64}$	0.636	$\frac{41}{64}$	89
C-25		30.0	3.173	$\frac{311}{64}$	0.513	$\frac{33}{64}$	95
C-26		25.0	3.050	$\frac{303}{64}$	0.390	$\frac{25}{64}$	95
C-27		20.5	2.940	$\frac{215}{16}$	0.280	$\frac{9}{32}$	95
C-32	10	35.0	3.183	$\frac{313}{16}$	0.823	$\frac{53}{64}$	75
C-33		30.0	3.036	$\frac{313}{32}$	0.676	$\frac{43}{64}$	85
C-34		25.0	2.889	$\frac{287}{64}$	0.529	$\frac{17}{32}$	100
C-35		20.0	2.742	$\frac{287}{64}$	0.382	$\frac{5}{8}$	100
C-36		15.0	2.600	$\frac{219}{32}$	0.240	$\frac{15}{64}$	100
C-41	9	25.0	2.815	$\frac{213}{16}$	0.615	$\frac{39}{64}$	75
C-42		20.0	2.652	$\frac{281}{32}$	0.452	$\frac{23}{64}$	85
C-43		15.0	2.488	$\frac{241}{64}$	0.288	$\frac{9}{32}$	100
C-44		13.25	2.430	$\frac{217}{16}$	0.230	$\frac{14}{64}$	100

Structural Channels

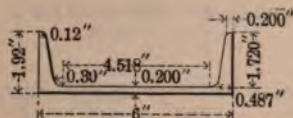
Continued



C-49-C-53 21.25, 18.75, 16.25, 13.75 and 11.25 lbs.



C-58-C-62 19.75, 17.25, 14.75, 12.25 and 9.75 lbs.

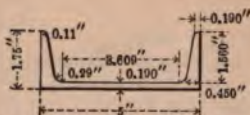


C-67-C-70 15.5, 13, 10.5 and 8 lbs.

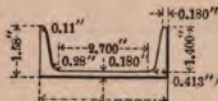
Section Index	Depth of Channel, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
C-49	8	21.25	2.622	$2\frac{5}{8}$	0.582	$\frac{31}{64}$	90
C-50		18.75	2.530	$2\frac{17}{32}$	0.490	$\frac{31}{64}$	100
C-51		16.25	2.439	$2\frac{17}{32}$	0.399	$\frac{13}{32}$	100
C-52		13.75	2.347	$2\frac{11}{32}$	0.307	$\frac{5}{16}$	100
C-53		11.25	2.260	$2\frac{11}{16}$	0.220	$\frac{7}{32}$	100
C-58	7	19.75	2.513	$2\frac{13}{32}$	0.633	$\frac{41}{64}$	100
C-59		17.25	2.408	$2\frac{13}{32}$	0.528	$\frac{17}{32}$	100
C-60		14.75	2.303	$2\frac{13}{32}$	0.423	$\frac{27}{64}$	100
C-61		12.25	2.198	$2\frac{13}{64}$	0.318	$\frac{5}{16}$	100
C-62		9.75	2.090	$2\frac{3}{32}$	0.210	$\frac{13}{64}$	100
C-67	6	15.5	2.283	$2\frac{9}{32}$	0.563	$\frac{2}{16}$	90
C-68		13.0	2.160	$2\frac{5}{32}$	0.440	$\frac{17}{64}$	100
C-69		10.5	2.038	$2\frac{1}{32}$	0.318	$\frac{13}{64}$	100
C-70		8.0	1.920	$1\frac{59}{64}$	0.200	$\frac{13}{64}$	100

Structural Channels

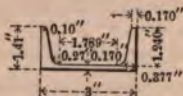
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C-75-C-77 11.5, 9 and 6.5 lbs.



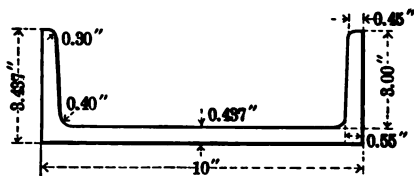
C-82-C-84 7.25, 6.25 and 5.25 lbs.



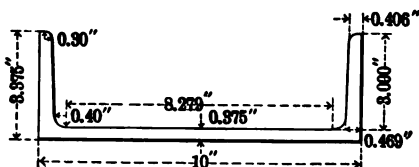
C-89-C-91 6, 5 and 4 lbs.

Section Index	Depth of Channel, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
C-75	5	11.5	2.037	$2\frac{1}{32}$	0.477	$\frac{31}{64}$	65
C-76		9.0	1.890	$1\frac{27}{32}$	0.330	$\frac{21}{64}$	65
C-77		6.5	1.750	$1\frac{3}{4}$	0.190	$\frac{3}{16}$	65
C-82	4	7.25	1.725	$1\frac{23}{32}$	0.325	$\frac{21}{64}$	65
C-83		6.25	1.652	$1\frac{33}{32}$	0.252	$\frac{1}{4}$	65
C-84		5.25	1.580	$1\frac{37}{64}$	0.180	$\frac{3}{16}$	65
C-89	3	6.0	1.602	$1\frac{29}{64}$	0.362	$\frac{23}{64}$	42
C-90		5.0	1.504	$1\frac{1}{2}$	0.264	$\frac{11}{64}$	50
C-91		4.0	1.410	$1\frac{13}{32}$	0.170	$\frac{11}{64}$	50

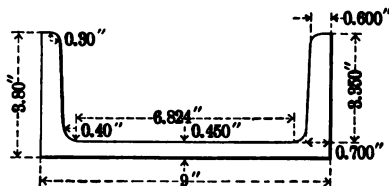
Ship Building Channels



C-101-C-102 27.2 and 25 lbs.



C-105 21.8 lbs.



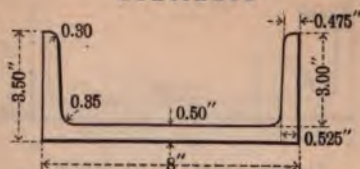
*C-107 to C-109

Section Index	Depth of Channel, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
C-101	10	27.2	3.500	3½	0.500	½	95
C-102		25.0	3.437	3⅞	0.437	⅞	95
C-105	10	21.8	3.375	3⅜	0.375	¾	95
*C-107	9	34.7	4.000	4	0.650	⅞	85
*C-108		31.7	3.900	3⅞	0.550	⅞	85
*C-109		28.6	3.800	3⅞	0.450	⅞	85

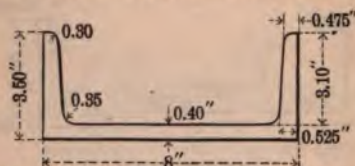
*Proposed Sections—Inserted for reference only.

Ship Building Channels

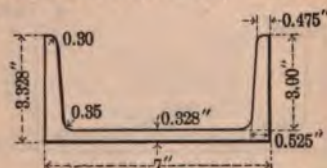
Continued



C-114 to C-116 26.5, 25.2 and 23.8 lbs.



C-117 to C-119 24.2, 22.8 and 21.4 lbs.

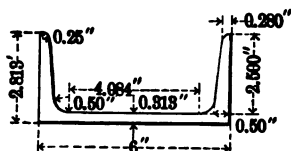


C-121 to C-123 22.1, 20 and 18 lbs.

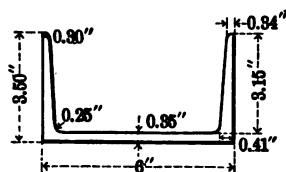
Section Index	Depth of Channel, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
C-114	8	26.5	3.600	$3\frac{13}{16}$	0.600	$\frac{13}{16}$	85
C-115		25.2	3.550	$3\frac{33}{64}$	0.550	$\frac{33}{64}$	85
C-116		23.8	3.500	$3\frac{1}{2}$	0.500	$\frac{1}{2}$	90
C-117	8	24.2	3.600	$3\frac{13}{16}$	0.500	$\frac{1}{2}$	90
C-118		22.8	3.550	$3\frac{33}{64}$	0.450	$\frac{23}{64}$	95
C-119		21.4	3.500	$3\frac{1}{2}$	0.400	$\frac{13}{32}$	100
C-121	7	22.1	3.500	$3\frac{1}{2}$	0.500	$\frac{1}{2}$	75
C-122		20.0	3.412	$3\frac{13}{32}$	0.412	$\frac{13}{32}$	85
C-123		18.0	3.328	$3\frac{21}{64}$	0.328	$\frac{21}{64}$	95

Ship Building Channels

Continued



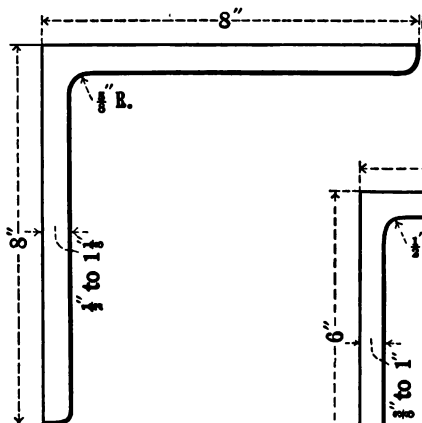
C-128 to C-132 18.1, 16.8, 15.6, 14.3 and 13.0 lbs.



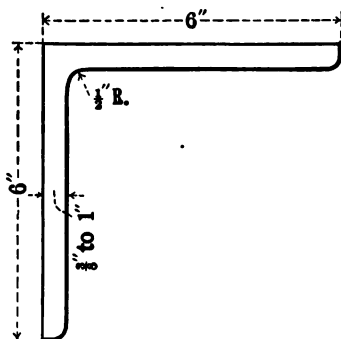
C-137 15 lbs.

Section Index	Depth of Channel, Inches	Weight per Foot, Pounds	FLANGE WIDTH, INCHES		WEB THICKNESS, INCHES		Maximum Length, Feet
			Decimal	Fractional	Decimal	Fractional	
C-128	6	18.1	3.063	$3\frac{1}{16}$	0.563	$\frac{9}{16}$	30
C-129		16.8	3.000	3	0.500	$\frac{1}{2}$	30
C-130		15.6	2.936	$2\frac{1}{8}$	0.437	$\frac{7}{16}$	35
C-131		14.3	2.874	$2\frac{7}{8}$	0.375	$\frac{3}{8}$	35
C-132		13.0	2.813	$2\frac{1}{4}$	0.313	$\frac{1}{4}$	40
C-137	6	15.0	3.500	$3\frac{1}{2}$	0.350	$\frac{1}{2}$	100

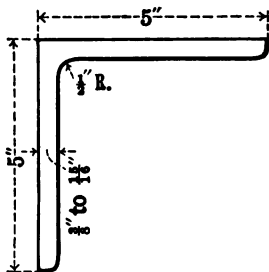
Angles With Equal Legs



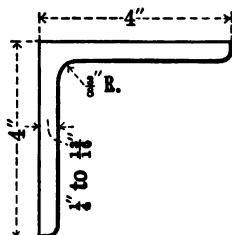
A-3 to A-13 56.9 to 26.4 lbs.



A-17 to A-27 37.4 to 14.9 lbs.



A-33 to A-42 28.9 to 12.3 lbs.



A-47 to A-56 19.9 to 6.6 lbs.

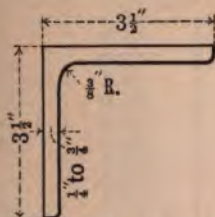
Angles With Equal Legs

Section Index	Size, Inches	Thickness, Inches	Weight per Foot, Pounds	Maximum Length, Feet
A-3	8 x 8	$1\frac{1}{8}$	56.9	78
A-4	8 x 8	$1\frac{1}{16}$	54.0	83
A-5	8 x 8	1	51.0	87
A-6	8 x 8	$\frac{15}{16}$	48.1	95
A-7	8 x 8	$\frac{7}{8}$	45.0	95
A-8	8 x 8	$\frac{13}{16}$	42.0	95
A-9	8 x 8	$\frac{3}{4}$	38.9	95
A-10	8 x 8	$\frac{11}{16}$	35.8	95
A-11	8 x 8	$\frac{5}{8}$	32.7	95
A-12	8 x 8	$\frac{9}{16}$	29.6	95
A-13	8 x 8	$\frac{1}{2}$	26.4	95
A-17	6 x 6	1	37.4	100
A-18	6 x 6	$\frac{15}{16}$	35.3	100
A-19	6 x 6	$\frac{7}{8}$	33.1	100
A-20	6 x 6	$\frac{13}{16}$	31.0	100
A-21	6 x 6	$\frac{3}{4}$	28.7	100
A-22	6 x 6	$\frac{11}{16}$	26.5	100
A-23	6 x 6	$\frac{5}{8}$	24.2	100
A-24	6 x 6	$\frac{9}{16}$	21.9	100
A-25	6 x 6	$\frac{1}{2}$	19.6	100
A-26	6 x 6	$\frac{7}{16}$	17.2	100
A-27	6 x 6	$\frac{3}{8}$	14.9	100
A-33	5 x 5	$\frac{15}{16}$	28.9	100
A-34	5 x 5	$\frac{7}{8}$	27.2	100
A-35	5 x 5	$\frac{13}{16}$	25.4	100
A-36	5 x 5	$\frac{3}{4}$	23.6	100
A-37	5 x 5	$\frac{11}{16}$	21.8	100
A-38	5 x 5	$\frac{5}{8}$	20.0	100
A-39	5 x 5	$\frac{9}{16}$	18.1	100
A-40	5 x 5	$\frac{1}{2}$	16.2	100
A-41	5 x 5	$\frac{7}{16}$	14.3	100
A-42	5 x 5	$\frac{3}{8}$	12.3	100
A-47	4 x 4	$\frac{13}{16}$	19.9	50
A-48	4 x 4	$\frac{3}{4}$	18.5	52
A-49	4 x 4	$\frac{11}{16}$	17.1	56
A-50	4 x 4	$\frac{5}{8}$	15.7	61
A-51	4 x 4	$\frac{9}{16}$	14.3	65
A-52	4 x 4	$\frac{1}{2}$	12.8	65
A-53	4 x 4	$\frac{7}{16}$	11.3	65
A-54	4 x 4	$\frac{3}{8}$	9.8	65
A-55	4 x 4	$\frac{5}{16}$	8.2	65
A-56	4 x 4	$\frac{1}{4}$	6.6	65

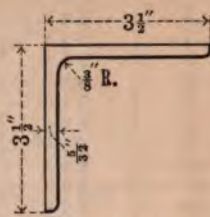
Sections appearing in bold-face type adopted as standard by the Association of American Steel Manufacturers for bridge, car, ship and general building construction.

Angles With Equal Legs

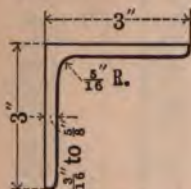
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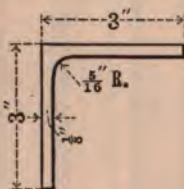
A-62 to A-70 16.0 to 5.8 lbs.



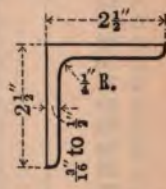
A-75 3.64 lbs.



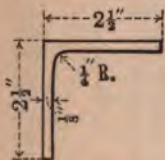
A-98 to A-105
11.5 to 3.71 lbs.



A-110
2.50 lbs.



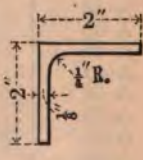
A-130 to A-135
7.7 to 3.07 lbs.



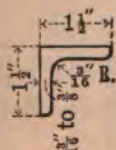
A-140
2.08 lbs.



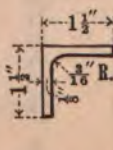
A-160 to A-165
6.0 to 2.44 lbs.



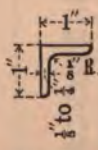
A-170
1.65 lbs.



A-189 to A-192
3.35 to 1.80 lbs.



A-197
1.23 lbs.



A-224 to A-226
1.49 to 0.80 lbs.

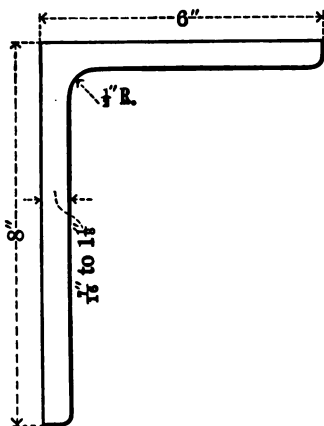
JONES & LAUGHLIN STEEL COMPANY

Angles With Equal Legs

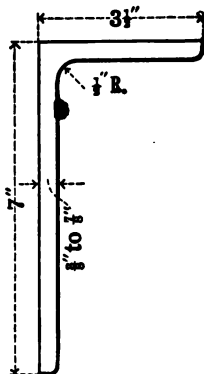
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Section Index	Size, Inches	Thickness, Inches	Weight per Foot, Pounds	Maximum Length, Feet
A- 62	3 1/2 x 3 1/2	3/4	16.0	50
A- 63	3 1/2 x 3 1/2	11/16	14.8	54
A- 64	3 1/2 x 3 1/2	5/8	13.6	60
A- 65	3 1/2 x 3 1/2	9/16	12.4	65
A- 66	3 1/2 x 3 1/2	1/2	11.1	65
A- 67	3 1/2 x 3 1/2	7/16	9.8	65
A- 68	3 1/2 x 3 1/2	3/8	8.5	65
A- 69	3 1/2 x 3 1/2	5/16	7.2	65
A- 70	3 1/2 x 3 1/2	1/4	5.8	65
A- 75	3 1/2 x 3 1/2	5/32	3.64	45
A- 98	3 x 3	5/8	11.5	50
A- 99	3 x 3	9/16	10.4	55
A-100	3 x 3	1/2	9.4	60
A-101	3 x 3	7/16	8.3	65
A-102	3 x 3	3/8	7.2	65
A-103	3 x 3	5/16	6.1	65
A-104	3 x 3	1/4	4.9	65
A-105	3 x 3	3/16	3.71	45
A-110	3 x 3	1/8	2.50	40
A-130	2 1/2 x 2 1/2	1/2	7.7	31
A-131	2 1/2 x 2 1/2	7/16	6.8	35
A-132	2 1/2 x 2 1/2	3/8	5.9	40
A-133	2 1/2 x 2 1/2	5/16	5.0	50
A-134	2 1/2 x 2 1/2	1/4	4.1	50
A-135	2 1/2 x 2 1/2	3/16	3.07	50
A-140	2 1/2 x 2 1/2	1/8	2.08	50
A-160	2 x 2	1/2	6.0	45
A-161	2 x 2	7/16	5.3	45
A-162	2 x 2	3/8	4.7	45
A-163	2 x 2	5/16	3.92	50
A-164	2 x 2	1/4	3.19	50
A-165	2 x 2	3/16	2.44	50
A-170	2 x 2	1/8	1.65	50
A-189	1 1/2 x 1 1/2	3/8	3.35	35
A-190	1 1/2 x 1 1/2	5/16	2.86	35
A-191	1 1/2 x 1 1/2	1/4	2.34	35
A-192	1 1/2 x 1 1/2	3/16	1.80	35
A-197	1 1/2 x 1 1/2	1/8	1.23	35
A-224	1 x 1	1/4	1.49	45
A-225	1 x 1	3/16	1.16	45
A-226	1 x 1	1/8	.80	45

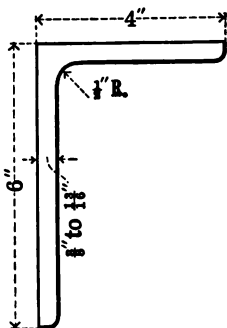
Angles With Unequal Legs



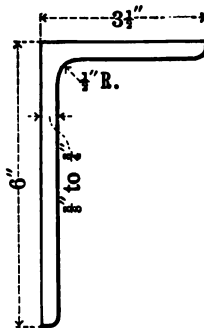
A-233 to A-243
49.3 to 23.0 lbs.
A-650 20.2 lbs.



A-244 to A-252
28.7 to 13.0 lbs.



A-253 to A-265
25.4 to 12.3 lbs.



A-274 to A-280
22.4 to 11.7 lbs.

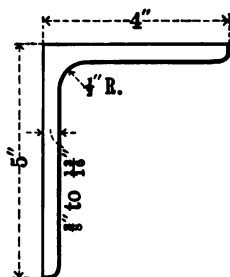
Angles With Unequal Legs

Section Index	Size, Inches	Thickness, Inches	Weight per Foot, Pounds	Maximum Length, Feet
A-233	8 x 6	1 $\frac{1}{8}$	49.3	80
A-234	8 x 6	1 $\frac{1}{16}$	46.8	85
A-235	8 x 6	1	44.2	90
A-236	8 x 6	1 $\frac{5}{16}$	41.7	95
A-237	8 x 6	1 $\frac{7}{8}$	39.1	95
A-238	8 x 6	1 $\frac{1}{2}$	36.5	95
A-239	8 x 6	3 $\frac{3}{4}$	33.8	95
A-240	8 x 6	1 $\frac{1}{2}$	31.2	95
A-241	8 x 6	5 $\frac{5}{8}$	28.5	95
A-242	8 x 6	5 $\frac{1}{8}$	25.7	95
A-243	8 x 6	1 $\frac{1}{2}$	23.0	95
A-650	8 x 6	1 $\frac{1}{8}$	20.2	95
A-244	7 x 3 $\frac{1}{2}$	7 $\frac{7}{8}$	28.7	79
A-245	7 x 3 $\frac{1}{2}$	1 $\frac{1}{2}$	26.8	86
A-246	7 x 3 $\frac{1}{2}$	3 $\frac{3}{4}$	24.9	95
A-247	7 x 3 $\frac{1}{2}$	1 $\frac{1}{2}$	23.0	95
A-248	7 x 3 $\frac{1}{2}$	5 $\frac{5}{8}$	21.0	95
A-249	7 x 3 $\frac{1}{2}$	5 $\frac{1}{8}$	19.1	95
A-250	7 x 3 $\frac{1}{2}$	1 $\frac{1}{2}$	17.0	95
A-251	7 x 3 $\frac{1}{2}$	7 $\frac{7}{8}$	15.0	95
A-252	7 x 3 $\frac{1}{2}$	3 $\frac{3}{8}$	13.0	95
A-258	6 x 4	1 $\frac{1}{8}$	25.4	90
A-259	6 x 4	3 $\frac{3}{4}$	23.6	100
A-260	6 x 4	1 $\frac{1}{2}$	21.8	100
A-261	6 x 4	5 $\frac{5}{8}$	20.0	100
A-262	6 x 4	5 $\frac{1}{8}$	18.1	100
A-263	6 x 4	1 $\frac{1}{2}$	16.2	100
A-264	6 x 4	7 $\frac{7}{8}$	14.3	100
A-265	6 x 4	3 $\frac{3}{8}$	12.3	100
A-274	6 x 3 $\frac{1}{2}$	3 $\frac{3}{4}$	22.4	95
A-275	6 x 3 $\frac{1}{2}$	1 $\frac{1}{2}$	20.6	100
A-276	6 x 3 $\frac{1}{2}$	5 $\frac{5}{8}$	18.9	100
A-277	6 x 3 $\frac{1}{2}$	5 $\frac{1}{8}$	17.1	100
A-278	6 x 3 $\frac{1}{2}$	1 $\frac{1}{2}$	15.3	100
A-279	6 x 3 $\frac{1}{2}$	7 $\frac{7}{8}$	13.5	100
A-280	6 x 3 $\frac{1}{2}$	3 $\frac{3}{8}$	11.7	100

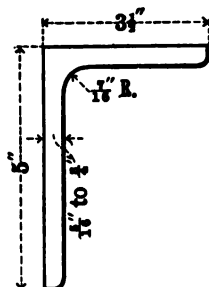
Sections appearing in bold-face type adopted as standard by the Association of American Steel Manufacturers, for bridge, car, ship and general building construction.

Angles With Unequal Legs

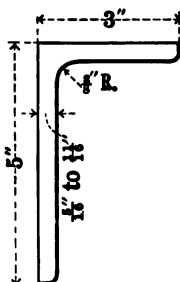
Continued



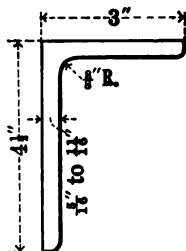
A-286 to A-293
22.7 to 11.0 lbs.



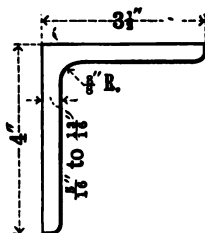
A-300 to A-307
19.8 to 8.7 lbs.



A-315 to A-321
17.1 to 8.3 lbs.



A-328 to A-334
16.0 to 7.7 lbs.



A-339 to A-347
18.5 to 7.7 lbs.

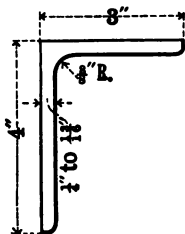
Angles With Unequal Legs

Continued

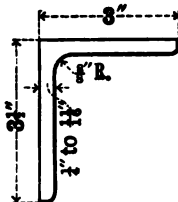
Section Index	Size, Inches	Thickness, Inches	Weight per Foot, Pounds	Maximum Length, Feet
A-286	5 x 4	$\frac{13}{16}$	22.7	68
A-287	5 x 4	$\frac{3}{4}$	21.1	75
A-288	5 x 4	$\frac{13}{16}$	19.5	82
A-289	5 x 4	$\frac{5}{8}$	17.8	90
A-290	5 x 4	$\frac{9}{16}$	16.2	100
A-291	5 x 4	$\frac{1}{2}$	14.5	100
A-292	5 x 4	$\frac{7}{16}$	12.8	100
A-293	5 x 4	$\frac{3}{8}$	11.0	100
A-300	5 x 3 $\frac{1}{2}$	$\frac{3}{4}$	19.8	80
A-301	5 x 3 $\frac{1}{2}$	$\frac{11}{16}$	18.3	87
A-302	5 x 3 $\frac{1}{2}$	$\frac{5}{8}$	16.8	90
A-303	5 x 3 $\frac{1}{2}$	$\frac{9}{16}$	15.2	100
A-304	5 x 3 $\frac{1}{2}$	$\frac{1}{2}$	13.6	100
A-305	5 x 3 $\frac{1}{2}$	$\frac{7}{16}$	12.0	100
A-306	5 x 3 $\frac{1}{2}$	$\frac{3}{8}$	10.4	100
A-307	5 x 3 $\frac{1}{2}$	$\frac{5}{16}$	8.7	100
A-315	5 x 3	$\frac{11}{16}$	17.1	90
A-316	5 x 3	$\frac{9}{16}$	15.7	97
A-317	5 x 3	$\frac{9}{16}$	14.3	100
A-318	5 x 3	$\frac{7}{16}$	12.8	100
A-319	5 x 3	$\frac{7}{16}$	11.3	100
A-320	5 x 3	$\frac{3}{8}$	9.8	100
A-321	5 x 3	$\frac{5}{16}$	8.2	100
A-328	4 $\frac{1}{2}$ x 3	$\frac{11}{16}$	16.0	50
A-329	4 $\frac{1}{2}$ x 3	$\frac{5}{8}$	14.7	54
A-330	4 $\frac{1}{2}$ x 3	$\frac{9}{16}$	13.3	60
A-331	4 $\frac{1}{2}$ x 3	$\frac{1}{2}$	11.9	65
A-332	4 $\frac{1}{2}$ x 3	$\frac{7}{16}$	10.6	65
A-333	4 $\frac{1}{2}$ x 3	$\frac{3}{8}$	9.1	65
A-334	4 $\frac{1}{2}$ x 3	$\frac{5}{16}$	7.7	65
A-339	4 x 3 $\frac{1}{2}$	$\frac{11}{16}$	18.5	44
A-340	4 x 3 $\frac{1}{2}$	$\frac{3}{4}$	17.3	46
A-341	4 x 3 $\frac{1}{2}$	$\frac{11}{16}$	16.0	50
A-342	4 x 3 $\frac{1}{2}$	$\frac{5}{8}$	14.7	54
A-343	4 x 3 $\frac{1}{2}$	$\frac{9}{16}$	13.3	60
A-344	4 x 3 $\frac{1}{2}$	$\frac{1}{2}$	11.9	65
A-345	4 x 3 $\frac{1}{2}$	$\frac{7}{16}$	10.6	65
A-346	4 x 3 $\frac{1}{2}$	$\frac{3}{8}$	9.1	65
A-347	4 x 3 $\frac{1}{2}$	$\frac{5}{16}$	7.7	65

Angles With Unequal Legs

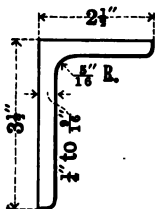
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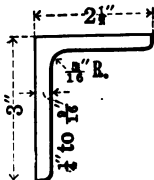
A-354 to A-361
14.8 to 5.8 lbs.



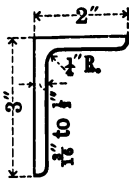
A-365 to A-372
12.6 to 5.4 lbs.



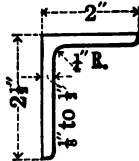
A-379 to A-384
10.4 to 4.9 lbs.



A-405 to A-410
9.5 to 4.5 lbs.



A-415 to A-420
7.7 to 3.07 lbs.



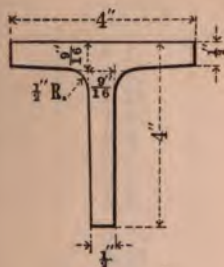
A-425 to A-431
6.8 to 1.86 lbs.

Angles With Unequal Legs

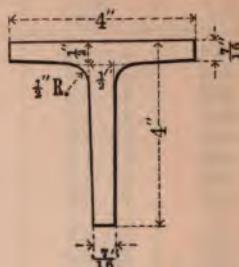
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Section Index	Size, Inches	Thickness, Inches	Weight per Foot, Pounds	Maximum Length, Feet
A-354	4 x 3	$\frac{1}{8}$	14.8	54
A-355	4 x 3	$\frac{5}{8}$	13.6	60
A-356	4 x 3	$\frac{1}{8}$	12.4	65
A-357	4 x 3	$\frac{1}{2}$	11.1	65
A-358	4 x 3	$\frac{1}{8}$	9.8	65
A-359	4 x 3	$\frac{3}{8}$	8.5	65
A-360	4 x 3	$\frac{1}{8}$	7.2	65
A-361	4 x 3	$\frac{1}{4}$	5.8	65
A-365	$3\frac{1}{2}$ x 3	$\frac{1}{8}$	13.6	40
A-366	$3\frac{1}{2}$ x 3	$\frac{5}{8}$	12.5	44
A-367	$3\frac{1}{2}$ x 3	$\frac{1}{8}$	11.4	48
A-368	$3\frac{1}{2}$ x 3	$\frac{1}{2}$	10.2	50
A-369	$3\frac{1}{2}$ x 3	$\frac{1}{8}$	9.1	55
A-370	$3\frac{1}{2}$ x 3	$\frac{3}{8}$	7.9	60
A-371	$3\frac{1}{2}$ x 3	$\frac{1}{8}$	6.6	65
A-372	$3\frac{1}{2}$ x 3	$\frac{1}{4}$	5.4	65
A-379	$3\frac{1}{2}$ x $2\frac{1}{2}$	$\frac{1}{8}$	10.4	50
A-380	$3\frac{1}{2}$ x $2\frac{1}{2}$	$\frac{1}{2}$	9.4	54
A-381	$3\frac{1}{2}$ x $2\frac{1}{2}$	$\frac{1}{8}$	8.3	65
A-382	$3\frac{1}{2}$ x $2\frac{1}{2}$	$\frac{3}{8}$	7.2	65
A-383	$3\frac{1}{2}$ x $2\frac{1}{2}$	$\frac{1}{8}$	6.1	65
A-384	$3\frac{1}{2}$ x $2\frac{1}{2}$	$\frac{1}{4}$	4.9	65
A-405	3 x $2\frac{1}{2}$	$\frac{1}{8}$	9.5	55
A-406	3 x $2\frac{1}{2}$	$\frac{1}{2}$	8.5	65
A-407	3 x $2\frac{1}{2}$	$\frac{1}{8}$	7.6	65
A-408	3 x $2\frac{1}{2}$	$\frac{3}{8}$	6.6	65
A-409	3 x $2\frac{1}{2}$	$\frac{1}{8}$	5.6	65
A-410	3 x $2\frac{1}{2}$	$\frac{1}{4}$	4.5	65
A-415	3 x 2	$\frac{1}{2}$	7.7	31
A-416	3 x 2	$\frac{1}{8}$	6.8	35
A-417	3 x 2	$\frac{3}{8}$	5.9	40
A-418	3 x 2	$\frac{1}{8}$	5.0	50
A-419	3 x 2	$\frac{1}{4}$	4.1	50
A-420	3 x 2	$\frac{1}{8}$	3.07	50
A-425	$2\frac{1}{2}$ x 2	$\frac{1}{2}$	6.8	35
A-426	$2\frac{1}{2}$ x 2	$\frac{1}{8}$	6.1	45
A-427	$2\frac{1}{2}$ x 2	$\frac{3}{8}$	5.3	45
A-428	$2\frac{1}{2}$ x 2	$\frac{1}{8}$	4.5	50
A-429	$2\frac{1}{2}$ x 2	$\frac{1}{4}$	3.62	50
A-430	$2\frac{1}{2}$ x 2	$\frac{1}{8}$	2.75	55
A-431	$2\frac{1}{2}$ x 2	$\frac{1}{8}$	1.88	55

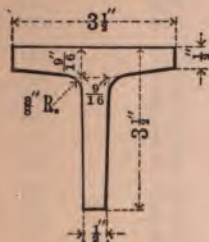
Tees With Equal Legs



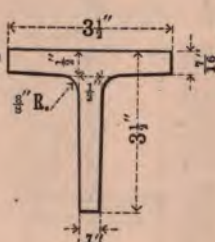
T-3
13.5 lbs.



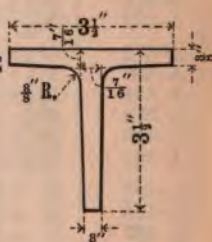
T-4
12.1 lbs.



T-8
11.9 lbs.



T-9
10.5 lbs.

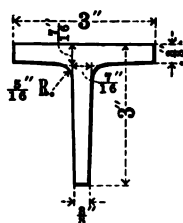


T-10
9.2 lbs.

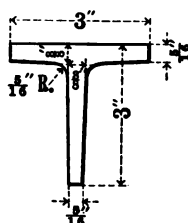
Section Index	SIZE, INCHES		THICKNESS OF METAL, INCHES		Weight per Foot, Pounds	Maximum Length, Feet
	Flange	Stem	Flange	Stem		
T- 3	4	4	1/2 to 9/16	1/2 to 9/16	13.5	40
T- 4	4	4	1/16 to 1/2	1/16 to 1/2	12.1	40
T- 8	3 1/2	3 1/2	1/2 to 9/16	1/2 to 9/16	11.9	40
T- 9	3 1/2	3 1/2	1/16 to 1/2	1/16 to 1/2	10.5	40
T-10	3 1/2	3 1/2	3/8 to 7/16	3/8 to 7/16	9.2	40

Tees With Equal Legs

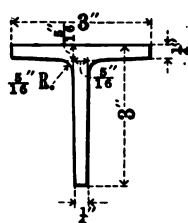
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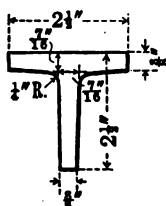
T-15
7.8 lbs.



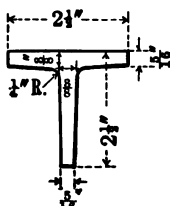
T-16
6.7 lbs.



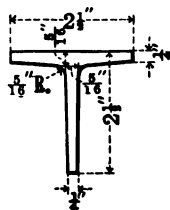
T-17
5.5 lbs.



T-22
6.4 lbs.



T-23
5.5 lbs.



T-24
4.6 lbs.

Section Index	SIZE, INCHES		THICKNESS OF METAL, INCHES		Weight per Foot, Pounds	Maximum Length, Feet
	Flange	Stem	Flange	Stem		
T-15	3	3	3/8 to 1/16	3/8 to 1/16	7.8	40
T-16	3	3	1/8 to 3/8	1/8 to 3/8	6.7	40
T-17	3	3	1/4 to 1/16	1/4 to 1/16	5.5	40
T-22	2 1/2	2 1/2	3/8 to 1/16	3/8 to 1/16	6.4	40
T-23	2 1/2	2 1/2	1/8 to 3/8	1/8 to 3/8	5.5	45
T-24	2 1/2	2 1/2	1/4 to 1/16	1/4 to 1/16	4.6	50

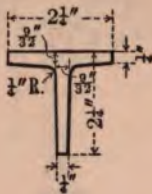
Tees With Equal Legs

Continued



T-28

4.7 lbs.



T-29

3.83 lbs.



T-33

4.1 lbs.



T-34

3.38 lbs.



T-39

2.93 lbs.



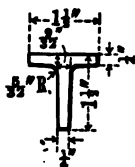
T-40

2.28 lbs.

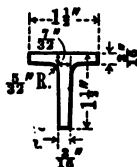
Section Index	SIZE, INCHES		THICKNESS OF METAL, INCHES		Weight per Foot, Pounds	Maximum Length, Feet
	Flange	Stem	Flange	Stem		
T-28	2 1/4	2 1/4	5/16 to 11/32	5/16 to 11/32	4.7	50
T-29	2 1/4	2 1/4	1/4 to 9/32	1/4 to 9/32	3.83	50
T-33	2	2	5/16 to 11/32	5/16 to 11/32	4.1	50
T-34	2	2	1/4 to 9/32	1/4 to 9/32	3.38	50
T-39	1 3/4	1 3/4	1/4 to 9/32	1/4 to 9/32	2.93	40
T-40	1 3/4	1 3/4	3/16 to 7/32	3/16 to 7/32	2.28	40

Tees With Equal Legs

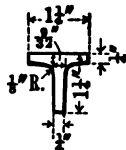
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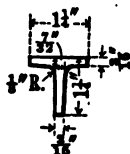
T-45
2.47 lbs.



T-46
1.94 lbs.



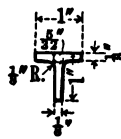
T-51
2.02 lbs.



T-52
1.59 lbs.



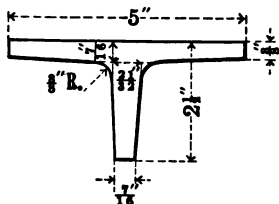
T-57
1.25 lbs.



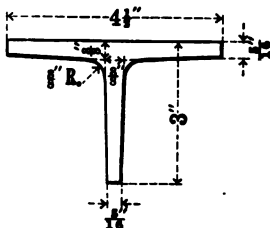
T-58
0.89 lbs.

Section Index	SIZE, INCHES		THICKNESS OF METAL, INCHES		Weight per Foot, Pounds	Maximum Length, Feet
	Flange	Stem	Flange	Stem		
T-45	1 1/2	1 1/2	1/4 to 2/32	1/4 to 2/32	2.47	40
T-46	1 1/2	1 1/2	3/16 to 2/32	3/16 to 2/32	1.94	40
T-51	1 1/4	1 1/4	1/4 to 2/32	1/4 to 2/32	2.02	45
T-52	1 1/4	1 1/4	3/16 to 2/32	3/16 to 2/32	1.59	45
T-57	1	1	3/16 to 2/32	3/16 to 2/32	1.25	45
T-58	1	1	1/8 to 2/32	1/8 to 2/32	.89	45

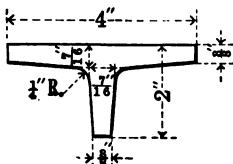
Tees With Unequal Legs



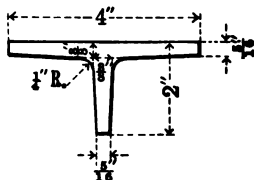
***T-69**
10.9 lbs.



***T-74**
8.4 lbs.



T-79
7.8 lbs.



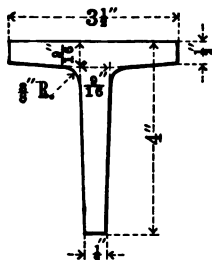
T-80
6.7 lbs.

Section Index	SIZE, INCHES		THICKNESS OF METAL, INCHES		Weight per Foot, Pounds	Maximum Length, Feet
	Flange	Stem	Flange	Stem		
*T-69	5	2 1/2	3/8 to 7/16	7/16 to 1 1/8	10.9	40
*T-74	4 1/2	3	5/16 to 3/8	5/16 to 3/8	8.4	40
T-79	4	2	3/8 to 7/16	3/8 to 7/16	7.8	40
T-80	4	2	5/16 to 3/8	5/16 to 3/8	6.7	40

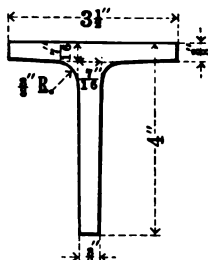
*Made only by special arrangement.

Tees With Unequal Legs

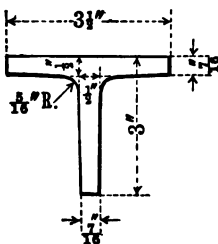
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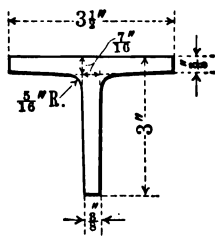
T-85
12.6 lbs.



T-86
9.8 lbs.



T-91
9.7 lbs.

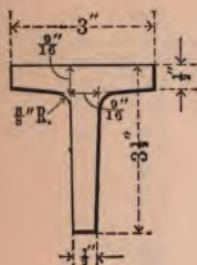


T-92
8.5 lbs.

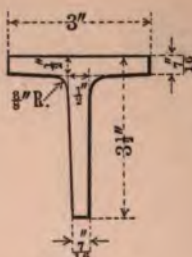
Section Index	Size, Inches		Thickness of Metal, Inches		Weight per Foot, Pounds	Maximum Length, Feet
	Flange	Stem	Flange	Stem		
-85	3 1/2	4	1/2 to 3/8	1/2 to 1/8	12.6	40
-86	3 1/2	4	3/8 to 1/8	3/8 to 1/8	9.8	40
-91	3 1/2	3	1/8 to 1/2	1/8 to 1/2	9.7	40
-92	3 1/2	3	3/8 to 1/8	3/8 to 1/8	8.5	40

Tees With Unequal Legs

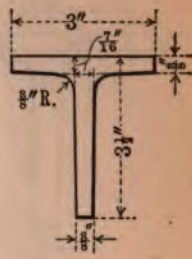
Continued



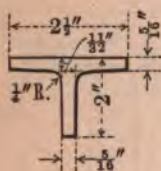
T-96
10.8 lbs.



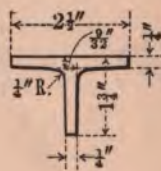
T-97
9.7 lbs.



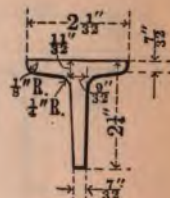
T-98
8.5 lbs.



T-103
4.7 lbs.



T-108
3.60 lbs.

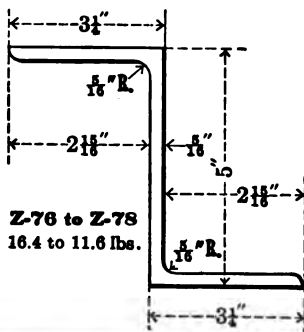
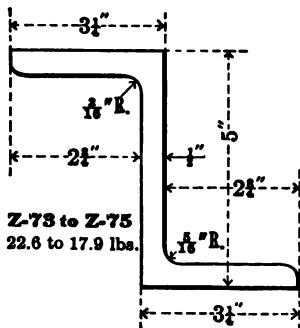
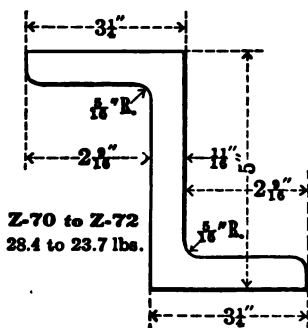


T-112
3.65 lbs.

Section Index	SIZE, INCHES		THICKNESS OF METAL, INCHES		Weight per Foot, Pounds	Maximum Length, Feet
	Flange	Stem	Flange	Stem		
T- 96	3	3 1/2	1/2 to 5/16	1/2 to 5/16	10.8	40
T- 97	3	3 1/2	1/16 to 1/2	1/16 to 1/2	9.7	40
T- 98	3	3 1/2	3/8 to 1/16	3/8 to 1/16	8.5	40
T-103	2 1/2	2	5/16 to 3/32	5/16 to 3/32	4.7	50
T-108	2 1/2	1 3/4	1/4 to 3/32	1/4 to 3/32	3.60	50
T-112	2 3/4	2 1/4	7/32 to 3/32	7/32 to 3/32	3.65	50

JONES & LAUGHLIN STEEL COMPANY

Zees

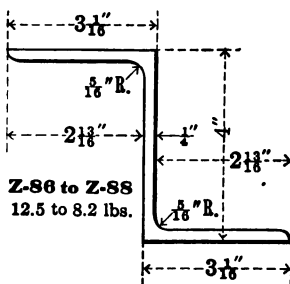
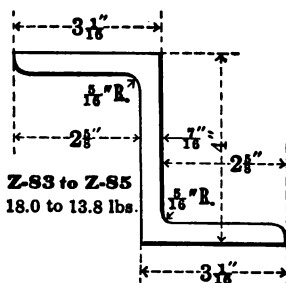
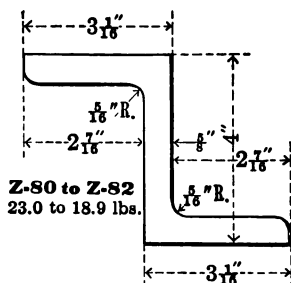


Section Index	SIZE, INCHES			Thickness of Metal, Inches	Weight per Foot, Pounds	Maximum Length, Feet
	Flange	Web	Flange			
Z-70	3 3/8	5 1/8	3 3/8	1 1/8	28.4	37
Z-71	3 5/16	5 1/16	3 5/16	3/4	26.0	40
Z-72	3 1/4	5	3 1/4	1 1/8	23.7	44
Z-73	3 3/8	5 1/8	3 3/8	5/8	22.6	46
Z-74	3 5/16	5 1/16	3 5/16	3/4	20.2	52
Z-75	3 1/4	5	3 1/4	1 1/2	17.9	60
Z-76	3 3/8	5 1/8	3 3/8	7/16	16.4	61
Z-77	3 5/16	5 1/16	3 5/16	3/8	14.0	65
Z-78	3 1/4	5	3 1/4	5/16	11.6	65

JONES & LAUGHLIN STEEL COMPANY

Zees

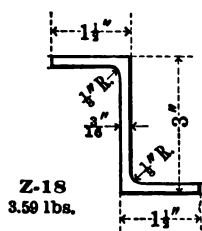
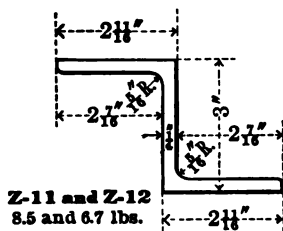
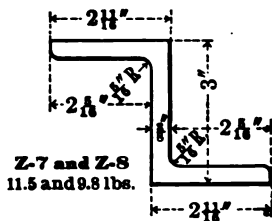
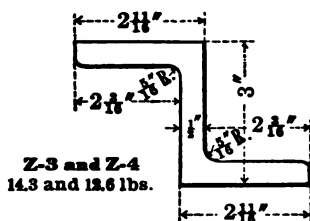
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Section Index	Size, Inches			Thickness of Metal, Inches	Weight per Foot, Pounds	Maximum Length, Feet
	Flange	Web	Flange			
Z-80	3 3/16	4 1/8	3 3/16	3/4	23.0	38
Z-81	3 1/8	4 1/8	3 1/8	1/2	20.9	42
Z-82	3 1/8	4	3 1/8	5/8	18.9	46
Z-83	3 1/8	4 1/8	3 1/8	3/8	18.0	48
Z-84	3 1/8	4 1/8	3 1/8	1/2	15.9	55
Z-85	3 1/8	4	3 1/8	1/8	13.8	62
Z-86	3 3/16	4 1/8	3 3/16	3/8	12.5	65
Z-87	3 1/8	4 1/8	3 1/8	5/16	10.3	65
Z-88	3 1/8	4	3 1/8	1/4	8.2	65

Zees

Continued



Section Index	SIZE, INCHES			Thickness of Metal, Inches	Weight per Foot, Pounds	Maximum Length, Feet
	Flange	Web	Flange			
Z- 3	2 3/4	3 1/16	2 3/4	9/16	14.3	56
Z- 4	2 11/16	3	2 11/16	1/2	12.6	64
Z- 7	2 3/4	3 1/16	2 3/4	7/16	11.5	65
Z- 8	2 11/16	3	2 11/16	3/8	9.8	65
Z-11	2 3/4	3 1/16	2 3/4	5/16	8.5	65
Z-12	2 11/16	3	2 11/16	1/4	6.7	65
Z-18	1 1/2	3	1 1/2	3/16	3.59	65

Areas of Angles Square Inches

Size, Inches	$\frac{1}{8}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{11}{16}$	$\frac{3}{4}$	$\frac{13}{16}$	$\frac{7}{8}$	$\frac{15}{16}$	1	$1\frac{1}{16}$	$1\frac{1}{8}$
8 x 8	7.75	8.68	9.61	10.53	11.44	12.34	13.23	14.12	15.00	15.87	16.73
8 x 6	5.94	6.75	7.56	8.36	9.15	9.94	10.72	11.48	12.25	13.00	13.77	14.50
7 x $3\frac{1}{2}$	3.81	4.40	5.00	5.59	6.17	6.75	7.31	7.87	8.42
6 x 6	4.36	5.06	5.75	6.43	7.11	7.78	8.44	9.09	9.73	10.37	11.00
6 x 4	3.61	4.18	4.75	5.31	5.86	6.40	6.94	7.47
6 x $3\frac{1}{2}$	3.42	3.97	4.50	5.03	5.55	6.06	6.56
5 x 5	3.61	4.18	4.75	5.31	5.86	6.40	6.94	7.47	7.99	8.50
5 x 4	3.23	3.75	4.25	4.75	5.23	5.71	6.19	6.65
5 x $3\frac{1}{2}$	2.56	3.05	3.53	4.00	4.47	4.92	5.37	5.81
5 x 3	2.40	2.86	3.31	3.75	4.18	4.61	5.03
4 x $3\frac{1}{2}$	2.25	2.67	3.09	3.50	3.90	4.30	4.68
4 x 4	1.94	2.40	2.86	3.31	3.75	4.18	4.61	5.03	5.44
4 x $3\frac{1}{2}$	2.25	2.67	3.09	3.50	3.90	4.30	4.68	5.06
3 x $3\frac{1}{2}$	1.69	2.09	2.48	2.87	3.25	3.62	3.98	4.34
3 x 3	1.56	1.93	2.30	2.65	3.00	3.34	3.67	4.00
3 x $2\frac{1}{2}$	1.44	1.78	2.11	2.43	2.75	3.06
3 x 3	0.73	1.09	1.44	1.78	2.11	2.43	2.75	3.06	3.36
3 x $2\frac{1}{2}$	1.31	1.62	1.92	2.21	2.50	2.78
3 x 2	1.19	1.47	1.73	2.00	2.25
2 x $2\frac{1}{2}$	0.61	0.90	1.19	1.47	1.73	2.00	2.25
2 x 2	0.81	1.06	1.31	1.55	1.78	2.00
2 x 2	0.48	0.71	0.94	1.15	1.36	1.56	1.75
1 x $1\frac{1}{2}$	0.36	0.53	0.69	0.84	0.99
1 x 1	0.23	0.34	0.44

Rounds



$\frac{1}{16}''$ to 1' advancing by 64ths.
 $1\frac{1}{2}''$ to 2' advancing by 32nds.
 $2\frac{1}{16}''$ to $7\frac{1}{2}''$ advancing by 16ths.



We have grooves for rolling a large variety of bolt and rivet sizes to decimal diameters.

Sizes $\frac{3}{4}''$ and under can be furnished in coils.

Squares



$\frac{1}{16}''$ to 2' advancing by 64ths.
 $2\frac{1}{16}''$ to 5' advancing by 16ths.



All intermediate sizes can be rolled by special arrangement.

Maximum Length of Rounds

Diameter, Inches	Length, Feet
$\frac{1}{4}$ to $\frac{7}{8}$	40
$\frac{1}{2}$ to $2\frac{1}{8}$	60
$2\frac{1}{8}$ to $4\frac{1}{2}$	48
$4\frac{1}{8}$ to $5\frac{1}{2}$	46
$5\frac{1}{8}$	44
$5\frac{5}{8}$	43
$5\frac{1}{4}$	42
$5\frac{3}{4}$	41
$5\frac{1}{2}$	40
$5\frac{7}{8}$ to $5\frac{1}{4}$	39
6	38
$6\frac{1}{8}$	37
$6\frac{1}{4}$	36
$6\frac{1}{2}$	35
$6\frac{3}{4}$ and $6\frac{5}{8}$	34
$6\frac{7}{8}$	33
$6\frac{1}{2}$	32
$6\frac{3}{4}$ and $6\frac{5}{8}$	31
$6\frac{1}{2}$ and $6\frac{3}{4}$	30
$6\frac{1}{4}$ and $6\frac{7}{8}$	29
$6\frac{1}{8}$ and 7	28
$7\frac{1}{8}$ and $7\frac{1}{4}$	27
$7\frac{1}{4}$ to $7\frac{5}{8}$	26
$7\frac{1}{8}$ to $7\frac{3}{8}$	26
$7\frac{1}{4}$ to $7\frac{1}{2}$	25

For rounds in coils, see our Shape Book.

Maximum Length of Squares

Size, Inches	Length, Feet
$\frac{1}{4}$ to $1\frac{1}{4}$	40
$\frac{3}{4}$ to 2	60
$2\frac{1}{8}$ to $4\frac{1}{4}$	48
5	45

Longer lengths can be rolled only by special arrangement.

Weights and Areas

Square and Round Bars and Circumferences of Round Bars

One Cubic Foot of Steel Weighing 489.6 lbs.

Side or Diameter, Inches	Weight of □ Bar per Foot	Weight of ○ Bar per Foot	Area of □ Bar Square Inches	Area of ○ Bar Square Inches	Circumference of ○ Bar Inches
$\frac{1}{16}$.013	.010	.0039	.0031	.1964
$\frac{5}{64}$.021	.016	.0061	.0048	.2454
$\frac{3}{32}$.030	.023	.0088	.0069	.2945
$\frac{7}{64}$.041	.032	.0120	.0094	.3436
$\frac{1}{8}$.053	.042	.0156	.0123	.3927
$\frac{9}{64}$.067	.053	.0198	.0155	.4418
$\frac{5}{32}$.083	.065	.0244	.0192	.4908
$\frac{11}{64}$.100	.079	.0295	.0232	.5400
$\frac{3}{16}$.120	.094	.0352	.0276	.5891
$\frac{13}{64}$.140	.110	.0413	.0324	.6381
$\frac{7}{32}$.163	.128	.0479	.0376	.6872
$\frac{15}{64}$.187	.147	.0549	.0431	.7363
$\frac{1}{4}$.212	.167	.0625	.0491	.7854
$\frac{17}{64}$.240	.188	.0706	.0554	.8345
$\frac{9}{32}$.269	.211	.0791	.0621	.8836
$\frac{19}{64}$.300	.235	.0881	.0692	.9327
$\frac{5}{16}$.332	.261	.0977	.0767	.9818
$\frac{21}{64}$.366	.288	.1077	.0846	1.0308
$\frac{11}{32}$.402	.316	.1182	.0928	1.0799
$\frac{23}{64}$.439	.345	.1292	.1014	1.1290
$\frac{3}{8}$.478	.376	.1406	.1104	1.1781
$\frac{25}{64}$.519	.407	.1526	.1198	1.2272
$\frac{13}{32}$.561	.441	.1650	.1296	1.2763
$\frac{27}{64}$.605	.475	.1780	.1398	1.3254
$\frac{7}{16}$.651	.511	.1914	.1503	1.3745
$\frac{29}{64}$.698	.548	.2053	.1613	1.4235
$\frac{15}{32}$.747	.587	.2197	.1726	1.4726
$\frac{31}{64}$.798	.627	.2346	.1843	1.5217
$\frac{1}{2}$.850	.668	.2500	.1963	1.5708
$\frac{33}{64}$.904	.710	.2659	.2088	1.6199
$\frac{17}{32}$.960	.754	.2822	.2217	1.6690
$\frac{35}{64}$	1.017	.799	.2991	.2349	1.7181
$\frac{9}{16}$	1.076	.845	.3164	.2485	1.7671

Weights and Areas

Square and Round Bars and Circumferences of Round Bars

Continued

Side or Diameter, Inches	Weight of □ Bar per Foot	Weight of ○ Bar per Foot	Area of □ Bar Square Inches	Area of ○ Bar Square Inches	Circumference of ○ Bar Inches
$\frac{37}{64}$	1.136	.893	.3342	.2625	1.8162
$\frac{19}{32}$	1.199	.941	.3525	.2769	1.8653
$\frac{33}{64}$	1.263	.992	.3713	.2916	1.9144
$\frac{34}{64}$	1.328	1.043	.3906	.3068	1.9635
$\frac{5}{8}$					
$\frac{41}{64}$	1.395	1.096	.4104	.3223	2.0126
$\frac{42}{64}$	1.464	1.150	.4307	.3382	2.0617
$\frac{43}{64}$	1.535	1.205	.4514	.3545	2.1108
$\frac{44}{64}$	1.607	1.262	.4727	.3712	2.1598
$\frac{11}{16}$					
$\frac{45}{64}$	1.681	1.320	.4944	.3883	2.2089
$\frac{46}{64}$	1.756	1.379	.5166	.4057	2.2580
$\frac{47}{64}$	1.834	1.440	.5393	.4236	2.3071
$\frac{48}{64}$	1.913	1.502	.5625	.4418	2.3562
$\frac{3}{4}$					
$\frac{49}{64}$	1.993	1.565	.5862	.4604	2.4053
$\frac{50}{64}$	2.075	1.630	.6103	.4794	2.4544
$\frac{51}{64}$	2.159	1.696	.6350	.4987	2.5035
$\frac{52}{64}$	2.245	1.763	.6602	.5185	2.5525
$\frac{13}{16}$					
$\frac{53}{64}$	2.332	1.831	.6858	.5386	2.6016
$\frac{54}{64}$	2.420	1.901	.7119	.5591	2.6507
$\frac{55}{64}$	2.511	1.972	.7385	.5800	2.6998
$\frac{56}{64}$	2.603	2.044	.7656	.6013	2.7489
$\frac{7}{8}$					
$\frac{57}{64}$	2.697	2.118	.7932	.6230	2.7980
$\frac{58}{64}$	2.792	2.193	.8213	.6450	2.8471
$\frac{59}{64}$	2.889	2.270	.8498	.6675	2.8962
$\frac{60}{64}$	2.988	2.347	.8789	.6903	2.9453
$\frac{15}{16}$					
$\frac{61}{64}$	3.089	2.426	.9084	.7135	2.9943
$\frac{62}{64}$	3.191	2.506	.9385	.7371	3.0434
$\frac{63}{64}$	3.294	2.587	.9689	.7610	3.0925
$\frac{64}{64}$	3.400	2.670	1.0000	.7854	3.1416
1					
$\frac{1}{32}$	3.616	2.840	1.0635	.8353	3.2398
$\frac{1}{8}$	3.838	3.014	1.1289	.8866	3.3379
$\frac{3}{8}$	4.067	3.194	1.1963	.9396	3.4361
$\frac{1}{2}$	4.303	3.379	1.2656	.9940	3.5343

Weights and Areas

Square and Round Bars and Circumferences of Round Bars

Continued

Side or Diameter, Inches	Weight of \square Bar per Foot	Weight of \circ Bar per Foot	Area of \square Bar Square Inches	Area of \circ Bar Square Inches	Circumference of \circ Bar Inches
$1\frac{5}{16}$	4.545	3.570	1.3369	1.0500	3.6325
$\frac{3}{8}$	4.795	3.766	1.4102	1.1075	3.7306
$\frac{7}{16}$	5.050	3.966	1.4853	1.1666	3.8288
$\frac{1}{4}$	5.312	4.173	1.5625	1.2272	3.9270
$\frac{9}{16}$	5.581	4.384	1.6416	1.2893	4.0252
$\frac{5}{8}$	5.857	4.600	1.7227	1.3530	4.1233
$\frac{11}{16}$	6.139	4.822	1.8056	1.4182	4.2215
$\frac{3}{4}$	6.428	5.049	1.8906	1.4849	4.3197
$\frac{13}{16}$	6.724	5.281	1.9775	1.5532	4.4179
$\frac{7}{8}$	7.026	5.518	2.0664	1.6230	4.5160
$\frac{15}{16}$	7.334	5.761	2.1572	1.6943	4.6142
$1\frac{1}{2}$	7.650	6.008	2.2500	1.7671	4.7124
$\frac{17}{16}$	7.972	6.261	2.3447	1.8415	4.8106
$\frac{9}{8}$	8.301	6.520	2.4414	1.9175	4.9087
$\frac{19}{16}$	8.636	6.783	2.5400	1.9949	5.0069
$\frac{5}{8}$	8.978	7.051	2.6406	2.0739	5.1051
$2\frac{1}{16}$	9.327	7.325	2.7431	2.1545	5.2033
$\frac{11}{8}$	9.682	7.604	2.8477	2.2365	5.3014
$\frac{23}{16}$	10.05	7.889	2.9541	2.3202	5.3996
$\frac{3}{4}$	10.41	8.178	3.0625	2.4053	5.4978
$2\frac{5}{16}$	10.79	8.473	3.1728	2.4920	5.5960
$\frac{13}{8}$	11.17	8.773	3.2852	2.5802	5.6941
$\frac{27}{16}$	11.56	9.078	3.3994	2.6699	5.7923
$\frac{7}{8}$	11.95	9.388	3.5156	2.7612	5.8905
$2\frac{9}{16}$	12.36	9.704	3.6337	2.8540	5.9887
$\frac{29}{16}$	12.76	10.02	3.7539	2.9483	6.0868
$\frac{31}{16}$	13.18	10.35	3.8760	3.0442	6.1850
3	13.60	10.68	4.0000	3.1416	6.2832
$1\frac{1}{8}$	14.46	11.36	4.2539	3.3410	6.4795
$\frac{1}{8}$	15.35	12.06	4.5156	3.5466	6.6759
$\frac{13}{8}$	16.27	12.78	4.7852	3.7583	6.8722
$\frac{1}{4}$	17.22	13.52	5.0625	3.9761	7.0686

Weights and Areas

Square and Round Bars and Circumferences of Round Bars

Continued

Side or Diameter, Inches	Weight of \square Bar per Foot	Weight of \bigcirc Bar per Foot	Area of \square Bar Square Inches	Area of \bigcirc Bar Square Inches	Circumference of \bigcirc Bar Inches
$2\frac{1}{16}$	18.19	14.28	5.3477	4.2000	7.2649
$\frac{3}{8}$	19.18	15.07	5.6406	4.4301	7.4613
$\frac{7}{16}$	20.20	15.86	5.9414	4.6664	7.6576
$\frac{1}{2}$	21.25	16.69	6.2500	4.9087	7.8540
$\frac{9}{16}$	22.33	17.53	6.5664	5.1572	8.0503
$\frac{5}{8}$	23.43	18.40	6.8906	5.4119	8.2467
$\frac{11}{16}$	24.56	19.29	7.2227	5.6727	8.4430
$\frac{3}{4}$	25.71	20.20	7.5625	5.9396	8.6394
$\frac{13}{16}$	26.90	21.12	7.9102	6.2126	8.8357
$\frac{7}{8}$	28.10	22.07	8.2656	6.4918	9.0321
$\frac{15}{16}$	29.34	23.04	8.6289	6.7771	9.2284
3	30.60	24.03	9.0000	7.0686	9.4248
$\frac{1}{16}$	31.89	25.04	9.3789	7.3662	9.6211
$\frac{1}{8}$	33.20	26.08	9.7656	7.6699	9.8175
$\frac{3}{16}$	34.55	27.13	10.160	7.9798	10.014
$\frac{1}{4}$	35.92	28.20	10.563	8.2958	10.210
$\frac{5}{16}$	37.31	29.30	10.973	8.6179	10.407
$\frac{3}{8}$	38.73	30.42	11.391	8.9462	10.603
$\frac{7}{16}$	40.18	31.56	11.816	9.2806	10.799
$\frac{1}{2}$	41.65	32.71	12.250	9.6211	10.996
$\frac{9}{16}$	43.14	33.90	12.691	9.9678	11.192
$\frac{5}{8}$	44.68	35.09	13.141	10.321	11.388
$\frac{11}{16}$	46.24	36.31	13.598	10.680	11.585
$\frac{3}{4}$	47.82	37.56	14.063	11.045	11.781
$\frac{13}{16}$	49.42	38.81	14.535	11.416	11.977
$\frac{7}{8}$	51.05	40.10	15.016	11.793	12.174
$\frac{15}{16}$	52.71	41.40	15.504	12.177	12.370
4	54.40	42.73	16.000	12.566	12.566
$\frac{1}{16}$	56.11	44.07	16.504	12.962	12.763
$\frac{1}{8}$	57.85	45.44	17.016	13.364	12.959
$\frac{3}{16}$	59.62	46.83	17.535	13.772	13.155
$\frac{1}{4}$	61.41	48.24	18.063	14.186	13.352

Weights and Areas

Square and Round Bars and Circumferences of Round Bars

Continued

Side or Diameter, Inches	Weight of \square Bar per Foot	Weight of \circ Bar per Foot	Area of \square Bar Square Inches	Area of \circ Bar Square Inches	Circumference of \circ Bar Inches
$4\frac{5}{16}$	63.23	49.66	18.598	14.607	13.548
$4\frac{3}{8}$	65.08	51.11	19.141	15.033	13.744
$4\frac{7}{16}$	66.95	52.58	19.691	15.466	13.941
$4\frac{1}{2}$	68.85	54.07	20.250	15.904	14.137
$4\frac{9}{16}$	70.78	55.59	20.816	16.349	14.334
$4\frac{5}{8}$	72.73	57.12	21.391	16.800	14.530
$4\frac{11}{16}$	74.70	58.67	21.973	17.257	14.726
$4\frac{3}{4}$	76.71	60.25	22.563	17.721	14.923
$4\frac{13}{16}$	78.74	61.84	23.160	18.190	15.119
$4\frac{7}{8}$	80.81	63.46	23.766	18.665	15.315
$4\frac{15}{16}$	82.89	65.10	24.379	19.147	15.512
5	85.00	66.76	25.000	19.635	15.708
$5\frac{1}{16}$	87.14	68.44	25.629	20.129	15.904
$5\frac{1}{8}$	89.30	70.14	26.266	20.629	16.101
$5\frac{3}{16}$	91.49	71.86	26.910	21.135	16.297
$5\frac{1}{4}$	93.72	73.60	27.563	21.648	16.493
$5\frac{5}{16}$	95.96	75.37	28.223	22.166	16.690
$5\frac{3}{8}$	98.23	77.15	28.891	22.691	16.886
$5\frac{7}{16}$	100.5	78.93	29.566	23.221	17.082
$5\frac{1}{2}$	102.8	80.77	30.250	23.758	17.279
$5\frac{9}{16}$	105.2	82.62	30.941	24.301	17.475
$5\frac{5}{8}$	107.6	84.49	31.641	24.850	17.671
$5\frac{11}{16}$	110.0	86.38	32.348	25.406	17.868
$5\frac{3}{4}$	112.4	88.29	33.063	25.967	18.064
$5\frac{13}{16}$	114.9	90.22	33.785	26.535	18.261
$5\frac{7}{8}$	117.4	92.17	34.516	27.109	18.457
$5\frac{15}{16}$	119.9	94.14	35.254	27.688	18.653
6	122.4	96.14	36.000	28.274	18.850
$6\frac{1}{16}$	125.0	98.14	36.754	28.866	19.046
$6\frac{1}{8}$	127.6	100.2	37.516	29.465	19.242
$6\frac{3}{16}$	130.2	102.2	38.285	30.069	19.439
$6\frac{1}{4}$	132.8	104.3	39.063	30.680	19.635

Weights and Areas

Square and Round Bars and Circumferences of Round Bars

Continued

Side or Diameter, Inches	Weight of \square Bar per Foot	Weight of \circ Bar per Foot	Area of \square Bar Square Inches	Area of \circ Bar Square Inches	Circumference of \circ Bar Inches
$6\frac{5}{16}$	135.5	106.4	39.848	31.296	19.831
$\frac{3}{8}$	138.2	108.5	40.641	31.919	20.028
$\frac{7}{16}$	140.9	110.7	41.441	32.548	20.224
$\frac{1}{2}$	143.6	112.8	42.250	33.183	20.420
$\frac{9}{16}$	146.5	114.9	43.066	33.824	20.617
$\frac{5}{8}$	149.2	117.2	43.891	34.472	20.813
$\frac{11}{16}$	152.1	119.4	44.723	35.125	21.009
$\frac{3}{4}$	154.9	121.7	45.563	35.785	21.206
$\frac{13}{16}$	157.8	123.9	46.410	36.450	21.402
$\frac{7}{8}$	160.8	126.2	47.266	37.122	21.598
$\frac{15}{16}$	163.6	128.5	48.129	37.800	21.795
7	166.6	130.9	49.000	38.485	21.991
$\frac{1}{16}$	169.6	133.2	49.879	39.175	22.187
$\frac{1}{8}$	172.6	135.6	50.766	39.871	22.384
$\frac{3}{16}$	175.6	137.9	51.660	40.574	22.580
$\frac{1}{4}$	178.7	140.4	52.563	41.282	22.777
$\frac{5}{16}$	181.8	142.8	53.473	41.997	22.973
$\frac{3}{8}$	184.9	145.3	54.391	42.718	23.169
$\frac{7}{16}$	188.1	147.7	55.316	43.445	23.366
$\frac{1}{2}$	191.3	150.2	56.250	44.179	23.562
$\frac{9}{16}$	194.4	152.7	57.191	44.918	23.758
$\frac{5}{8}$	197.7	155.2	58.141	45.664	23.955
$\frac{11}{16}$	200.9	157.8	59.098	46.415	24.151
$\frac{3}{4}$	204.2	160.3	60.063	47.173	24.347
$\frac{13}{16}$	207.6	163.0	61.035	47.937	24.544
$\frac{7}{8}$	210.8	165.6	62.016	48.707	24.740
$\frac{15}{16}$	214.2	168.2	63.004	49.483	24.936
8	217.6	171.0	64.000	50.265	25.133

Areas of Bars and Plates Square Inches

Width, Inches		Thickness, Inches															
		$\frac{1}{16}$	$\frac{1}{8}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{11}{16}$	$\frac{3}{4}$	$\frac{7}{8}$	$\frac{15}{16}$	1	
$\frac{1}{2}$.031	.063	.094	.125	.156	.188	.219	.25	.28	.31	.34	.38	.41	.44	.47	.50
1		.063	.125	.188	.250	.313	.375	.438	.50	.56	.63	.69	.75	.81	.88	.94	1.00
2		.125	.250	.375	.500	.625	.750	.875	1.00	1.13	1.25	1.38	1.50	1.63	1.75	1.88	2.00
3		.188	.375	.563	.750	.938	1.125	1.313	1.50	1.69	1.88	2.06	2.25	2.44	2.63	2.81	3.00
4		.250	.500	.750	1.000	1.250	1.500	1.750	2.00	2.25	2.50	2.75	3.00	3.25	3.50	3.75	4.00
5		.313	.625	.938	1.250	1.563	1.875	2.188	2.50	2.81	3.13	3.44	3.75	4.06	4.38	4.69	5.00
6		.375	.750	1.125	1.500	1.875	2.250	2.625	3.00	3.38	3.75	4.13	4.50	4.88	5.25	5.63	6.00
7		.438	.875	1.313	1.750	2.188	2.625	3.063	3.50	3.94	4.38	4.81	5.25	5.69	6.13	6.56	7.00
8		.500	1.000	1.500	2.000	2.500	3.000	3.500	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50	8.00
9		.563	1.125	1.688	2.250	2.813	3.375	3.938	4.50	5.06	5.63	6.19	6.75	7.31	7.88	8.44	9.00
10		.625	1.250	1.875	2.50	3.13	3.75	4.38	5.00	5.63	6.25	6.88	7.50	8.13	8.75	9.38	10.00
11		.688	1.375	2.063	2.75	3.44	4.13	4.81	5.50	6.19	6.88	7.56	8.25	8.94	9.63	10.31	11.00
12		.750	1.500	2.250	3.00	3.75	4.50	5.25	6.00	6.75	7.50	8.25	9.00	9.75	10.50	11.25	12.00
13		.813	1.625	2.438	3.25	4.06	4.88	5.69	6.50	7.31	8.13	8.94	9.75	10.56	11.38	12.19	13.00
14		.875	1.750	2.625	3.50	4.38	5.25	6.13	7.00	7.88	8.75	9.63	10.50	11.38	12.25	13.13	14.00
15		.938	1.875	2.813	3.75	4.69	5.63	6.56	7.50	8.44	9.38	10.31	11.25	12.19	13.13	14.06	15.00
16		1.000	2.000	3.000	4.00	5.00	6.00	7.00	8.00	9.00	10.00	11.00	12.00	13.00	14.00	15.00	16.00
17		1.063	2.125	3.188	4.25	5.31	6.38	7.44	8.50	9.56	10.63	11.69	12.75	13.81	14.88	15.94	17.00
18		1.125	2.250	3.375	4.50	5.63	6.75	7.88	9.00	10.13	11.25	12.38	13.50	14.63	15.75	16.88	18.00
19		1.188	2.375	3.563	4.75	5.94	7.13	8.31	9.50	10.69	11.88	13.06	14.25	15.44	16.63	17.81	19.00
20		1.250	2.500	3.750	5.00	6.25	7.50	8.75	10.00	11.25	12.50	13.75	15.00	16.25	17.50	18.75	20.00
21		1.313	2.625	3.938	5.25	6.56	7.88	9.19	10.50	11.81	13.14	14.45	15.75	17.06	18.38	19.69	21.00
22		1.375	2.750	4.125	5.50	6.88	8.25	9.63	11.00	12.38	13.75	15.13	16.50	17.88	19.25	20.63	22.00
23		1.438	2.875	4.313	5.75	7.19	8.63	10.06	11.50	12.94	14.38	15.81	17.25	18.69	20.13	21.56	23.00
24		1.500	3.000	4.500	6.00	7.50	9.00	10.50	12.00	13.50	15.00	16.50	18.00	19.50	21.00	22.50	24.00

Weights and Areas

Square and Round Bars and Circumferences of Round Bars

Continued

Side or Diameter, Inches	Weight of \square Bar per Foot	Weight of \circ Bar per Foot	Area of \square Bar Square Inches	Area of \circ Bar Square Inches	Circumference of \circ Bar Inches
$6\frac{5}{16}$	135.5	106.4	39.848	31.296	19.831
$\frac{3}{8}$	138.2	108.5	40.641	31.919	20.028
$\frac{7}{16}$	140.9	110.7	41.441	32.548	20.224
$\frac{1}{2}$	143.6	112.8	42.250	33.183	20.420
$\frac{9}{16}$	146.5	114.9	43.066	33.824	20.617
$\frac{5}{8}$	149.2	117.2	43.891	34.472	20.813
$\frac{11}{16}$	152.1	119.4	44.723	35.125	21.009
$\frac{3}{4}$	154.9	121.7	45.563	35.785	21.206
$\frac{13}{16}$	157.8	123.9	46.410	36.450	21.402
$\frac{7}{8}$	160.8	126.2	47.266	37.122	21.598
$\frac{15}{16}$	163.6	128.5	48.129	37.800	21.795
7	166.6	130.9	49.000	38.485	21.991
$\frac{1}{8}$	169.6	133.2	49.879	39.175	22.187
$\frac{1}{8}$	172.6	135.6	50.766	39.871	22.384
$\frac{3}{16}$	175.6	137.9	51.660	40.574	22.580
$\frac{1}{4}$	178.7	140.4	52.563	41.282	22.777
$\frac{5}{16}$	181.8	142.8	53.473	41.997	22.973
$\frac{3}{8}$	184.9	145.3	54.391	42.718	23.169
$\frac{7}{16}$	188.1	147.7	55.316	43.445	23.366
$\frac{1}{2}$	191.3	150.2	56.250	44.179	23.562
$\frac{9}{16}$	194.4	152.7	57.191	44.918	23.758
$\frac{5}{8}$	197.7	155.2	58.141	45.664	23.955
$\frac{11}{16}$	200.9	157.8	59.098	46.415	24.151
$\frac{3}{4}$	204.2	160.3	60.063	47.173	24.347
$\frac{13}{16}$	207.6	163.0	61.035	47.937	24.544
$\frac{7}{8}$	210.8	165.6	62.016	48.707	24.740
$\frac{15}{16}$	214.2	168.2	63.004	49.483	24.936
8	217.6	171.0	64.000	50.265	25.133

Areas of Bars and Plates
Square Inches

Width, Inches	THICKNESS, INCHES													
	$\frac{1}{16}$	$\frac{1}{8}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$	$1\frac{1}{8}$	$1\frac{1}{4}$	1
$\frac{1}{2}$.031	.063	.094	.125	.156	.188	.219	.25	.28	.31	.34	.38	.41	.44
1	.063	.125	.188	.250	.313	.375	.438	.50	.56	.63	.69	.75	.81	.88
2	.125	.250	.375	.500	.625	.750	.875	1.00	1.13	1.25	1.38	1.50	1.63	1.75
3	.188	.375	.563	.750	.938	1.125	1.313	1.50	1.69	1.88	2.06	2.25	2.44	2.63
4	.250	.500	.750	1.000	1.250	1.500	1.750	2.00	2.25	2.50	2.75	3.00	3.25	3.50
5	.313	.625	.938	1.250	1.563	1.875	2.188	2.50	2.81	3.13	3.44	3.75	4.06	4.38
6	.375	.750	1.125	1.500	1.875	2.250	2.625	3.00	3.38	3.75	4.13	4.50	4.88	5.25
7	.438	.875	1.313	1.750	2.188	2.625	3.063	3.50	3.94	4.38	4.81	5.25	5.69	6.13
8	.500	1.000	1.500	2.000	2.500	3.000	3.500	4.00	4.50	5.00	5.50	6.00	6.50	7.00
9	.563	1.125	1.688	2.250	2.813	3.375	3.938	4.50	5.06	5.63	6.19	6.75	7.31	7.88
10	.625	1.250	1.875	2.50	3.13	3.75	4.38	5.00	5.63	6.25	6.88	7.50	8.13	8.75
11	.688	1.375	2.063	2.75	3.44	4.13	4.81	5.50	6.19	6.88	7.56	8.25	8.94	9.63
12	.750	1.500	2.250	3.00	3.75	4.50	5.25	6.00	6.75	7.50	8.25	9.00	9.75	10.50
13	.813	1.625	2.438	3.25	4.06	4.88	5.69	6.50	7.31	8.13	8.94	9.75	10.56	11.38
14	.875	1.750	2.625	3.50	4.38	5.25	6.13	7.00	7.88	8.75	9.63	10.50	11.38	12.25
15	.938	1.875	2.813	3.75	4.69	5.63	6.56	7.50	8.44	9.38	10.31	11.25	12.19	13.14
16	1.000	2.000	3.000	4.00	5.00	6.00	7.00	8.00	9.00	10.00	11.00	12.00	13.00	14.00
17	1.063	2.125	3.188	4.25	5.31	6.38	7.44	8.50	9.56	10.63	11.69	12.75	13.81	14.88
18	1.125	2.250	3.375	4.50	5.63	6.75	7.88	9.00	10.13	11.25	12.38	13.50	14.63	15.75
19	1.188	2.375	3.563	4.75	5.94	7.13	8.31	9.50	10.69	11.88	13.06	14.25	15.44	16.63
20	1.250	2.500	3.750	5.00	6.25	7.50	8.75	10.00	11.25	12.50	13.75	15.00	16.25	17.50
21	1.313	2.625	3.938	5.25	6.56	7.88	9.19	10.50	11.81	13.14	14.44	15.75	17.06	18.38
22	1.375	2.750	4.125	5.50	6.88	8.25	9.63	11.00	12.38	13.75	15.13	16.50	17.88	19.25
23	1.438	2.875	4.313	5.75	7.19	8.63	10.06	11.50	12.94	14.38	15.81	17.25	18.69	20.13
24	1.500	3.000	4.500	6.00	7.50	9.00	10.50	12.00	13.50	15.00	16.50	18.00	19.50	21.00

Areas of Bars and Plates Square Inches Continued

Width, Inches	THICKNESS, INCHES													
	$\frac{1}{16}$	$\frac{1}{8}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{11}{16}$	$\frac{3}{4}$	$\frac{13}{16}$	1
25	1.563	3.125	4.688	6.25	7.81	9.38	10.94	12.50	14.06	15.63	17.19	18.75	20.31	21.88
26	1.625	3.250	4.875	6.50	8.13	9.75	11.38	13.00	14.63	16.25	17.88	19.50	21.13	22.75
27	1.688	3.375	5.063	6.75	8.44	10.13	11.81	13.50	15.16	16.88	18.56	20.25	21.94	23.63
28	1.750	3.500	5.250	7.00	8.75	10.50	12.25	14.00	15.75	17.50	19.25	21.00	22.75	24.50
29	1.813	3.625	5.438	7.25	9.06	10.88	12.69	14.50	16.31	18.13	19.94	21.75	23.56	25.38
30	1.875	3.750	5.625	7.50	9.38	11.25	13.13	15.00	16.88	18.75	20.63	22.50	24.38	26.25
31	1.938	3.875	5.813	7.75	9.69	11.63	13.56	15.50	17.44	19.38	21.31	23.25	25.19	27.13
32	2.000	4.000	6.000	8.00	10.00	12.00	14.00	16.00	18.00	20.00	22.00	24.00	26.00	28.00
33	2.063	4.125	6.188	8.25	10.31	12.38	14.44	16.50	18.56	20.63	22.69	24.75	26.81	28.88
34	2.125	4.250	6.375	8.50	10.63	12.75	14.88	17.00	19.13	21.25	23.38	25.50	27.63	29.75
35	2.188	4.375	6.563	8.75	10.94	13.13	15.31	17.50	19.69	21.88	24.06	26.25	28.44	30.63
36	2.250	4.500	6.750	9.00	11.25	13.50	15.75	18.00	20.25	22.50	24.75	27.00	29.25	31.50
37	2.313	4.625	6.938	9.25	11.56	13.88	16.19	18.50	20.81	23.13	25.44	27.75	30.06	32.38
38	2.375	4.750	7.125	9.50	11.88	14.25	16.63	19.00	21.38	23.75	26.13	28.50	30.88	33.25
39	2.438	4.875	7.313	9.75	12.19	14.63	17.06	19.50	21.94	24.38	26.81	29.25	31.69	34.13
40	2.500	5.000	7.500	10.00	12.50	15.00	17.50	20.00	22.50	25.00	27.50	30.00	32.50	35.00
41	2.563	5.125	7.688	10.25	12.81	15.38	17.94	20.50	23.06	25.63	28.19	30.75	33.31	35.88
42	2.625	5.250	7.875	10.50	13.13	15.75	18.38	21.00	23.63	26.25	28.83	31.41	34.00	36.58
43	2.688	5.375	8.063	10.75	13.44	16.13	18.81	21.50	24.19	26.88	29.56	32.25	34.94	37.63
44	2.750	5.500	8.250	11.00	13.75	16.50	19.25	22.00	24.75	27.50	30.25	33.00	35.75	38.50
45	2.813	5.625	8.438	11.25	14.06	16.88	19.69	22.50	25.31	28.13	31.00	33.83	36.69	39.44
46	2.875	5.750	8.625	11.50	14.38	17.25	20.13	23.00	25.88	28.75	31.63	34.50	37.38	40.44
47	2.938	5.875	8.813	11.75	14.69	17.63	20.56	23.50	26.44	29.38	32.31	35.25	38.19	41.44
48	3.000	6.000	9.000	12.00	15.00	18.00	21.00	24.00	27.00	30.00	33.00	36.00	39.00	42.00

Weights of Flat Rolled Steel

Per Lineal Foot

Thick- ness, Inches	WIDTH, INCHES							
	$\frac{1}{32}$	$\frac{1}{16}$	$\frac{3}{32}$	$\frac{1}{8}$	$\frac{5}{32}$	$\frac{3}{16}$	$\frac{7}{32}$	1
$\frac{1}{16}$.007	.013	.020	.027	.033	.040	.046	.213
$\frac{5}{64}$.008	.017	.025	.033	.042	.050	.058	.266
$\frac{3}{32}$.010	.020	.030	.040	.050	.060	.070	.319
$\frac{7}{64}$.012	.023	.035	.046	.058	.070	.081	.372
$\frac{1}{8}$.013	.027	.040	.053	.066	.080	.093	.425
$\frac{9}{64}$.015	.030	.045	.060	.075	.090	.105	.478
$\frac{5}{32}$.017	.033	.050	.066	.083	.100	.116	.531
$\frac{3}{16}$.018	.037	.055	.073	.091	.110	.128	.584
$\frac{2}{16}$.020	.040	.060	.080	.100	.120	.139	.638
$\frac{13}{64}$.022	.043	.065	.086	.108	.130	.151	.691
$\frac{7}{32}$.023	.046	.070	.093	.116	.140	.163	.744
$\frac{15}{64}$.025	.050	.075	.100	.125	.149	.174	.797
$\frac{1}{4}$.027	.053	.080	.106	.133	.159	.186	.850
$\frac{17}{64}$.028	.056	.085	.113	.141	.169	.198	.903
$\frac{9}{32}$.030	.060	.090	.120	.149	.179	.209	.956
$\frac{19}{64}$.032	.063	.095	.126	.158	.189	.221	1.01
$\frac{5}{16}$.033	.067	.100	.133	.166	.199	.232	1.06
$\frac{21}{64}$.035	.070	.105	.139	.174	.209	.244	1.12
$\frac{11}{32}$.037	.073	.110	.146	.182	.219	.256	1.17
$\frac{23}{64}$.038	.076	.115	.153	.191	.229	.267	1.22
$\frac{3}{8}$.040	.080	.120	.160	.200	.239	.279	1.28
$\frac{25}{64}$.042	.083	.125	.166	.208	.249	.291	1.33
$\frac{13}{32}$.043	.086	.129	.172	.216	.259	.302	1.38
$\frac{27}{64}$.045	.090	.134	.179	.224	.269	.314	1.43
$\frac{7}{16}$.046	.093	.139	.186	.232	.279	.325	1.49
$\frac{29}{64}$.048	.096	.144	.193	.241	.289	.337	1.54
$\frac{15}{32}$.050	.100	.149	.200	.249	.299	.349	1.59
$\frac{31}{64}$.051	.103	.154	.206	.257	.309	.360	1.65
$\frac{1}{2}$.053	.106	.159	.213	.266	.319	.372	1.70
$\frac{33}{64}$.055	.110	.164	.219	.274	.329	.383	1.75
$\frac{17}{32}$.056	.113	.169	.226	.282	.339	.395	1.81
$\frac{35}{64}$.058	.116	.174	.232	.290	.349	.407	1.86
$\frac{19}{32}$.060	.120	.179	.239	.299	.359	.418	1.91

Weights of Flat Rolled Steel

Per Lineal Foot

Continued

Thickness, Inches	Width, Inches								
	$\frac{3}{32}$	$\frac{5}{16}$	$\frac{11}{32}$	$\frac{3}{8}$	$\frac{13}{32}$	$\frac{7}{16}$	$\frac{15}{32}$	$\frac{1}{2}$	1
$\frac{1}{16}$.060	.066	.073	.080	.086	.093	.100	.106	.213
$\frac{5}{64}$.075	.083	.091	.100	.108	.116	.125	.133	.266
$\frac{3}{32}$.090	.100	.110	.120	.129	.139	.149	.159	.319
$\frac{7}{64}$.105	.116	.128	.139	.151	.163	.174	.186	.372
$\frac{1}{8}$.120	.133	.146	.159	.173	.186	.199	.212	.425
$\frac{9}{64}$.134	.149	.164	.179	.194	.209	.224	.239	.478
$\frac{5}{32}$.149	.166	.183	.199	.216	.232	.249	.266	.531
$\frac{11}{64}$.164	.183	.201	.219	.237	.256	.274	.292	.584
$\frac{3}{16}$.179	.199	.219	.239	.259	.279	.299	.319	.638
$\frac{13}{64}$.194	.216	.237	.259	.281	.302	.324	.345	.691
$\frac{7}{32}$.209	.232	.256	.279	.302	.325	.349	.372	.744
$\frac{15}{64}$.224	.249	.274	.299	.324	.349	.374	.398	.797
$\frac{1}{4}$.239	.266	.292	.319	.345	.372	.398	.425	.850
$\frac{17}{64}$.254	.282	.310	.339	.367	.395	.423	.452	.903
$\frac{9}{32}$.269	.299	.329	.359	.388	.418	.448	.478	.956
$\frac{19}{64}$.284	.315	.347	.379	.410	.442	.473	.505	1.01
$\frac{5}{16}$.299	.332	.365	.398	.432	.465	.498	.531	1.06
$\frac{21}{64}$.314	.349	.383	.418	.453	.488	.523	.558	1.12
$\frac{11}{32}$.329	.365	.402	.438	.475	.511	.548	.584	1.17
$\frac{23}{64}$.344	.382	.420	.458	.496	.535	.573	.611	1.22
$\frac{3}{8}$.359	.398	.438	.478	.518	.558	.598	.638	1.28
$\frac{25}{64}$.374	.415	.457	.498	.540	.581	.623	.664	1.33
$\frac{13}{32}$.388	.432	.475	.518	.561	.604	.647	.691	1.38
$\frac{27}{64}$.403	.448	.493	.538	.583	.628	.672	.717	1.43
$\frac{7}{16}$.418	.465	.511	.558	.604	.651	.697	.744	1.49
$\frac{29}{64}$.433	.481	.530	.578	.626	.674	.722	.770	1.54
$\frac{15}{32}$.448	.498	.548	.598	.647	.697	.747	.797	1.59
$\frac{31}{64}$.463	.515	.566	.618	.669	.721	.772	.823	1.65
$\frac{1}{2}$.478	.531	.584	.638	.691	.744	.797	.850	1.70
$\frac{33}{64}$.493	.548	.603	.657	.712	.767	.822	.877	1.75
$\frac{17}{32}$.508	.564	.621	.677	.734	.790	.847	.903	1.81
$\frac{35}{64}$.523	.581	.639	.697	.755	.813	.872	.930	1.86
$\frac{7}{8}$.538	.598	.657	.717	.777	.837	.896	.956	1.91

Weights of Flat Rolled Steel

Per Lineal Foot

Continued

Thick- ness, Inches	WIDTH, INCHES							
	$\frac{1}{16}$	$\frac{7}{8}$	$\frac{15}{16}$	1	$1\frac{1}{8}$	$1\frac{1}{4}$	$1\frac{3}{8}$	$1\frac{1}{2}$
$\frac{1}{16}$.173	.186	.199	.213	.239	.266	.292	.319
$\frac{9}{64}$.216	.232	.249	.266	.299	.332	.365	.398
$\frac{3}{32}$.259	.279	.299	.319	.358	.398	.438	.478
$\frac{7}{64}$.302	.325	.349	.372	.418	.465	.511	.558
$\frac{1}{8}$.345	.372	.399	.425	.478	.531	.584	.638
$\frac{9}{64}$.388	.418	.448	.478	.538	.598	.657	.717
$\frac{5}{32}$.432	.465	.498	.531	.598	.664	.730	.797
$\frac{11}{64}$.475	.511	.548	.584	.657	.730	.803	.876
$\frac{3}{16}$.518	.558	.598	.638	.717	.797	.877	.956
$\frac{13}{64}$.561	.604	.647	.691	.777	.863	.950	1.04
$\frac{7}{32}$.604	.651	.697	.744	.837	.930	1.02	1.12
$\frac{15}{64}$.647	.697	.747	.797	.896	.996	1.10	1.20
$\frac{1}{4}$.691	.744	.797	.850	.956	1.06	1.17	1.28
$\frac{17}{64}$.734	.790	.847	.903	1.02	1.13	1.24	1.35
$\frac{9}{32}$.777	.837	.896	.956	1.08	1.20	1.31	1.43
$\frac{19}{64}$.820	.883	.946	1.01	1.14	1.26	1.39	1.51
$\frac{5}{16}$.863	.929	.996	1.06	1.20	1.33	1.46	1.59
$\frac{21}{64}$.906	.976	1.05	1.12	1.25	1.39	1.53	1.67
$\frac{11}{32}$.949	1.02	1.10	1.17	1.31	1.46	1.61	1.75
$\frac{23}{64}$.993	1.07	1.15	1.22	1.37	1.53	1.68	1.83
$\frac{3}{8}$	1.04	1.12	1.20	1.28	1.43	1.59	1.75	1.91
$\frac{25}{64}$	1.08	1.16	1.25	1.33	1.49	1.66	1.83	1.99
$\frac{13}{32}$	1.12	1.21	1.29	1.38	1.55	1.72	1.90	2.07
$\frac{27}{64}$	1.16	1.25	1.34	1.43	1.61	1.79	1.97	2.15
$\frac{7}{16}$	1.21	1.30	1.39	1.49	1.67	1.86	2.05	2.23
$\frac{29}{64}$	1.25	1.35	1.44	1.54	1.73	1.93	2.12	2.31
$\frac{15}{32}$	1.29	1.39	1.49	1.59	1.79	1.99	2.19	2.39
$\frac{31}{64}$	1.34	1.44	1.54	1.65	1.85	2.06	2.26	2.47
$\frac{1}{2}$	1.38	1.49	1.59	1.70	1.91	2.13	2.34	2.55
$\frac{33}{64}$	1.42	1.53	1.64	1.75	1.97	2.19	2.41	2.63
$\frac{17}{32}$	1.47	1.58	1.69	1.81	2.03	2.26	2.48	2.71
$\frac{35}{64}$	1.51	1.63	1.74	1.86	2.09	2.32	2.56	2.79
$\frac{19}{32}$	1.55	1.67	1.79	1.91	2.15	2.39	2.63	2.87

Weights of Flat Rolled Steel

Per Lineal Foot

Continued

Thick- ness, Inches	Width, Inches								
	3	3¼	3½	3¾	4	4¼	4½	4¾	12
$\frac{3}{16}$	1.91	2.07	2.23	2.39	2.55	2.71	2.87	3.03	7.65
$\frac{1}{4}$	2.55	2.76	2.98	3.19	3.40	3.61	3.83	4.04	10.20
$\frac{5}{16}$	3.19	3.45	3.72	3.99	4.25	4.52	4.78	5.05	12.75
$\frac{3}{8}$	3.83	4.15	4.47	4.78	5.10	5.42	5.74	6.06	15.30
$\frac{7}{16}$	4.46	4.83	5.20	5.58	5.95	6.32	6.70	7.07	17.85
$\frac{1}{2}$	5.10	5.53	5.95	6.38	6.80	7.22	7.65	8.08	20.40
$\frac{9}{16}$	5.74	6.22	6.70	7.17	7.65	8.13	8.61	9.09	22.95
$\frac{5}{8}$	6.38	6.91	7.44	7.97	8.50	9.03	9.57	10.10	25.50
$\frac{11}{16}$	7.02	7.60	8.18	8.76	9.35	9.93	10.52	11.11	28.05
$\frac{3}{4}$	7.65	8.29	8.93	9.57	10.20	10.84	11.48	12.12	30.60
$\frac{13}{16}$	8.29	8.98	9.67	10.36	11.05	11.74	12.43	13.12	33.15
$\frac{7}{8}$	8.93	9.67	10.41	11.16	11.90	12.65	13.39	14.13	35.70
$\frac{15}{16}$	9.57	10.36	11.16	11.95	12.75	13.55	14.34	15.14	38.25
1	10.20	11.05	11.90	12.75	13.60	14.45	15.30	16.15	40.80
$1\frac{1}{16}$	10.84	11.74	12.65	13.55	14.45	15.35	16.26	17.16	43.35
$1\frac{1}{8}$	11.48	12.43	13.39	14.34	15.30	16.26	17.22	18.17	45.90
$1\frac{3}{16}$	12.12	13.12	14.13	15.14	16.15	17.16	18.17	19.18	48.45
$1\frac{1}{4}$	12.75	13.81	14.87	15.94	17.00	18.06	19.13	20.19	51.00
$1\frac{5}{16}$	13.39	14.50	15.62	16.74	17.85	18.96	20.08	21.20	53.55
$1\frac{3}{8}$	14.03	15.20	16.36	17.53	18.70	19.87	21.04	22.21	56.10
$1\frac{7}{16}$	14.66	15.88	17.10	18.33	19.55	20.77	21.99	23.22	58.65
$1\frac{1}{2}$	15.30	16.58	17.85	19.13	20.40	21.68	22.95	24.23	61.20
$1\frac{9}{16}$	15.94	17.27	18.60	19.92	21.25	22.58	23.91	25.24	63.75
$1\frac{5}{8}$	16.58	17.96	19.34	20.72	22.10	23.48	24.87	26.25	66.30
$1\frac{11}{16}$	17.22	18.65	20.08	21.51	22.95	24.38	25.82	27.26	68.85
$1\frac{3}{4}$	17.85	19.34	20.83	22.32	23.80	25.29	26.78	28.27	71.40
$1\frac{7}{8}$	18.49	20.03	21.57	23.11	24.65	26.19	27.73	29.27	73.95
$1\frac{15}{16}$	19.13	20.72	22.31	23.91	25.50	27.10	28.69	30.28	76.50
$1\frac{1}{2}$	19.77	21.41	23.06	24.70	26.35	28.00	29.64	31.29	79.05
2	20.40	22.10	23.80	25.50	27.20	28.90	30.60	32.30	81.60

Weights of Flat Rolled Steel

Per Lineal Foot

Continued

Thick- ness, Inches	WIDTH, INCHES								
	5	5¼	5½	5¾	6	6¼	6½	6¾	12
$\frac{1}{16}$	3.19	3.35	3.51	3.67	3.83	3.99	4.14	4.30	7.65
$\frac{1}{8}$	4.25	4.46	4.67	4.89	5.10	5.31	5.53	5.74	10.20
$\frac{3}{16}$	5.31	5.58	5.84	6.11	6.38	6.64	6.90	7.17	12.75
$\frac{1}{4}$	6.38	6.69	7.02	7.34	7.65	7.97	8.29	8.61	15.30
$\frac{5}{16}$	7.44	7.81	8.18	8.56	8.93	9.29	9.67	10.04	17.85
$\frac{3}{8}$	8.50	8.93	9.35	9.77	10.20	10.63	11.05	11.48	20.40
$\frac{7}{16}$	9.57	10.04	10.53	11.00	11.48	11.95	12.43	12.91	22.95
$\frac{1}{2}$	10.63	11.16	11.69	12.22	12.75	13.28	13.81	14.34	25.50
$\frac{9}{16}$	11.69	12.27	12.85	13.44	14.03	14.61	15.20	15.78	28.05
$\frac{5}{8}$	12.75	13.39	14.03	14.67	15.30	15.94	16.58	17.22	30.60
$\frac{11}{16}$	13.81	14.50	15.19	15.88	16.58	17.27	17.95	18.65	33.15
$\frac{3}{4}$	14.87	15.62	16.36	17.10	17.85	18.60	19.34	20.08	35.70
$\frac{7}{8}$	15.94	16.74	17.53	18.33	19.13	19.92	20.72	21.51	38.25
1	17.00	17.85	18.70	19.55	20.40	21.25	22.10	22.95	40.80
$1\frac{1}{16}$	18.06	18.96	19.87	20.77	21.68	22.58	23.48	24.39	43.35
$1\frac{1}{8}$	19.13	20.08	21.04	21.99	22.95	23.91	24.87	25.82	45.90
$1\frac{1}{4}$	20.19	21.20	22.21	23.22	24.23	25.23	26.24	27.25	48.45
$1\frac{3}{8}$	21.25	22.32	23.38	24.44	25.50	26.56	27.62	28.69	51.00
$1\frac{1}{2}$	22.32	23.43	24.54	25.66	26.78	27.90	29.01	30.12	53.55
$1\frac{5}{8}$	23.38	24.54	25.71	26.88	28.05	29.22	30.39	31.56	56.10
$1\frac{3}{4}$	24.44	25.66	26.88	28.10	29.33	30.55	31.77	32.99	58.65
$1\frac{7}{8}$	25.50	26.78	28.05	29.33	30.60	31.88	33.15	34.43	61.20
2	26.57	27.89	29.22	30.55	31.88	33.20	34.53	35.86	63.75
$2\frac{1}{16}$	27.63	29.01	30.39	31.77	33.15	34.53	35.91	37.29	66.30
$2\frac{1}{8}$	28.69	30.12	31.55	32.99	34.43	35.86	37.30	38.73	68.85
$2\frac{1}{4}$	29.75	31.24	32.73	34.22	35.70	37.19	38.68	40.17	71.40
$2\frac{3}{8}$	30.81	32.35	33.89	35.43	36.98	38.52	40.05	41.60	73.95
$2\frac{1}{2}$	31.87	33.47	35.06	36.65	38.25	39.85	41.44	43.03	76.50
$2\frac{5}{8}$	32.94	34.59	36.23	37.88	39.53	41.17	42.82	44.46	79.05
3	34.00	35.70	37.40	39.10	40.80	42.50	44.20	45.90	81.60

Weights of Flat Rolled Steel

Per Lineal Foot

Continued

Thick- ness, Inches	WIDTH, INCHES								
	7	7¼	7½	7¾	8	8¼	8½	8¾	12
$\frac{3}{16}$	4.46	4.62	4.78	4.94	5.10	5.26	5.42	5.58	7.65
$\frac{1}{4}$	5.95	6.16	6.36	6.58	6.80	7.01	7.22	7.43	10.20
$\frac{5}{16}$	7.44	7.70	7.97	8.23	8.50	8.76	9.03	9.29	12.75
$\frac{3}{8}$	8.93	9.25	9.57	9.88	10.20	10.52	10.84	11.16	15.30
$\frac{7}{16}$	10.41	10.78	11.16	11.53	11.90	12.27	12.64	13.02	17.85
$\frac{1}{2}$	11.90	12.32	12.75	13.18	13.60	14.03	14.44	14.87	20.40
$\frac{9}{16}$	13.39	13.86	14.34	14.82	15.30	15.78	16.26	16.74	22.95
$\frac{5}{8}$	14.87	15.40	15.94	16.47	17.00	17.53	18.06	18.59	25.50
$\frac{11}{16}$	16.36	16.94	17.53	18.12	18.70	19.28	19.86	20.45	28.05
$\frac{3}{4}$	17.85	18.49	19.13	19.77	20.40	21.04	21.68	22.32	30.60
$\frac{13}{16}$	19.34	20.03	20.72	21.41	22.10	22.79	23.48	24.17	33.15
$\frac{7}{8}$	20.83	21.57	22.32	23.05	23.80	24.55	25.30	26.04	35.70
$\frac{15}{16}$	22.32	23.11	23.91	24.70	25.50	26.30	27.10	27.89	38.25
1	23.80	24.65	25.50	26.35	27.20	28.05	28.90	29.75	40.80
$1\frac{1}{16}$	25.29	26.19	27.10	28.00	28.90	29.80	30.70	31.61	43.35
$1\frac{1}{8}$	26.78	27.73	28.68	29.64	30.60	31.56	32.52	33.47	45.90
$1\frac{3}{16}$	28.26	29.27	30.28	31.29	32.30	33.31	34.32	35.33	48.45
$1\frac{1}{4}$	29.75	30.81	31.88	32.94	34.00	35.06	36.12	37.20	51.00
$1\frac{5}{16}$	31.23	32.35	33.48	34.59	35.70	36.81	37.93	39.05	53.55
$1\frac{3}{8}$	32.72	33.89	35.06	36.23	37.40	38.57	39.74	40.91	56.10
$1\frac{7}{16}$	34.21	35.44	36.66	37.88	39.10	40.32	41.54	42.77	58.65
$1\frac{1}{2}$	35.70	36.98	38.26	39.53	40.80	42.08	43.35	44.63	61.20
$1\frac{9}{16}$	37.19	38.51	39.84	41.17	42.50	43.83	45.16	46.49	63.75
$1\frac{5}{8}$	38.67	40.05	41.44	42.82	44.20	45.58	46.96	48.34	66.30
$1\frac{11}{16}$	40.16	41.59	43.03	44.47	45.90	47.33	48.76	50.20	68.85
$1\frac{3}{4}$	41.65	43.14	44.63	46.12	47.60	49.09	50.58	52.07	71.40
$1\frac{13}{16}$	43.14	44.68	46.22	47.76	49.30	50.84	52.38	53.92	73.95
$1\frac{7}{8}$	44.63	46.22	47.82	49.40	51.00	52.60	54.20	55.79	76.50
$1\frac{15}{16}$	46.12	47.76	49.41	51.05	52.70	54.35	56.00	57.60	79.05
2	47.60	49.30	51.00	52.70	54.40	56.10	57.80	59.50	81.60

Weights of Flat Rolled Steel

Per Lineal Foot

Continued

Thick- ness, Inches	WIDTH, INCHES								
	9	9¼	9½	9¾	10	10¼	10½	10¾	12
$\frac{3}{16}$	5.74	5.90	6.06	6.22	6.38	6.54	6.70	6.86	7.65
$\frac{1}{4}$	7.65	7.86	8.08	8.29	8.50	8.71	8.92	9.14	10.20
$\frac{5}{16}$	9.56	9.83	10.10	10.36	10.62	10.89	11.16	11.42	12.75
$\frac{3}{8}$	11.48	11.80	12.12	12.44	12.75	13.07	13.39	13.71	15.30
$\frac{7}{16}$	13.40	13.76	14.14	14.51	14.88	15.25	15.62	15.99	17.85
$\frac{1}{2}$	15.30	15.73	16.16	16.58	17.00	17.42	17.85	18.28	20.40
$\frac{9}{16}$	17.22	17.69	18.18	18.65	19.14	19.61	20.08	20.56	22.95
$\frac{5}{8}$	19.13	19.65	20.19	20.72	21.25	21.78	22.32	22.85	25.50
$\frac{11}{16}$	21.04	21.62	22.21	22.79	23.38	23.96	24.54	25.13	28.05
$\frac{3}{4}$	22.96	23.59	24.23	24.86	25.50	26.14	26.78	27.42	30.60
$\frac{13}{16}$	24.86	25.55	26.24	26.94	27.62	28.32	29.00	29.69	33.15
$\frac{7}{8}$	26.78	27.52	28.26	29.01	29.75	30.50	31.24	31.98	35.70
$\frac{15}{16}$	28.69	29.49	30.28	31.08	31.88	32.67	33.48	34.28	38.25
1	30.60	31.45	32.30	33.15	34.00	34.85	35.70	36.55	40.80
$1\frac{1}{16}$	32.52	33.41	34.32	35.22	36.12	37.03	37.92	38.83	43.35
$1\frac{1}{8}$	34.43	35.38	36.34	37.29	38.25	39.21	40.17	41.12	45.90
$1\frac{1}{4}$	36.34	37.35	38.36	39.37	40.38	41.39	42.40	43.40	48.45
$1\frac{3}{8}$	38.26	39.31	40.37	41.44	42.50	43.56	44.63	45.69	51.00
$1\frac{5}{8}$	40.16	41.28	42.40	43.52	44.64	45.75	46.86	47.97	53.55
$1\frac{3}{4}$	42.08	43.25	44.41	45.58	46.75	47.92	49.08	50.25	56.10
$1\frac{7}{8}$	44.00	45.22	46.44	47.66	48.88	50.10	51.32	52.54	58.65
$1\frac{1}{2}$	45.90	47.18	48.45	49.73	51.00	52.28	53.55	54.83	61.20
$1\frac{9}{8}$	47.82	49.14	50.48	51.80	53.14	54.46	55.78	57.11	63.75
$1\frac{5}{4}$	49.73	51.10	52.49	53.87	55.25	56.63	58.02	59.40	66.30
$1\frac{11}{8}$	51.64	53.07	54.51	55.94	57.38	58.81	60.24	61.68	68.85
$1\frac{3}{4}$	53.56	55.04	56.53	58.01	59.50	60.99	62.48	63.97	71.40
$1\frac{13}{8}$	55.46	57.00	58.54	60.09	61.62	63.17	64.70	66.24	73.95
$1\frac{7}{4}$	57.38	58.97	60.56	62.16	63.75	65.35	66.94	68.53	76.50
$1\frac{15}{8}$	59.29	60.94	62.58	64.23	65.88	67.52	69.18	70.83	79.05
2	61.20	62.90	64.60	66.30	68.00	69.70	71.40	73.10	81.60

Weights of Flat Rolled Steel

Per Lineal Foot

Continued

Thick- ness, Inches	WIDTH, INCHES							
	11	11 $\frac{1}{4}$	11 $\frac{1}{2}$	11 $\frac{3}{4}$	12	12 $\frac{1}{4}$	12 $\frac{1}{2}$	12 $\frac{3}{4}$
$\frac{3}{16}$	7.02	7.17	7.32	7.49	7.65	7.82	7.98	8.13
$\frac{1}{4}$	9.34	9.57	9.78	10.00	10.20	10.42	10.63	10.84
$\frac{5}{16}$	11.68	11.95	12.22	12.49	12.75	13.01	13.28	13.55
$\frac{3}{8}$	14.03	14.35	14.68	14.99	15.30	15.62	15.94	16.26
$\frac{7}{16}$	16.36	16.74	17.12	17.49	17.85	18.23	18.60	18.97
$\frac{1}{2}$	18.70	19.13	19.55	19.97	20.40	20.82	21.25	21.67
$\frac{9}{16}$	21.02	21.51	22.00	22.48	22.95	23.43	23.90	24.39
$\frac{5}{8}$	23.38	23.91	24.44	24.97	25.50	26.03	26.56	27.09
$\frac{11}{16}$	25.70	26.30	26.88	27.47	28.05	28.64	29.22	29.80
$\frac{3}{4}$	28.05	28.68	29.33	29.97	30.60	31.25	31.88	32.52
$\frac{13}{16}$	30.40	31.08	31.76	32.46	33.15	33.83	34.53	35.22
$\frac{7}{8}$	32.72	33.47	34.21	34.95	35.70	36.44	37.19	37.93
$\frac{15}{16}$	35.06	35.86	36.66	37.46	38.25	39.05	39.84	40.64
1	37.40	38.25	39.10	39.95	40.80	41.65	42.50	43.35
$1\frac{1}{16}$	39.74	40.64	41.54	42.45	43.35	44.25	45.16	46.06
$1\frac{1}{8}$	42.08	43.04	44.00	44.94	45.90	46.86	47.82	48.77
$1\frac{3}{8}$	44.42	45.42	46.44	47.45	48.45	49.46	50.46	51.48
$1\frac{1}{4}$	46.76	47.82	48.88	49.94	51.00	52.06	53.12	54.19
$1\frac{5}{8}$	49.08	50.20	51.32	52.44	53.55	54.67	55.78	56.90
$1\frac{3}{2}$	51.42	52.59	53.76	54.93	56.10	57.27	58.44	59.60
$1\frac{7}{8}$	53.76	54.99	56.21	57.43	58.65	59.87	61.10	62.32
$1\frac{1}{2}$	56.10	57.37	58.65	59.93	61.20	62.48	63.75	65.03
$1\frac{9}{8}$	58.42	59.76	61.10	62.43	63.75	65.08	66.40	67.74
$1\frac{5}{4}$	60.78	62.16	63.54	64.92	66.30	67.68	69.06	70.44
$1\frac{11}{8}$	63.10	64.55	65.98	67.42	68.85	70.29	71.72	73.15
$1\frac{3}{4}$	65.45	66.93	68.43	69.92	71.40	72.90	74.38	75.87
$1\frac{13}{8}$	67.80	69.33	70.86	72.41	73.95	75.48	77.03	78.57
$1\frac{7}{4}$	70.12	71.72	73.31	74.90	76.50	78.09	79.69	81.28
$1\frac{15}{8}$	72.46	74.11	75.76	77.41	79.05	80.70	82.34	83.99
2	74.80	76.50	78.20	79.90	81.60	83.30	85.00	86.70

Weights of Flat Rolled Steel

Per Lineal Foot

Continued

Thick- ness, Inches	Width, Inches								
	13	14	15	16	17	18	19	20	21
$\frac{3}{16}$	8.28	8.92	9.56	10.20	10.84	11.48	12.10	12.76	13.40
$\frac{1}{4}$	11.06	11.90	12.75	13.60	14.44	15.30	16.16	17.00	17.84
$\frac{5}{16}$	13.81	14.88	15.94	17.00	18.06	19.12	20.20	21.24	22.32
$\frac{3}{8}$	16.58	17.86	19.14	20.40	21.68	22.96	24.24	25.50	26.78
$\frac{7}{16}$	19.34	20.82	22.32	23.80	25.28	26.79	28.28	29.75	31.24
$\frac{1}{2}$	22.10	23.80	25.50	27.20	28.89	30.60	32.31	34.00	35.70
$\frac{9}{16}$	24.86	26.78	28.70	30.60	32.52	34.44	36.34	38.27	40.16
$\frac{5}{8}$	27.62	29.74	31.88	34.00	36.12	38.25	40.37	42.50	44.64
$\frac{11}{16}$	30.39	32.72	35.06	37.40	39.72	42.08	44.42	46.74	49.08
$\frac{3}{4}$	33.16	35.71	38.26	40.80	43.36	45.92	48.46	51.00	53.56
$\frac{7}{8}$	35.91	38.67	41.43	44.20	46.96	49.72	52.48	55.25	58.01
$\frac{15}{16}$	38.68	41.65	44.62	47.60	50.60	53.56	56.52	59.50	62.49
1	41.44	44.63	47.82	51.00	54.20	57.38	60.57	63.76	66.96
	44.20	47.60	51.00	54.40	57.80	61.20	64.60	68.00	71.40
$1\frac{1}{16}$	46.96	50.57	54.20	57.80	61.40	65.02	68.64	72.25	75.85
$1\frac{1}{8}$	49.72	53.55	57.37	61.20	65.04	68.85	72.68	76.50	80.33
$1\frac{1}{4}$	52.48	56.52	60.56	64.60	68.64	72.68	76.72	80.75	84.79
$1\frac{3}{4}$	55.25	59.50	63.76	68.00	72.26	76.50	80.74	85.00	89.26
$1\frac{5}{8}$	58.02	62.47	66.95	71.40	75.86	80.33	84.80	89.28	93.72
$1\frac{3}{4}$	60.77	65.45	70.12	74.80	79.48	84.15	88.83	93.50	98.17
$1\frac{7}{8}$	63.54	68.42	73.32	78.20	83.08	88.00	92.88	97.75	102.65
$1\frac{1}{2}$	66.30	71.40	76.51	81.60	86.70	91.80	96.90	102.00	107.10
$1\frac{9}{16}$	69.06	74.38	79.69	85.00	90.31	95.63	100.94	106.25	111.56
$1\frac{5}{8}$	71.83	77.35	82.88	88.40	93.93	99.45	104.98	110.50	116.03
$1\frac{11}{16}$	74.59	80.33	86.06	91.80	97.54	103.28	109.01	114.75	120.49
$1\frac{3}{4}$	77.35	83.30	89.25	95.20	101.15	107.10	113.05	119.00	124.95
$1\frac{13}{16}$	80.11	86.28	92.44	98.60	104.76	110.93	117.09	123.25	129.41
$1\frac{7}{8}$	82.88	89.25	95.63	102.00	108.38	114.75	121.13	127.50	133.88
$1\frac{15}{16}$	85.64	92.23	98.81	105.40	111.99	118.58	125.16	131.75	138.34
2	88.40	95.20	102.00	108.80	115.60	122.40	129.20	136.00	142.80

Weights of Flat Rolled Steel

Per Lineal Foot

Continued

Thick- ness, Inches	Width, Inches								
	22	23	24	25	26	27	28	29	30
$\frac{3}{16}$	14.04	14.64	15.32	15.96	16.56	17.20	17.84	18.48	19.12
$\frac{1}{4}$	18.69	19.56	20.40	21.26	22.12	22.96	23.80	24.64	25.50
$\frac{5}{16}$	23.36	24.44	25.52	26.56	27.62	28.68	29.76	30.80	31.88
$\frac{3}{8}$	28.06	29.33	30.60	31.88	33.16	34.44	35.72	37.00	38.28
$\frac{7}{16}$	32.72	34.24	35.72	37.20	38.68	40.17	41.65	43.14	44.64
$\frac{1}{2}$	37.40	39.10	40.80	42.50	44.20	45.92	47.60	49.28	51.00
$\frac{9}{16}$	42.04	44.00	45.92	47.80	49.73	51.64	53.56	55.48	57.40
$\frac{5}{8}$	46.76	48.88	51.00	53.12	55.24	57.37	59.49	61.60	63.76
$\frac{11}{16}$	51.40	53.76	56.12	58.44	60.78	63.11	65.44	67.77	70.13
$\frac{3}{4}$	56.10	58.66	61.20	63.76	66.32	68.88	71.42	73.97	76.53
$\frac{7}{8}$	60.79	63.53	66.29	69.06	71.82	74.58	77.34	80.10	82.86
$\frac{15}{16}$	65.44	68.43	71.40	74.38	77.36	80.33	83.30	86.29	89.24
1	70.13	73.32	76.50	79.68	82.88	86.07	89.26	92.44	95.64
	74.80	78.20	81.60	85.00	88.40	91.80	95.20	98.60	102.00
$1\frac{1}{16}$	79.48	83.08	86.70	90.32	93.92	97.54	101.14	104.75	108.38
$1\frac{1}{8}$	84.16	88.00	91.80	95.64	99.44	103.26	107.10	110.92	114.74
$1\frac{3}{16}$	88.83	92.88	96.92	100.92	104.96	109.01	113.05	117.09	121.13
$1\frac{1}{4}$	93.52	97.76	102.00	106.24	110.50	114.76	119.00	123.24	127.51
$1\frac{5}{16}$	98.16	102.64	107.12	111.56	116.04	120.50	124.94	129.40	133.89
$1\frac{3}{8}$	102.84	107.52	112.20	116.88	121.54	126.22	130.90	135.58	140.24
$1\frac{7}{16}$	107.52	112.42	117.30	122.20	127.08	131.96	136.84	141.76	146.64
$1\frac{1}{2}$	112.20	117.30	122.40	127.50	132.60	137.72	142.80	147.92	153.02
$1\frac{9}{16}$	116.88	122.19	127.50	132.81	138.13	143.44	148.75	154.06	159.38
$1\frac{5}{8}$	121.55	127.08	132.60	138.13	143.65	149.18	154.70	160.23	165.75
$1\frac{3}{4}$	126.23	131.96	137.70	143.44	149.18	154.91	160.65	166.39	172.13
$1\frac{7}{8}$	130.90	136.85	142.80	148.75	154.70	160.65	166.60	172.55	178.50
$1\frac{8}{16}$	135.58	141.74	147.90	154.06	160.23	166.39	172.55	178.71	184.88
$1\frac{7}{8}$	140.25	146.63	153.00	159.38	165.75	172.13	178.50	184.88	191.25
$1\frac{15}{16}$	144.93	151.51	158.10	164.69	171.28	177.86	184.45	191.04	197.63
2	149.60	156.40	163.20	170.00	176.80	183.60	190.40	197.20	204.00

Weights of Flat Rolled Steel

Per Lineal Foot

Continued

Thick- ness, Inches	WIDTH, INCHES								
	31	32	33	34	35	36	38	40	42
$\frac{3}{16}$	19.75	20.40	21.04	21.68	22.32	22.96	24.20	25.52	26.80
$\frac{1}{4}$	26.36	27.20	28.04	28.88	29.72	30.59	32.32	34.00	35.68
$\frac{5}{16}$	32.94	34.00	35.04	36.12	37.16	38.24	40.39	42.48	44.64
$\frac{3}{8}$	39.54	40.80	42.08	43.36	44.64	45.92	48.48	51.00	53.56
$\frac{7}{16}$	46.12	47.60	49.08	50.57	52.07	53.58	56.56	59.50	62.48
$\frac{1}{2}$	52.70	54.40	56.10	57.78	59.50	61.20	64.62	68.00	71.40
$\frac{9}{16}$	59.32	61.22	63.12	65.04	66.96	68.88	72.68	76.54	80.32
$\frac{5}{8}$	65.88	68.00	70.13	72.24	74.36	76.50	80.74	85.00	89.28
$\frac{11}{16}$	72.48	74.80	77.12	79.44	81.79	84.15	88.84	93.48	98.16
$\frac{3}{4}$	79.08	81.61	84.16	86.72	89.28	91.84	96.92	102.00	107.12
$\frac{13}{16}$	85.62	88.39	91.15	93.91	96.68	99.44	104.96	110.50	116.02
$\frac{7}{8}$	92.20	95.20	98.20	101.20	104.16	107.12	113.04	119.00	124.98
$\frac{15}{16}$	98.82	102.00	105.20	108.40	111.59	114.76	121.14	127.52	133.92
1	105.40	108.80	112.20	115.60	119.00	122.40	129.20	136.00	142.80
$1\frac{1}{16}$	112.00	115.59	119.20	122.80	126.42	130.04	137.28	144.50	151.70
$1\frac{1}{8}$	118.56	122.40	126.24	130.08	133.90	137.70	145.36	153.00	160.66
$1\frac{1}{4}$	125.16	129.21	133.24	137.28	141.32	145.36	153.44	161.50	169.58
$1\frac{3}{4}$	131.76	136.00	140.28	144.52	148.76	153.00	161.48	170.00	178.52
$1\frac{5}{8}$	138.36	142.81	147.24	151.72	156.20	160.66	169.60	178.56	187.44
$1\frac{3}{2}$	144.92	149.60	154.28	158.96	163.62	168.30	177.66	187.00	196.34
$1\frac{7}{8}$	151.52	156.40	161.28	166.16	171.08	176.00	185.75	195.50	205.29
$1\frac{1}{2}$	158.11	163.20	168.32	173.40	178.51	183.60	193.80	204.00	214.20
$1\frac{9}{8}$	164.69	170.00	175.31	180.63	185.94	191.25	201.88	212.50	223.13
$1\frac{5}{4}$	171.28	176.80	182.33	187.85	193.38	198.90	209.95	221.00	232.05
$1\frac{11}{8}$	177.86	183.60	189.34	195.08	200.81	206.55	218.03	229.50	240.98
$1\frac{3}{4}$	184.45	190.40	196.35	202.30	208.25	214.20	226.10	238.00	249.90
$1\frac{13}{8}$	191.04	197.20	203.36	209.53	215.69	221.85	234.18	246.50	258.83
$1\frac{7}{4}$	197.63	204.00	210.38	216.75	223.13	229.50	242.25	255.00	267.75
$1\frac{15}{8}$	204.21	210.80	217.39	223.98	230.56	237.15	250.33	263.50	276.68
2	210.80	217.60	224.40	231.20	238.00	244.80	258.40	272.00	285.60

Weights of Flat Rolled Steel
Per Lineal Foot
Continued

Thick- ness, Inches	Width, Inches								
	44	46	48	50	52	54	56	58	60
$\frac{3}{16}$	28.08	29.29	30.64	31.92	33.12	34.40	35.68	36.96	38.24
$\frac{1}{4}$	37.38	39.11	40.80	42.52	44.24	45.92	47.60	49.28	51.00
$\frac{5}{16}$	46.72	48.88	51.04	53.12	55.24	57.36	59.51	61.60	63.76
$\frac{3}{8}$	56.12	58.65	61.20	63.76	66.32	68.88	71.44	74.00	76.56
$\frac{7}{16}$	65.44	68.47	71.44	74.40	77.37	80.34	83.30	86.28	89.28
$\frac{1}{2}$	74.80	78.20	81.60	85.00	88.40	91.84	95.20	98.56	102.00
$\frac{9}{16}$	84.09	88.00	91.84	95.60	99.46	103.28	107.12	110.96	114.80
$\frac{5}{8}$	93.52	97.76	102.00	106.24	110.48	114.74	118.98	123.20	127.52
$\frac{11}{16}$	102.81	107.53	112.24	116.88	121.56	126.22	130.88	135.54	140.26
$\frac{3}{4}$	112.20	117.31	122.40	127.52	132.64	137.76	142.85	147.94	153.06
$\frac{13}{16}$	121.56	127.06	132.58	138.12	143.64	149.16	154.68	160.20	165.72
$\frac{7}{8}$	130.89	136.86	142.80	148.76	154.72	160.66	166.60	172.58	178.48
$\frac{15}{16}$	140.27	146.64	153.00	159.36	165.76	172.15	178.52	184.88	191.28
1	149.60	156.40	163.20	170.00	176.80	183.60	190.40	197.20	204.00
$1\frac{1}{16}$	158.96	166.16	173.40	180.64	187.84	195.08	202.28	209.50	216.76
$1\frac{1}{8}$	168.32	175.99	183.60	191.28	198.88	206.52	214.20	221.84	229.48
$1\frac{3}{16}$	177.66	185.76	193.84	201.84	209.92	218.02	226.10	234.18	242.26
$1\frac{1}{4}$	187.04	195.52	204.00	212.48	221.00	229.52	238.00	246.48	255.02
$1\frac{5}{16}$	196.32	205.28	214.24	223.12	232.08	241.00	249.88	258.80	267.78
$1\frac{3}{8}$	205.68	215.04	224.40	233.76	243.08	252.44	261.80	271.16	280.48
$1\frac{7}{16}$	215.04	224.84	234.60	244.40	254.16	263.92	273.68	283.52	293.28
$1\frac{1}{2}$	224.40	234.60	244.80	255.00	265.20	275.44	285.60	295.84	306.04
$1\frac{9}{16}$	233.75	244.38	255.00	265.63	276.25	286.88	297.50	308.13	318.75
$1\frac{5}{8}$	243.10	254.15	265.20	276.25	287.30	298.35	309.40	320.45	331.50
$1\frac{11}{16}$	252.45	263.93	275.40	286.88	298.35	309.83	321.30	332.78	344.25
$1\frac{3}{4}$	261.80	273.70	285.60	297.50	309.40	321.30	333.20	345.10	357.00
$1\frac{13}{16}$	271.15	283.48	295.80	308.13	320.45	332.78	345.10	357.43	369.75
$1\frac{7}{8}$	280.50	293.25	306.00	318.75	331.50	344.25	357.00	369.75	382.50
$1\frac{15}{16}$	289.85	303.03	316.20	329.38	342.55	355.73	368.90	382.08	395.25
2	299.20	312.80	326.40	340.00	353.60	367.20	380.80	394.40	408.00

Universal Mill Plates

Sizes, with Maximum Lengths in Feet

Thickness, Inches	Width, Inches				
	14-17 Inclusive	18-21 Inclusive	22	23	24-36 Inclusive
$\frac{1}{4}$	85	85	85	85	85
$\frac{5}{16}$	85	85	85	85	85
$\frac{3}{8}$	85	85	85	85	85
$\frac{7}{16}$	85	85	85	85	85
$\frac{1}{2}$	85	85	85	85	85
$\frac{5}{8}$	85	85	85	85	85
$\frac{3}{4}$	85	85	85	85	85
$\frac{7}{8}$	85	85	85	85	85
1	85	85	85	85	85
$1\frac{1}{8}$	85	85	85	85	83
$1\frac{1}{4}$	85	85	85	85	78
$1\frac{3}{8}$	85	85	85	85	70
$1\frac{1}{2}$	85	85	83	78	64
$1\frac{5}{8}$	80	80	76	71	58
$1\frac{3}{4}$	73	73	70	68	53
$1\frac{7}{8}$	68	68	65	61	48
2	64	64	61	56	46
2	60	60	56	53	43

For intermediate widths not shown in above table, use length of next greater width.

Sheared Plates

Lengths of Rectangular Plates Rolled on 108-inch Mill

Thickness, Inches	Width, Inches									
	102	98	94	90	88	84	80	76	72	68
$\frac{1}{4}$	192	192	216	228	240	252	264
$\frac{5}{16}$	192	240	252	264	264	276	282	300	340
$\frac{3}{8}$	180	192	240	252	264	300	360	360	360	360
$\frac{7}{16}$	180	192	240	252	264	300	360	360	360	360
$\frac{1}{2}$	180	216	240	276	300	300	360	360	360	360
$\frac{9}{16}$	180	216	240	276	300	360	360	360	360	360
$\frac{5}{8}$	180	216	240	276	300	360	360	360	360	360
$\frac{11}{16}$	180	216	240	276	300	360	360	360	360	360
$\frac{3}{4}$	180	216	240	252	300	360	360	360	360	360
$\frac{13}{16}$	180	216	240	252	300	300	336	340	360	360
$\frac{7}{8}$	180	216	240	240	300	300	336	340	360	360
1	180	216	240	240	300	300	300	324	360	360
$1\frac{1}{4}$	156	180	192	216	276	276	276	276	300	300
$1\frac{3}{8}$	132	132	180	192	240	240	252	252	252	276
$1\frac{1}{2}$	132	132	180	192	240	240	192	192	192	240
$1\frac{5}{8}$	120	120	120	132	132	192	192	192	192	192
$1\frac{3}{4}$	108	108	108	120	120	180	180	180	180	180
$1\frac{7}{8}$	108	120	120	144	144	144	144	144
2	96	108	120	120	126	132	144	144
$2\frac{1}{4}$	96	108	120	126	132	132	144	144
$2\frac{1}{2}$	96	108	120	126	132	132	144	144

Plates of greater dimensions than shown in this table may be submitted for special consideration.

Sheared Plates
Lengths of Rectangular Plates Rolled on 108-inch Mill
Continued

Thickness, Inches	Width, Inches								
	64	60	56	52	48	44	40	36	24
$\frac{1}{4}$	288	300	300	312	336	360	360	360	360
$\frac{5}{16}$	360	360	360	360	360	360	360	360	360
$\frac{3}{8}$	360	360	360	360	360	360	360	360	360
$\frac{7}{16}$	360	360	360	360	360	360	360	360	360
$\frac{1}{2}$	360	360	360	360	360	360	360	360	360
$\frac{9}{16}$	360	360	360	360	360	360	360	360	360
$\frac{5}{8}$	360	360	360	360	360	360	360	360	360
$\frac{11}{16}$	360	360	360	360	360	360	360	360	360
$\frac{3}{4}$	360	360	360	360	360	360	360	360	360
$\frac{13}{16}$	360	360	360	360	360	360	360	360	360
$\frac{7}{8}$	360	360	360	360	360	360	360	360	360
1	360	360	360	360	360	360	360	360	360
$1\frac{1}{4}$	300	300	300	300	360	360	360	360	300
$1\frac{3}{8}$	276	276	276	300	300	300	300	360	300
$1\frac{1}{2}$	240	252	252	252	276	300	300	300	276
$1\frac{5}{8}$	216	240	252	252	276	276	276	300	276
$1\frac{3}{4}$	192	192	240	240	252	252	252	276	252
$1\frac{7}{8}$	156	180	192	192	240	240	240	252	240
2	156	180	180	180	192	192	192	240	240
$2\frac{1}{4}$	156	180	180	180	180	180	180	144	144
$2\frac{1}{2}$	156	156	156	180	180	180	180	144	144

Plates of greater dimensions than shown in this table may be submitted for special consideration.

Sheared Plates

Lengths of Rectangular Plates Rolled on 78-inch Mill

THICKNESS, With Decimal Equivalent	WIDTH, INCHES							
	72	70	68	66	65	60	56	52
*No. 11 Gauge... .125"						144	168	180
†No. 10 Gauge... .134"				120	132	168	180	192
†No. 9 Gauge... .148"				120	144	168	180	192
†No. 8 Gauge... .165"			120	144	156	168	180	192
$\frac{1}{8}$ -inch... .187"	132	144	156	168	180	192	204	216
$\frac{1}{8}$ and $\frac{1}{4}$ -inch... $\begin{cases} .219" \\ .250" \end{cases}$	120	120	132	144	180	192	204	216
$\frac{1}{4}$ -inch... .313"					108	144	156	168
$\frac{3}{8}$ -inch... .375"					96	120	144	156

THICKNESS, With Decimal Equivalent	WIDTH, INCHES						
	48	44	40	36	32	28	24
*No. 11 Gauge..... .125"	192	204	216	228	240	252	264
†No. 10 Gauge..... .134"	204	216	228	240	252	264	276
†No. 9 Gauge..... .148"	204	216	228	240	252	264	276
†No. 8 Gauge..... .165"	216	228	240	252	264	276	288
$\frac{1}{8}$ -inch..... .187"	228	240	264	288	300	300	300
$\frac{1}{8}$ and $\frac{1}{4}$ -inch..... $\begin{cases} .219'' \\ .250'' \end{cases}$	228	240	252	264	276	288	300
$\frac{1}{4}$ -inch..... .313"	180	192	204	216	264	300	300
$\frac{3}{8}$ -inch..... .375"	180	192	216	240	252	264	276

*U. S. Standard.

†Birmingham.

Plates of greater dimensions than shown in this table may be submitted for special consideration.

All our plates are accurately straightened by the most improved methods.

Sketch Plates

Sketch plates, as known in the trade, are sheared plates having other than a rectangular outline. This is modified, in practice, to except straight taper plates varying not more than four inches in width at the ends and having a width at the narrowest end of not less than thirty inches.

It is also customary to except complete circles, circular plates being classified by themselves.

Dimensions of Circular Plates

Thickness, Inches	Maximum Diameter, Inches	Thickness, Inches	Maximum Diameter, Inches
$\frac{1}{8}$	65	$\frac{1}{8}$	103
$\frac{1}{4}$	72	$\frac{3}{8}$	103
$\frac{3}{8}$	90	$\frac{1}{2}$	103
$\frac{1}{2}$	100	$\frac{3}{4}$ }	103
$\frac{5}{8}$	103	up to }	
$\frac{3}{4}$	103	$1\frac{1}{2}$ }	
$\frac{7}{8}$	103		

Weights of Circular Plates

Diameter, Inches	THICKNESS INCHES										
	$\frac{1}{8}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{11}{16}$	$\frac{3}{4}$
16	7	11	14	18	21	25	28	32	36	39	42
17	8	12	16	20	24	28	32	36	40	44	48
18	9	14	18	23	27	32	36	41	46	50	54
19	10	15	20	25	30	35	40	45	50	55	60
20	11	17	22	28	33	39	45	50	56	61	67
21	12	19	25	31	37	43	50	55	61	68	74
22	14	20	27	34	40	47	54	61	67	74	81
23	15	22	30	37	44	52	59	66	74	81	88
24	16	24	32	40	48	56	64	72	80	88	96
25	18	26	35	44	52	61	70	78	87	96	104
26	19	28	38	47	57	66	75	85	94	103	113
27	20	31	41	51	61	71	81	91	101	112	122
28	22	33	44	55	66	76	87	98	109	120	131
29	24	35	47	59	70	82	94	105	117	129	140
30	25	38	50	63	75	88	100	113	125	138	150
31	27	40	54	67	80	94	107	120	134	147	160
32	29	43	57	71	86	100	114	128	142	157	171
33	31	46	61	76	91	106	121	136	152	167	182
34	32	48	64	81	97	113	129	145	161	177	193
35	34	51	68	85	102	119	136	153	170	187	204
36	36	54	72	90	108	126	144	162	180	198	216
37	38	57	76	95	114	133	152	171	190	210	229
38	40	60	80	100	121	141	161	181	201	221	241
39	42	64	85	106	127	148	169	190	212	233	254
40	45	67	89	111	134	156	178	200	223	245	267

Weights of Circular Plates

Continued

Diameter, Inches	THICKNESS, INCHES										
	$\frac{1}{8}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{11}{16}$	$\frac{3}{4}$
41	47	70	94	117	140	164	187	210	234	257	281
42	49	74	98	123	147	172	196	221	245	270	294
43	52	77	103	129	154	180	206	232	257	283	309
44	54	81	108	135	162	189	215	242	269	296	323
45	56	85	113	141	169	197	225	254	282	310	338
46	59	88	118	147	167	206	236	265	294	324	353
47	62	92	123	154	184	215	246	277	307	338	369
48	64	96	128	160	192	224	256	288	320	353	385
49	67	100	134	167	200	234	267	301	334	367	401
50	70	104	139	174	209	243	278	313	348	383	417
51	73	109	145	181	217	253	289	326	362	398	434
52	75	113	150	188	226	263	301	339	376	414	451
53	78	117	156	195	234	274	313	352	391	430	469
54	81	122	162	203	243	284	325	365	406	446	487
55	84	126	168	210	252	295	337	379	421	463	505
56	88	131	175	218	262	305	349	393	436	480	524
57	91	136	181	226	271	317	362	407	452	497	542
58	94	141	187	234	281	328	375	421	468	515	562
59	97	145	194	242	291	339	388	436	484	533	581
60	101	150	201	251	301	351	401	451	501	551	601
61	104	155	207	259	311	363	414	466	518	570	621
62	107	160	214	268	321	375	428	482	535	588	642
63	111	166	221	276	332	387	442	497	552	608	663
64	114	171	228	285	342	399	456	513	570	627	684
65	118	176	235	294	353	412	470	529	588	647	705

Weights of Circular Plates

Diameter, Inches	THICKNESS INCHES										
	$\frac{1}{8}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{11}{16}$	$\frac{3}{4}$
16	7	11	14	18	21	25	28	32	36	39	42
17	8	12	16	20	24	28	32	36	40	44	48
18	9	14	18	23	27	32	36	41	46	50	54
19	10	15	20	25	30	35	40	45	50	55	60
20	11	17	22	28	33	39	45	50	56	61	67
21	12	19	25	31	37	43	50	55	61	68	74
22	14	20	27	34	40	47	54	61	67	74	81
23	15	22	30	37	44	52	59	66	74	81	88
24	16	24	32	40	48	56	64	72	80	88	96
25	18	26	35	44	52	61	70	78	87	96	104
26	19	28	38	47	57	66	75	85	94	103	113
27	20	31	41	51	61	71	81	91	101	112	122
28	22	33	44	55	66	76	87	98	109	120	131
29	24	35	47	59	70	82	94	105	117	129	140
30	25	38	50	63	75	88	100	113	125	138	150
31	27	40	54	67	80	94	107	120	134	147	160
32	29	43	57	71	86	100	114	128	142	157	171
33	31	46	61	76	91	106	121	136	152	167	182
34	32	48	64	81	97	113	129	145	161	177	193
35	34	51	68	85	102	119	136	153	170	187	204
36	36	54	72	90	108	126	144	162	180	198	216
37	38	57	76	95	114	133	152	171	190	210	229
38	40	60	80	100	121	141	161	181	201	221	241
39	42	64	85	106	127	148	169	190	212	233	254
40	45	67	89	111	134	156	178	200	223	245	267

Weights of Circular Plates

Continued

Diameter, Inches	THICKNESS, INCHES										
	$\frac{1}{8}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{11}{16}$	$\frac{3}{4}$
41	47	70	94	117	140	164	187	210	234	257	281
42	49	74	98	123	147	172	196	221	245	270	294
43	52	77	103	129	154	180	206	232	257	283	309
44	54	81	108	135	162	189	215	242	269	296	323
45	56	85	113	141	169	197	225	254	282	310	338
46	59	88	118	147	167	206	236	265	294	324	353
47	62	92	123	154	184	215	246	277	307	338	369
48	64	96	128	160	192	224	256	288	320	353	385
49	67	100	134	167	200	234	267	301	334	367	401
50	70	104	139	174	209	243	278	313	348	383	417
51	73	109	145	181	217	253	289	326	362	398	434
52	75	113	150	188	226	263	301	339	376	414	451
53	78	117	156	195	234	274	313	352	391	430	469
54	81	122	162	203	243	284	325	365	406	446	487
55	84	126	168	210	252	295	337	379	421	463	505
56	88	131	175	218	262	305	349	393	436	480	524
57	91	136	181	226	271	317	362	407	452	497	542
58	94	141	187	234	281	328	375	421	468	515	562
59	97	145	194	242	291	339	388	436	484	533	581
60	101	150	201	251	301	351	401	451	501	551	601
61	104	155	207	259	311	363	414	466	518	570	621
62	107	160	214	268	321	375	428	482	535	588	642
63	111	166	221	276	332	387	442	497	552	608	663
64	114	171	228	285	342	399	456	513	570	627	684
65	118	176	235	294	353	412	470	529	588	647	705

Weights of Circular Plates

Continued

Diameter, Inches	THICKNESS, INCHES												
	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{11}{16}$	$\frac{3}{4}$	$\frac{13}{16}$	$\frac{7}{8}$	$\frac{15}{16}$	1
66	243	303	364	424	485	546	606	667	727	757	848	909	970
67	250	312	375	437	500	562	625	687	750	812	874	937	1000
68	258	322	386	450	515	579	643	708	772	786	900	965	1030
69	265	331	398	464	530	596	662	729	795	866	928	994	1060
70	273	341	409	477	546	614	682	750	818	886	954	1023	1092
71	281	351	421	491	561	631	702	772	842	912	982	1052	1122
72	289	361	433	505	577	649	721	794	866	938	1010	1082	1154
73	297	371	445	519	593	667	741	816	890	964	1038	1112	1186
74	305	381	457	533	610	686	762	838	914	990	1066	1143	1220
75	313	391	470	548	626	705	783	861	939	1018	1096	1172	1252
76	322	402	482	563	643	723	804	884	964	1045	1125	1205	1286
77	330	413	495	578	660	743	825	907	990	1072	1155	1237	1320
78	339	423	508	593	677	762	847	931	1016	1100	1185	1270	1354
79	348	434	521	608	695	782	868	955	1042	1129	1216	1302	1389
80	356	445	534	623	712	802	891	980	1069	1158	1247	1336	1425
81	365	457	548	639	730	822	913	1004	1095	1187	1278	1369	1460
82	374	468	561	655	748	842	936	1029	1123	1216	1310	1403	1497
83	384	479	575	671	767	863	960	1054	1150	1246	1342	1438	1533
84	393	491	589	687	785	884	982	1080	1178	1276	1374	1472	1571
85	402	503	603	704	804	905	1005	1106	1206	1307	1407	1509	1608
86	412	515	618	720	823	926	1029	1132	1235	1338	1441	1543	1646
87	421	527	632	737	843	948	1053	1158	1264	1369	1474	1580	1685
88	431	539	647	754	862	970	1077	1185	1293	1400	1508	1616	1724
89	441	551	662	772	882	992	1102	1212	1323	1433	1543	1653	1763
90	451	564	676	789	902	1014	1127	1240	1352	1465	1577	1690	1803

Weights of Circular Plates

Continued

Diameter, Inches	THICKNESS, INCHES											
	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{11}{16}$	$\frac{3}{4}$	$\frac{13}{16}$	$\frac{7}{8}$	$\frac{15}{16}$	1
91	576	691	807	922	1037	1152	1267	1382	1498	1613	1728	1843
92	589	707	824	942	1060	1178	1295	1413	1531	1648	1766	1884
93	602	722	842	963	1083	1203	1324	1444	1564	1684	1805	1925
94	615	738	861	984	1106	1224	1352	1475	1598	1721	1844	1967
95	628	754	879	1005	1130	1256	1381	1507	1632	1758	1883	2009
96	641	769	897	1025	1154	1282	1410	1538	1666	1795	1923	2051
97	654	785	916	1047	1178	1309	1440	1570	1701	1832	1963	2094
98	668	801	935	1069	1202	1336	1469	1603	1737	1870	2004	2137
99	682	818	954	1091	1227	1363	1500	1636	1772	1908	2045	2181
100	695	835	974	1113	1252	1391	1530	1669	1808	1947	2086	2225
101	709	851	993	1135	1277	1419	1561	1703	1844	1986	2128	2270
102	724	868	1013	1158	1302	1447	1592	1736	1881	2026	2171	2315
103	738	885	1033	1180	1328	1476	1623	1771	1918	2066	2213	2361
104	752	903	1053	1203	1354	1504	1655	1805	1956	2106	2257	2407
105	767	920	1073	1227	1380	1533	1687	1840	1993	2147	2300	2453
106	781	938	1094	1250	1407	1563	1719	1875	2032	2188	2344	2500
107	796	955	1115	1274	1433	1592	1752	1911	2070	2229	2389	2548
108	811	973	1136	1298	1460	1622	1785	1947	2109	2271	2433	2596
109	826	992	1157	1322	1487	1652	1818	1983	2148	2313	2479	2644
110	841	1010	1178	1346	1515	1683	1851	2020	2188	2356	2524	2693
111	857	1028	1200	1371	1542	1714	1885	2056	2228	2400	2570	2742
112	872	1047	1221	1396	1570	1745	1919	2094	2268	2443	2617	2791
113	888	1065	1243	1420	1598	1776	1953	2131	2308	2486	2663	2841
114	904	1085	1266	1446	1627	1808	1989	2170	2350	2531	2712	2893
115	920	1104	1288	1471	1656	1839	2024	2208	2392	2575	2759	2943

Our limit for rolling is 103" diameter (100" for $\frac{5}{16}$ " thickness). Larger sizes are for reference only. Plates up to 1 $\frac{1}{2}$ " thick are rolled. To obtain weights add weight of fractional thickness to that given above for 1" thickness.

Bars for Concrete Reinforcement

Cold Twisted Square Bar



Size, Inches	Area, Square Inches	Weight per Foot, Pounds	Maximum Length, Feet
$\frac{1}{4}$.0625	.212	40
$\frac{5}{16}$.0977	.332	40
$\frac{3}{8}$.1406	.478	40
$\frac{7}{16}$.1914	.651	40
$\frac{1}{2}$.2500	.850	40
$\frac{9}{16}$.3164	1.076	40
$\frac{5}{8}$.3906	1.328	40
$\frac{11}{16}$.4727	1.607	40
$\frac{3}{4}$.5625	1.913	60
$\frac{13}{16}$.6602	2.245	60
$\frac{7}{8}$.7656	2.603	60
$\frac{15}{16}$.8789	2.988	60
1	1.0000	3.400	60
$1\frac{1}{8}$	1.2656	4.303	60
$1\frac{1}{4}$	1.5625	5.312	60
$1\frac{3}{8}$	1.8906	6.428	60
$1\frac{1}{2}$	2.2500	7.650	60

Unless otherwise specified, cold twisted bars are made from low carbon Steel, and after twisting have an elastic limit ranging from 55,000 pounds per square inch for $1\frac{1}{4}$ " bars to 75,000 pounds per square inch for $\frac{1}{4}$ " bars.

All intermediate sizes can be furnished.

Weights and Areas of Twisted Bars are equal to plain square bars of like denominations.

Longer lengths furnished only by special arrangement.

Circular mailed upon application.

Bars for Concrete Reinforcement

Diamond Bar



Size, Inches	Area, Square Inches	Weight per Foot, Pounds	Maximum Length, Feet
$\frac{3}{8}$.1406	.478	40
$\frac{7}{16}$.1914	.651	40
$\frac{1}{2}$.2500	.850	40
$\frac{5}{8}$.3906	1.328	40
$\frac{3}{4}$.5625	1.913	60
$\frac{7}{8}$.7656	2.603	60
1	1.0000	3.400	60
$1\frac{1}{8}$	1.2656	4.303	60
$1\frac{1}{4}$	1.5625	5.312	60
$1\frac{1}{2}$	2.2500	7.650	60

Weights and areas of Diamond Bars are equal to plain Square Bars of like denominations.

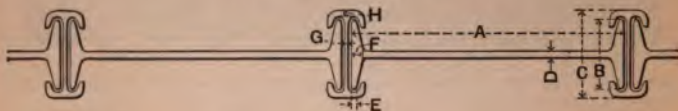
Longer lengths furnished only by special arrangement.

Circular mailed upon application.

J & L Sheet Piling

Under Patent Dated October 13, 1908

Weights and Dimensions



Section Index	Size, Inches	Weight Per Sq. Ft., Pounds	A	B	C	D	E	F	G	H
000	12 x 4 1/4	32.00	12	2.90	4 1/4	0.335	0.35	0.75	0.21	0.56
00	12 x 4 1/4	33.50	12	2.94	4 1/4	0.375	0.35	0.75	0.21	0.56
0	12 x 4 1/4	35.00	12	2.94	4 1/4	0.415	0.35	0.75	0.21	0.56
1	12 x 5	35.00	12	3.94	5	0.34	0.35	0.65	0.21	0.44
2	12 x 5	36.25	12	3.94	5	0.38	0.35	0.65	0.21	0.44
3	15 x 6	37.20	15	4.75	6	0.38	0.37	0.74	0.23	0.49
4	15 x 6	39.75	15	4.75	6	0.44	0.37	0.74	0.23	0.49
5	15 x 6	42.25	15	4.75	6	0.50	0.37	0.74	0.23	0.49

From the above table and cuts and those on following pages, it will be seen that J & L SHEET PILING has been designed from an economical and efficient basis. There are eight sections available, embracing economy in weight, high section modulus, free driving qualities, etc.

The metal is so distributed as to form a rigid section, which means efficiency inasmuch as the blows from the hammer are all effective and the energy is not lost in overcoming excessive friction and distortion.

The joints are practically watertight as driven, which is important, especially in cofferdam work or in "cut-off" walls.

We attach a locking bar to one flange of each piling beam at the mill before shipment and these are shipped, handled and driven as a unit.

The piling beams have a maximum salvage value, as, when no longer required as piling, the sections (being 12" and 15" beams) are available for other uses.

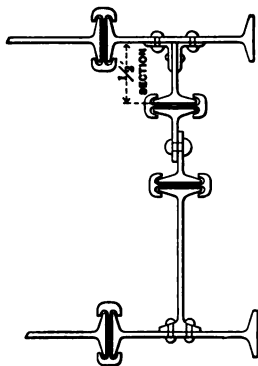
For information regarding the strength of the interlock see page 86.

Illustrated Catalogue mailed upon application.

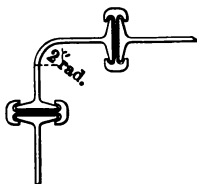
J & L Sheet Piling

Standard Corner Pieces and Special Connections

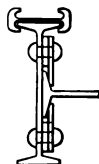
Special Fabricated Corner and Connection. $\frac{1}{2}$ Section attached to Web of Another Section by Means of Angles and Rivets.



Section Employed to Straighten Wall when Toe of Section has been Thrown Forward or Back from a Vertical Line.

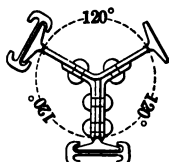


Standard Corner with Web Bent 90° with a 2 inch Radius

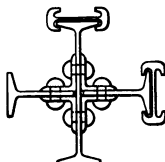


Special Section for Cross Wall Connection

Special Corner and Connection. Flange of One I-Beam Riveted Direct to Web of Another Section.



120° Y Pile



90° Cross

The above are corner pieces and special connections which are ordinarily used but if unusual conditions or special designs require other details, this piling can readily be adapted to meet such situations.

J & L Sheet Piling



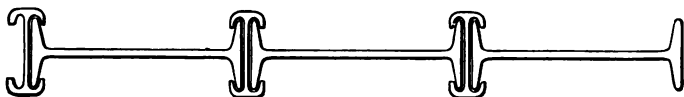
Properties of Sheet Piling Beams

Section Index	Depth of Beam, Inches	Weight per Linear Foot, Pounds	Area of Section, Square Inches	Thickness of Web, Inches	Width of Flange, Inches	Moment of Inertia Neutral Axis Perpendicular to Web at Center	Moment of Inertia Neutral Axis Coincident with Center Line of Web	Radius of Gyration Neutral Axis Perpendicular to Web at Center	Radius of Gyration Neutral Axis Coincident with Center Line of Web	Section Factor Neutral Axis Perpendicular to Web at Center	Section Factor Neutral Axis Coincident with Center Line of Web
B-315	12	23.26	6.84	0.34	2.90	140.50	1.92	4.53	0.53	23.42	1.32
B-314	12	24.90	7.32	0.38	2.94	146.27	2.01	4.47	0.52	24.38	1.37
B-313	12	26.37	7.76	0.42	2.94	150.47	2.04	4.40	0.51	25.08	1.38
B-310	12	26.30	7.72	0.34	3.94	167.76	4.43	4.67	0.76	27.96	2.25
B-309	12	27.60	8.10	0.38	3.94	172.10	4.56	4.61	0.75	28.68	2.30
B-302	15	35.75	10.50	0.38	4.75	358.16	8.52	5.84	0.90	47.75	3.59
B-301	15	39.00	11.44	0.44	4.75	375.03	8.91	5.71	0.88	50.00	3.70
B-300	15	42.25	12.37	0.50	4.75	391.92	9.31	5.62	0.87	52.25	3.82

Properties of Locking Bars

Section Index	Depth of Locking Bar, Inches	Weight per Linear Foot, Pounds	Area of Sections, Square Inches	Thickness of Web, Inches	Moment of Inertia Neutral Axis Perpendicular to Web at Center	Moment of Inertia Neutral Axis Coincident with Center Line of Web	Radius of Gyration Neutral Axis Perpendicular to Web at Center	Radius of Gyration Neutral Axis Coincident with Center Line of Web	Section Factor Neutral Axis Perpendicular to Web at Center	Section Factor Neutral Axis Coincident with Center Line of Web
B-322	4 $\frac{3}{4}$	10.3	3.00	0.21	7.50	0.87	1.58	0.54	3.53	0.54
B-321	5	9.75	2.87	0.21	10.50	0.64	1.91	0.47	4.20	0.64
B-316	6	12.25	3.61	0.23	18.42	1.11	2.26	0.55	6.14	1.03

J & L Sheet Piling



Properties of Combined Sections
Joints Considered as a Unit

Section Index	Size, Inches	Weight per Square Ft. of Assembled Area, Pounds	Total Sectional Area Assembled Section, Sq. Inches	Width of Joint Over All, Inches	Moment of Inertia Neutral Axis Coincident with Center Line of Web	Radius of Gyration Neutral Axis Coincident with Center Line of Web	Section Factor Neutral Axis Coincident with Center Line of Web
000	12x4 $\frac{1}{4}$	32.0	9.84	4 $\frac{1}{4}$	9.42	0.99	4.85
00	12x4 $\frac{1}{4}$	33.5	10.32	4 $\frac{1}{4}$	9.52	0.96	4.90
0	12x4 $\frac{1}{4}$	35.0	10.76	4 $\frac{1}{4}$	9.54	0.94	4.91
1	12x5	35.0	10.59	5	14.93	1.19	6.45
2	12x5	36.25	10.97	5	15.06	1.17	6.50
3	15x6	37.20	14.11	5	26.94	1.38	9.73
4	15x6	39.75	15.05	5	27.33	1.35	9.84
5	15x6	42.25	15.98	5	27.73	1.31	9.96

J & L Sheet Piling**Unlocking Tests**

The following table shows the result of a series of tests made on J & L Sheet Piling to determine the strength of the interlock.

Pieces of the proper length were locked together, placed in the grips of a 200,000 pound Riehle Testing Machine and a pull exerted which would tend to "unlock" the beams and locking bars. This table shows actual results from tests on nine different sets of beams and locking bars.

12-inch Piling Beams— $4\frac{1}{4}$ -inch Locking Bars
Medium Grade Open Hearth Steel

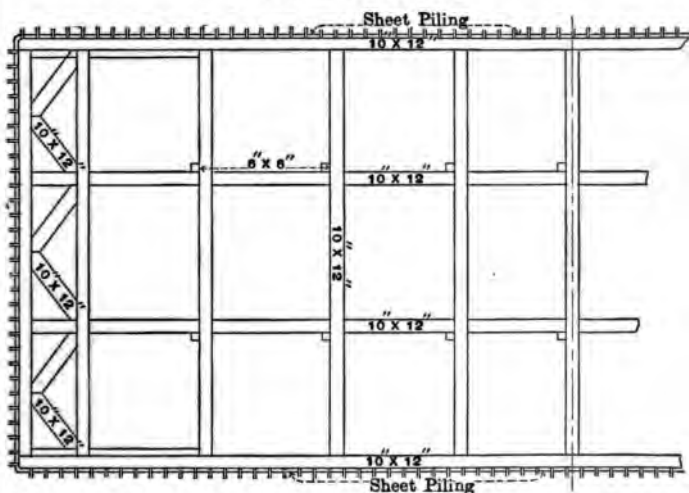
Set No.	Section Index	Weight per Square Foot	Resistance per Linear Inch of Section
1	000	32 pounds	13,010 pounds
2	000	32 pounds	13,360 pounds
3	000	32 pounds	13,420 pounds
4	0	35 pounds	12,650 pounds
5	0	35 pounds	13,040 pounds
6	0	35 pounds	12,450 pounds
7	0	35 pounds	12,500 pounds
8	0	35 pounds	12,350 pounds
9	0	35 pounds	13,240 pounds

The strength of an interlock or grip at a joint is important, especially where there is a tension in a wall of piling tending to "unlock" the sections at the joints. Such tension usually exists in double wall dams, or in any enclosure where the pressure is exerted outwardly, usually caused by an earthen or concrete filling. The joints in a wall of piling, used as a retaining wall, are also very often subjected to pressures, causing heavy tension.

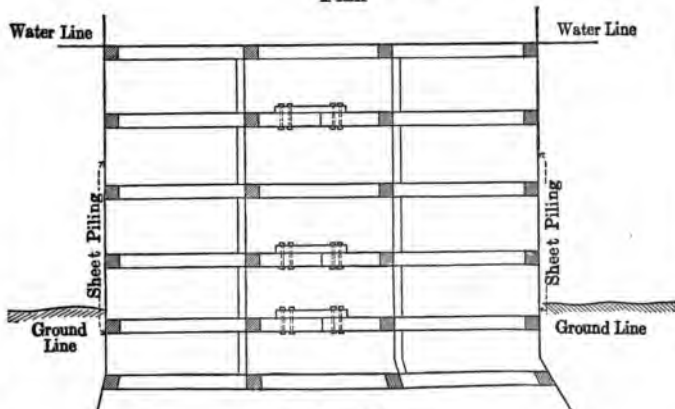
The table above will show, at a glance, that J & L Sheet Piling has been designed to take care of these conditions. The strength of interlock is in excess of any sheet piling now on the market.

J & L Sheet Piling

Plan and Sectional View of Cofferdam showing Typical Timber Bracing



Plan



Sectional View

Steel Piling for Retaining Earth

Formulae

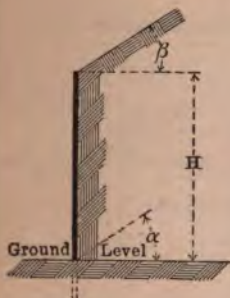
Let W = Weight of a cubic foot of soil retained, in lbs.

H = Height of steel piling above ground on outside, in feet.

α = Angle of repose of soil. (See following tables.)

β = Angle of slope of earth retained (if any).

P = Pressure on each lineal foot of the steel sheet piling wall, in lbs.



$$\text{Then } P = \frac{WH^2}{2} \times \frac{1 - \sin \alpha}{1 + \sin \alpha} \text{ when } \beta = 0$$

$$P = \frac{WH^2 \cos \alpha}{2} \text{ when } \beta = \alpha$$

$$P = \cos \beta \frac{\cos \beta - \sqrt{\cos^2 \beta - \cos^2 \alpha}}{\cos \beta + \sqrt{\cos^2 \beta - \cos^2 \alpha}} \times \frac{WH^2}{2} \text{ for any other slope.}$$

In the following examples let

$W = 100$ lbs. per cubic foot

$H = 30$ feet

$\alpha = 36^\circ 53'$ for soil

1. Then, when $\beta = 0$

$$P = \frac{WH^2}{2} \times \frac{1 - \sin 36^\circ 53'}{1 + \sin 36^\circ 53'} = \frac{100 \times 900}{2} \times \frac{1 - .6}{1 + .6} \\ = 45,000 \times .25 = 11,250 \text{ lbs. or 5.63 tons.}$$

2. When $\beta = \text{say } 20^\circ$

$$P = \frac{WH^2}{2} \cos 20^\circ \frac{\cos 20^\circ - \sqrt{\cos^2 20^\circ - \cos^2 36^\circ 53'}}{\cos 20^\circ + \sqrt{\cos^2 20^\circ - \cos^2 36^\circ 53'}} \\ = \frac{100 \times 900}{2} \times .939 \times \frac{.939 - .493}{.939 + .493} \\ = 45,000 \times .293 = 13,185 \text{ lbs. or 6.6 tons.}$$

3. When $\beta = 36^\circ 53' = \alpha$

$$P = \frac{WH^2}{2} \cos 36^\circ 53' \\ = \frac{100 \times 900}{2} \times .8 = 36,000 \text{ lbs. or 18 tons.}$$

Steel Piling for Retaining Earth

Continued

Slope of Repose and Weights for Loose Earth

KIND OF EARTH	Slope of Repose	Angle of Repose	Weight, Pounds per Cubic Foot
Sand, clean.....	1.5 to 1	33° 41'	100
Sand and Clay.....	1.33 to 1	36° 53'	100
Clay, dry.....	1.33 to 1	36° 53'	100
Clay, damp, plastic.....	2.00 to 1	26° 34'	100
Gravel, clean.....	1.33 to 1	36° 53'	100
Gravel and Clay.....	1.33 to 1	36° 53'	100
Gravel, Sand and Clay....	1.33 to 1	36° 53'	100
Soil.....	1.33 to 1	36° 53'	100
Soft Rotten Rock.....	1.33 to 1	36° 53'	110
Hard Rock.....	1 to 1	45° 0'	100
Bituminous Cinders.....	1 to 1	45° 0'	50
Anthracite Ashes.....	1 to 1	45° 0'	30

Material Excavated by a Wet or Dry Process and dumped into Water, as at the Back of a Sea-Wall, has Weights and Slopes approximately as follows

KIND OF MATERIAL	Slope of Repose	Angle of Repose	Weight, Pounds per Cubic Foot
Sand, clean.....	2 to 1	26° 34'	60
Sand and Clay.....	3 to 1	18° 26'	65
Clay.....	3½ to 1	15° 57'	80
Gravel, clean.....	2 to 1	26° 34'	60
Gravel and Clay.....	3 to 1	18° 26'	65
Gravel, Sand and Clay....	3 to 1	18° 26'	65
Soil.....	3½ to 1	15° 57'	70
Soft Rotten Rock.....	1 to 1	45° 0'	65
Hard Rock.....	1 to 1	45° 0'	65
River Mud.....	∞ to 1	0° 0'	90

Chain

Straight
Link
Coil
Chain



Conveyor or
Sprocket
Wheel
Chain



Twist
Coil Chain



Straight-Link Coil Chain

Size of Chain, Inches	Length of Link, Inches	Width of Link, Inches	Weight of Chain, per Foot	Proof Test for BB Chain	Proof Test for BBB Chain	Proof Test for Dredge Chain
t	l	W	Pounds	Tons	Tons	Tons
$\frac{1}{8}$	$1\frac{3}{8}$	$\frac{1}{8}$.50	.39	.45	.50
$\frac{1}{4}$	$1\frac{1}{2}$	1	.75	.66	.75	.80
$\frac{5}{16}$	$1\frac{3}{4}$	$1\frac{1}{8}$	1.10	1.37	1.60	1.70
$\frac{3}{8}$	2	$1\frac{3}{8}$	1.55	1.92	2.21	2.36
$\frac{7}{16}$	$2\frac{1}{4}$	$1\frac{5}{8}$	2.00	2.64	3.05	3.33
$\frac{1}{2}$	$2\frac{1}{2}$	$1\frac{3}{4}$	2.65	3.41	3.92	4.42
$\frac{9}{16}$	$2\frac{7}{8}$	$1\frac{7}{8}$	3.25	4.29	4.93	5.53
$\frac{5}{8}$	$3\frac{1}{4}$	$2\frac{1}{8}$	4.20	5.28	6.07	6.67
$\frac{11}{16}$	$3\frac{1}{2}$	$2\frac{5}{8}$	5.00	6.32	7.28	8.02
$\frac{3}{4}$	$3\frac{3}{4}$	$2\frac{1}{2}$	5.90	7.59	8.74	9.24
$\frac{13}{16}$	4	$2\frac{11}{16}$	7.00	8.91	10.3	10.7
$\frac{7}{8}$	$4\frac{1}{4}$	3	8.00	10.3	11.9	12.1
$\frac{15}{16}$	$4\frac{1}{2}$	$3\frac{1}{4}$	9.00	11.8	13.6	14.5
1	$4\frac{3}{4}$	$3\frac{1}{2}$	10.0	13.5	15.6	16.3
$1\frac{1}{8}$	$5\frac{1}{2}$	$3\frac{7}{8}$	12.5	16.2	18.6	19.6
$1\frac{1}{4}$	6	$4\frac{1}{4}$	16.0	20.1	23.1	24.0
$1\frac{3}{8}$	$6\frac{1}{2}$	$4\frac{3}{4}$	19.0	24.2	27.8	28.7
$1\frac{1}{2}$	$7\frac{1}{4}$	$5\frac{1}{4}$	21.0	28.9	33.2	34.6
$1\frac{5}{8}$	$7\frac{7}{8}$	$5\frac{3}{4}$	25.0	34.9	39.0	41.0

Safe working loads of chain are one-half of proof test loads. Twist Coil Chain is made in all sizes from $\frac{1}{8}$ " to $\frac{3}{4}$ " inclusive. Conveyor or Sprocket Wheel Chain is made to any dimensions required, and in ordering give dimensions of links wanted, or preferably a sketch of same.

Chain

Standard
Stud-Link
Cable Chain



Standard
Close-Link
Cable Chain



Standard Stud-Link Cable Chain

Size of Chain, Inches	Length of Link, Inches	Width of Link, Inches	Weight of Chain, per Foot	Proof Test
t	l	W	Pounds	Tons
$\frac{3}{4}$	$4\frac{3}{8}$	$2\frac{3}{4}$	5.5	10.1
$\frac{1}{2}$	$4\frac{3}{4}$	3	6.3	12.0
$\frac{7}{8}$	5	$3\frac{1}{4}$	8.2	13.7
$\frac{1}{2}$	$5\frac{3}{8}$	$3\frac{1}{2}$	9.2	15.7
1	$5\frac{7}{8}$	$3\frac{3}{4}$	10.2	18.0
$1\frac{1}{16}$	$6\frac{1}{4}$	$3\frac{7}{8}$	11.5	20.3
$1\frac{1}{8}$	$6\frac{1}{2}$	$4\frac{1}{8}$	12.3	22.8
$1\frac{3}{16}$	$6\frac{3}{4}$	$4\frac{1}{4}$	13.5	25.5
$1\frac{1}{4}$	$7\frac{1}{8}$	$4\frac{1}{2}$	15.0	28.1
$1\frac{5}{16}$	$7\frac{3}{8}$	$4\frac{5}{8}$	16.2	31.0
$1\frac{3}{8}$	$7\frac{3}{4}$	$4\frac{7}{8}$	18.3	34.0
$1\frac{7}{16}$	$8\frac{1}{8}$	$5\frac{1}{8}$	18.8	37.2
$1\frac{1}{2}$	$8\frac{1}{2}$	$5\frac{3}{8}$	21.2	40.5
$1\frac{9}{16}$	$8\frac{7}{8}$	$5\frac{5}{8}$	23.8	44.0
$1\frac{5}{8}$	$9\frac{1}{4}$	$5\frac{7}{8}$	25.0	47.5
$1\frac{11}{16}$	$9\frac{5}{8}$	6	26.2	51.2
$1\frac{3}{4}$	10	$6\frac{1}{4}$	28.8	55.2
$1\frac{7}{8}$	$10\frac{1}{2}$	$6\frac{3}{4}$	33.8	63.3
$1\frac{13}{16}$	$10\frac{3}{4}$	7	35.8	67.5
2	$11\frac{1}{8}$	$7\frac{1}{4}$	38.8	72.0
$2\frac{1}{16}$	$11\frac{1}{2}$	$7\frac{1}{2}$	42.3	76.5
$2\frac{1}{8}$	12	$7\frac{3}{4}$	46.0	81.2
$2\frac{3}{16}$	$12\frac{1}{2}$	8	48.3	86.1
$2\frac{1}{4}$	13	$8\frac{1}{4}$	50.0	91.0

Safe working loads of chain are one-half of proof test loads.

JONES & LAUGHLIN STEEL COMPANY

Standard Close-Link Cable Chain

Size of Chain, Inches	Length of Link, Inches	Width of Link, Inches	Weight of Chain, per Foot	Proof Test
t	l	W	Pounds	Tons
1	4 $\frac{5}{8}$	3 $\frac{1}{2}$	10.3	12.0
1 $\frac{1}{16}$	5	3 $\frac{5}{8}$	11.8	12.5
1 $\frac{1}{8}$	5 $\frac{3}{8}$	3 $\frac{7}{8}$	12.7	15.1
1 $\frac{1}{4}$	5 $\frac{1}{2}$	4 $\frac{1}{8}$	13.7	16.9
1 $\frac{3}{8}$	5 $\frac{3}{4}$	4 $\frac{1}{4}$	15.2	18.7
1 $\frac{1}{2}$	6	4 $\frac{1}{2}$	16.5	20.6
1 $\frac{5}{8}$	6 $\frac{1}{4}$	4 $\frac{3}{4}$	18.8	22.6
1 $\frac{7}{8}$	6 $\frac{5}{8}$	5	19.7	24.7
1 $\frac{1}{2}$	6 $\frac{7}{8}$	5 $\frac{1}{4}$	21.7	27.0
1 $\frac{3}{4}$	7 $\frac{1}{4}$	5 $\frac{1}{2}$	23.0	29.2
1 $\frac{5}{8}$	7 $\frac{1}{2}$	5 $\frac{3}{4}$	25.3	31.6

Safe working loads of chain are one-half of proof test loads.

Properties of Sections

Definitions and Mathematical Expressions Used in Structural Designing

A = AREA OF SECTION, given in square inches.

I = MOMENT OF INERTIA. For any cross-section, the moment of inertia is the sum of the products obtained by multiplying the area of each particle in the cross-section by the square of its distance from the neutral axis.

r = RADIUS OF GYRATION. This may be defined as the distance from the neutral axis to the point at which, if all the area were concentrated, the moment of inertia would be the same.

The radius of gyration is used for ascertaining the safe load any section or shape will sustain when used in compression as a strut or column. The unbraced length of the section in inches, divided by the radius of gyration in inches is the working basis of all column formulae, commonly written $\frac{l}{r}$.

The value of the radius of gyration of any section is determined by the formulae, $r = \frac{\sqrt{I}}{A}$

NEUTRAL AXIS = Axis of moments through center of gravity of sections.

x-x and y-y = The neutral axis through center of gravity of unsymmetrical sections.

x and y = The distance from neutral axis x-x and y-y to the back or working line of this section.

S = SECTION MODULUS

The moment of inertia divided by the distance from axis to extreme fiber = $\frac{I}{n}$

The section modulus is used to determine the stress in the extreme fiber of a shape subject to bending, by dividing the bending moment by the section modulus, both expressed in like units of measurement.


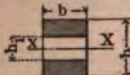
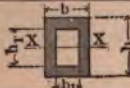
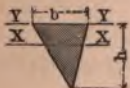




In an unsymmetrical section there are two section moduli for each axis, the least of which determines the safe unit stress.

The properties of steel sections are based upon the theoretical dimensions given in pages 11 to 45 inclusive. No account has been taken of fillets or rounded corners, neither have any approximations entered into any of the calculations.

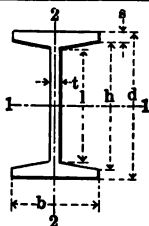
Values of Moments of Inertia

Various Sections

 I = Moment of Inertia S = Section Factor

Sections	I	S
	For axis X-X = $\frac{b h^3}{12}$ For axis Y-Y = $\frac{b h^3}{3}$	$\frac{b h^3}{6}$
	$\frac{b (h^3 - h_1^3)}{12}$	$\frac{b (h^3 - h_1^3)}{6 h}$
	$\frac{b h^3 - b_1 h_1^3}{12}$	$\frac{b h^3 - b_1 h_1^3}{6 h}$
	For axis X-X = $\frac{b h^3}{36}$ For axis Y-Y = $\frac{b h^3}{12}$	Min. = $\frac{b h^3}{24}$
	$\frac{\pi d^4}{64}$	$\frac{\pi d^3}{32}$
	$\frac{\pi (d^4 - d_1^4)}{64}$	$\frac{\pi (d^4 - d_1^4)}{32 d}$
	$\frac{\pi b h^3}{64}$	$\frac{\pi b h^2}{32}$
	$\frac{b h^3 - (b - b_1) h_1^3}{12}$	$\frac{2 I}{h}$

Values of Moments of Inertia Rolled Steel Sections

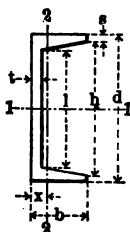


$$A = td + 2s(b - t) + \frac{(b - t)^2}{12}$$

$$I, \text{ Axis 1-1} = \frac{bd^3}{12} - \frac{h^4 - t^4}{8}$$

$$I', \text{ Axis 2-2} = \frac{b^3s}{6} + \frac{ht^3}{12} + \frac{b^4 - t^4}{288}$$

Slope of flange $= g = \frac{h - t}{b - t} = \frac{1}{6}$ for standard sections
 $h = d - 2s$ $l = h - g(b - t)$



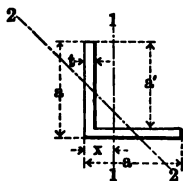
$$A = td + 2s(b - t) + \frac{(b - t)^2}{6}$$

$$X = \left[b^2s + \frac{ht^3}{2} + \frac{(b - t)^2(b + 2t)}{18} \right] \div A$$

$$I, \text{ Axis 1-1} = \frac{bd^3}{12} - \frac{h^4 - t^4}{16}$$

$$I', \text{ Axis 2-2} = \frac{1}{3} \left[2sb^3 + lt^3 + \frac{b^4 - t^4}{12} \right] - AX^2$$

Slope of flange $= g = \frac{h - t}{2(b - t)} = \frac{1}{6}$ for standard sections.
 $h = d - 2s$ $l = h - 2g(b - t)$



$$A = t(2a - t)$$

$$X = \frac{a^2 + at - t^2}{2(2a - t)}$$

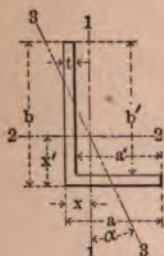
$$I, \text{ Axis 1-1} = \frac{t(a - x)^3 + ax^3 - (a - t)(x - t)^3}{3}$$

$$I', \text{ Axis 2-2} = \frac{2x^4 - 2(x - t)^4 + t \left[a - (2x - \frac{t}{2}) \right]^3}{3}$$

Values of Moments of Inertia

Rolled Steel Sections

Continued



$$A = t(a + b - t)$$

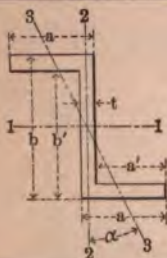
$$X = \frac{t(2a' + b) + a'^2}{2(a' + b)} \quad X' = \frac{t(2b' + a) + b'^2}{2(b' + a)}$$

$$\tan 2\alpha = - \frac{[(2x-t)b(b-2x') + (2x'-t)(a-t)(a+t-2x)]t}{2(l'-l)}$$

$$I, \text{ Axis } 1-1 = \frac{t(a-x)^3 + bx^3 - (b-t)(x-t)^3}{3}$$

$$I', \text{ Axis } 2-2 = \frac{t(b-x')^3 + ax'^3 - (a-t)(x'-t)^3}{3}$$

$$I'', \text{ Axis } 3-3 = \frac{I \cos^2 \alpha - I' \sin^2 \alpha}{\cos 2\alpha}$$



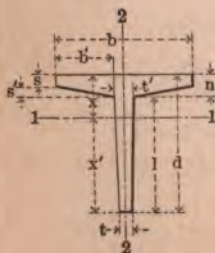
$$A = [b + 2(a-t)]t$$

$$\tan 2\alpha = - \frac{(bt - t^2)(a^2 - at)}{I - I'}$$

$$I, \text{ Axis } 1-1 = \frac{ab^3 - a'(b-2t)^3}{12}$$

$$I', \text{ Axis } 2-2 = \frac{b(a+a')^3 - 2a'^3b' - 6a'a^2b'}{12}$$

$$I'', \text{ Minimum, Axis } 3-3 = \frac{I \cos^2 \alpha - I' \sin^2 \alpha}{\cos 2\alpha}$$



$$A = \frac{l(t+t')}{2} + n t' + b'(s+n)$$

$$X = \frac{3s^2(b-t') + 2b's'(s'+3s) + 3t'd^2 - l(t'-l)(3d-l)}{6A}$$

$$I, \text{ Axis } 1-1 = \frac{l^3(3t+t') + 4bn^3 - 2b's'^3}{12} - A(x-n)^2$$

$$I', \text{ Axis } 2-2 = \frac{sb^3 + s't'^3 + ll^3}{12} + \frac{s'b'[2b'^2 + (2b' + 3t')^2]}{36}$$

$$+ \frac{l(t'-l)[(t'-l)^2 + 2(t'+2t)^2]}{144}$$

Compound Sections

Method of Finding Moments of Inertia, Radii of Gyration and Section Moduli

The moment of inertia I of a compound section about its neutral axis is equal to the sum of the moments of inertia I' , of its component parts about axes through their own centers of gravity and parallel to the neutral axis of the compound section, plus areas A' of the component parts multiplied by the squares of the distances d , of their own centers of gravity from the neutral axis of the compound section.

$$\text{Moment of inertia } I = I' + A'd^2$$

$$\text{Radius of gyration } r = \sqrt{\frac{I}{A}}$$

$$\text{Section modulus } S = \frac{I}{n}$$

Where n = distance of extreme fiber from neutral axis of compound section.

Example 1. Find the moments of inertia and radii of gyration about the axes X-X and Y-Y of a column section composed of

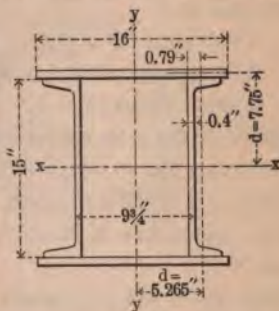
2 channels 15" \times 33 lbs. per ft.

2 cover plates 16" \times $\frac{1}{2}$ "

considering the gross area of section.

The properties of the component sections will be found tabulated in other parts of the book. Calculate the distances d from the neutral axes of the component sections

to the neutral axes X-X and Y-Y in accordance with dimensions given in sketch.



Axis X-X

$$I_{x-x} \text{ of 2-15" channels 33 lbs.} = 2 \times 312.6 = 625.20 \text{ inches}^4$$

$$I_{x-x} \text{ of 2-16} \times \frac{1}{2}" \text{ plates} = 2 \times \frac{16 \times 0.5^3}{12} = .33 \text{ inches}^4$$

$$Ad^2 \text{ of 2-16} \times \frac{1}{2}" \text{ plates} = 2 \times 8 \times 7.75^2 = 961.00 \text{ inches}^4$$

$$\text{Moment of inertia—gross section} = 1586.53 \text{ inches}^4$$

$$\text{Radius of gyration—gross section} = \sqrt{\frac{1586.53}{35.8}} = 6.66 \text{ inches}$$

Compound Sections

Continued

Axis Y-Y

$$I_{y-y} \text{ of } 2\text{-}15'' \text{ channels } 33 \text{ lbs.} = 2 \times 8.2 = 16.40 \text{ inches}^4$$

$$Ad^2 \text{ of } 2\text{-}15'' \text{ channels } 33 \text{ lbs.} = 2 \times 9.9 \times 5.265^2 = 548.86 \text{ inches}^4$$

$$I_{y-y} \text{ of } 2\text{-}16 \times \frac{1}{2} \text{ plates} = 2 \times \frac{0.5 \times 16^3}{12} = 341.33 \text{ inches}^4$$

$$\text{Moment of inertia—gross section} = 906.59 \text{ inches}^4$$

$$\text{Radius of gyration—gross section} = \sqrt{\frac{906.59}{35.8}} = 5.03 \text{ inches}$$

Example 2. Find the moments of inertia and section moduli about the axes X-X and Y-Y of a girder section composed of

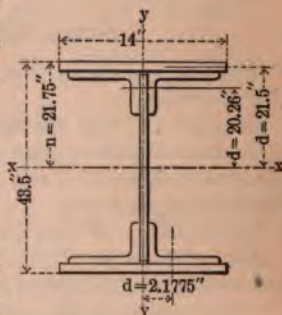
1 web plate $42'' \times \frac{3}{8}''$

4 flange angles $6 \times 4 \times \frac{1}{2}''$

2 flange plates $14 \times \frac{1}{2}''$

considering the gross area of section.

Calculate the distances d from the neutral axes of the component sections to the neutral axes X-X and Y-Y.



Axis X-X

$$I_{x-x} \text{ of } 4\text{-}6 \times 4 \times \frac{1}{2} \text{ angles} = 4 \times 6.3 = 25.20 \text{ inches}^4$$

$$Ad^2 \text{ of } 4\text{-}6 \times 4 \times \frac{1}{2} \text{ angles} = 4 \times 4.75 \times 20.26^2 = 7798.88 \text{ inches}^4$$

$$I_{x-x} \text{ of } 1\text{-}42 \times \frac{3}{8} \text{ plate} = 1 \times \frac{0.375 \times 42^3}{12} = 2315.25 \text{ inches}^4$$

$$I_{x-x} \text{ of } 2\text{-}14 \times \frac{1}{2} \text{ plates} = 2 \times \frac{14 \times 0.5^3}{12} = .29 \text{ inches}^4$$

$$Ad^2 \text{ of } 2\text{-}14 \times \frac{1}{2} \text{ plates} = 2 \times 7 \times 21.5^2 = 6471.50 \text{ inches}^4$$

$$\text{Moment of inertia—gross section} = 16611.12 \text{ inches}^4$$

$$\text{Section modulus—gross section} = \frac{16611.2}{21.75} = 763.72 \text{ inches}^3$$

Compound Sections

Continued

Axis Y-Y

$$I_{y-y} \text{ of } 4-6 \times 4 \times \frac{1}{2} \text{ angles} = 4 \times 17.4 = 69.60 \text{ inches}^4$$

$$Ad^2 \text{ of } 4-6 \times 4 \times \frac{1}{2} \text{ angles} = 4 \times 4.75 \times 2.1775^2 = 90.09 \text{ inches}^4$$

$$I_{y-y} \text{ of } 1-42 \times \frac{3}{8} \text{ plate} = 1 \times \frac{42 \times 0.375^3}{12} = .49 \text{ inches}^4$$

$$I_{y-y} \text{ of } 2-14 \times \frac{1}{2} \text{ plates} = 2 \times \frac{0.5 \times 14^3}{12} = 228.67 \text{ inches}^4$$

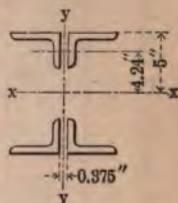
$$\text{Moment of inertia—gross section} = 388.85 \text{ inches}^4$$

$$\text{Section modulus—gross section} = \frac{388.85}{7} = 55.55 \text{ inches}$$

To find the moment of inertia of the net section calculate the moments of inertia of the areas of the rivet holes about the neutral axis of the compound section and deduct their sum from the moment of inertia of the gross section as determined above.

Example 3. Find the radii of gyration about axes X-X and Y-Y of a latticed column composed of

4-4 × 3 × $\frac{5}{16}$ angles with $\frac{3}{8}$ " lattice bars considering gross section of angles, no allowance being made for lattice bars. Calculate the distance *d* from the neutral axis of the angles to the neutral axis X-X.



Axis X-X

$$I_{x-x} \text{ of } 4-4 \times 3 \times \frac{5}{16} \text{ angles} = 4 \times 1.7 = 6.8 \text{ inches}^4$$

$$Ad^2 \text{ of } 4-4 \times 3 \times \frac{5}{16} \text{ angles} = 4 \times 2.09 \times 4.24^2 = 150.29 \text{ inches}^4$$

$$\text{Moment of inertia—gross section} = 157.09 \text{ inches}^4$$

$$\text{Radius of gyration—gross section} = \sqrt{\frac{157.09}{8.36}} = 4.34 \text{ inches}$$

Axis Y-Y

I_{y-y} of 4-4 × 3 × $\frac{5}{16}$ angles = 1.93. See tables of radii of gyration for 2 angles placed back to back (page 209).

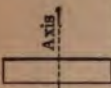
Moments of Inertia of Rectangles



Depth, Inches		Width of Rectangle, Inches								
		$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{3}{4}$	1
5		2.60	3.26	3.91	4.56	5.21	5.86	6.51	7.81	10.42
6		4.50	5.63	6.75	7.88	9.00	10.13	11.25	13.50	18.00
7		7.15	8.93	10.72	12.51	14.29	16.08	17.86	21.44	28.58
8		10.67	13.33	16.00	18.67	21.33	24.00	26.67	32.00	42.67
9		15.19	18.98	22.78	26.58	30.38	34.17	37.97	45.56	60.75
10		20.83	26.04	31.25	36.46	41.67	46.87	52.08	62.50	83.33
11		27.73	34.66	41.59	48.53	55.46	62.39	69.32	83.19	110.92
12		36.00	45.00	54.00	63.00	72.00	81.00	90.00	108.00	144.00
13		45.77	57.21	68.66	80.10	91.54	102.98	114.43	137.31	183.08
14		57.17	71.46	85.75	100.04	114.33	128.63	142.92	171.50	228.67
15		70.31	87.89	105.47	123.05	140.63	158.20	175.78	210.94	281.25
16		85.33	106.67	128.00	149.33	170.67	192.00	213.33	256.00	341.33
17		102.35	127.94	153.53	179.12	204.71	230.30	255.89	307.06	409.42
18		121.50	151.88	182.25	212.63	243.00	273.38	303.75	364.50	486.00
19		142.90	178.62	214.34	250.07	285.79	321.52	357.24	428.69	571.58
20		166.67	208.33	250.00	291.67	333.33	375.00	416.67	500.00	666.67
21		192.94	241.17	289.41	337.64	385.88	434.11	482.34	578.81	771.75
22		221.83	277.29	332.75	388.21	443.67	499.13	554.58	665.50	887.33
23		253.48	316.85	380.22	443.59	506.96	570.33	633.70	760.44	1013.92
24		288.00	360.00	432.00	504.00	576.00	648.00	720.00	864.00	1152.00

Moments of Inertia of Rectangles

Continued


 Neutral Axis

Depth, Inches	WIDTH OF RECTANGLE, INCHES							
	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{3}{4}$
25	325.52	406.90	488.28	569.66	651.04	732.42	813.80	976.56
26	366.17	457.71	549.25	640.79	732.33	823.88	915.42	1098.50
27	410.06	512.58	615.09	717.61	820.13	922.64	1025.16	1230.19
28	457.33	571.67	686.00	800.33	914.67	1029.00	1143.33	1372.00
29	508.10	635.13	762.16	889.18	1016.21	1143.23	1270.26	1524.31
30	562.50	703.13	843.75	984.38	1125.00	1265.63	1406.25	1687.50
31	620.65	775.81	930.97	1086.13	1241.30	1396.46	1551.62	1861.95
32	682.67	853.33	1024.00	1194.67	1365.33	1536.00	1706.67	2048.00
33	748.69	935.86	1123.03	1310.20	1497.38	1684.55	1871.72	2246.07
34	818.83	1023.54	1228.25	1432.96	1637.67	1842.38	2047.08	2456.50
35	893.23	1116.54	1339.84	1563.15	1786.46	2009.76	2233.07	2679.69
36	972.00	1215.00	1458.00	1701.00	1944.00	2187.00	2430.00	2916.00
37	1055.27	1319.09	1582.90	1846.72	2110.54	2374.35	2638.17	3165.81
38	1143.17	1428.96	1714.75	2000.54	2286.33	2572.13	2857.92	3429.50
39	1235.81	1544.77	1853.72	2162.67	2471.62	2780.58	3089.53	3707.43
								4943.24

Moments of Inertia of Rectangles Continued

Neutral Axis

WIDTH OF RECTANGLE, INCHES

Depth, Inches	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{3}{4}$	1
40	1333.33	1666.67	2000.00	2333.33	2666.67	3000.00	3333.33	4000.00	5333.33
41	1435.85	1794.82	2153.78	2512.75	2871.71	3230.69	3589.64	4307.56	5743.42
42	1543.50	1929.38	2315.25	2701.13	3087.00	3472.88	3858.75	4630.50	6174.00
43	1656.39	2070.49	2484.59	2898.68	3312.79	3726.89	4140.98	4969.18	6625.59
44	1774.67	2218.33	2662.00	3105.67	3549.33	3993.00	4436.67	5324.00	7098.67
45	1898.44	2373.05	2847.66	3322.27	3796.88	4271.48	4746.09	5695.31	7593.75
46	2027.83	2534.79	3041.75	3548.71	4055.67	4562.63	5069.58	6083.50	8111.33
47	2162.98	2703.73	3244.47	3785.22	4325.96	4866.71	5407.45	6488.94	8651.92
48	2304.00	2880.00	3456.00	4032.00	4608.00	5184.00	5760.00	6912.00	9216.00

Properties of Structural Beams



Section Index	Depth of Beam, In.	Weight per Foot, Lbs.	Area of Section, Sq. In.	Width of Flange, In.	Thickness of Web, In.	AXIS X-X			AXIS Y-Y		
						I	r In.	S	I	r In.	S
B-0	24	115.0	33.98	8.000	0.750	2955.5	9.33	246.3	83.2	1.57	20.8
B-1		110.0	32.48	7.938	0.688	2883.5	9.42	240.3	81.0	1.58	20.4
B-2		105.0	30.98	7.875	0.625	2811.5	9.53	234.3	78.9	1.60	20.0
B-3	24	100.0	29.41	7.254	0.754	2379.6	9.00	198.3	48.6	1.28	13.4
B-4		95.0	27.94	7.193	0.693	2309.0	9.09	192.4	47.1	1.30	13.1
B-5		90.0	26.47	7.131	0.631	2238.4	9.20	186.5	45.7	1.31	12.8
B-6		85.0	25.00	7.070	0.570	2167.8	9.31	180.7	44.4	1.33	12.6
B-7		80.0	23.32	7.000	0.500	2087.2	9.46	173.9	42.9	1.36	12.3
B-12	20	100.0	29.41	7.284	0.884	1655.6	7.50	165.6	52.7	1.34	14.5
B-13		95.0	27.94	7.210	0.810	1606.6	7.58	160.7	50.8	1.35	14.1
B-14		90.0	26.47	7.137	0.737	1557.6	7.67	155.8	49.0	1.36	13.7
B-15		85.0	25.00	7.063	0.663	1508.5	7.77	150.9	47.3	1.37	13.4
B-16		80.0	23.73	7.000	0.600	1466.3	7.86	146.6	45.8	1.39	13.1
B-20	20	75.0	22.06	6.399	0.649	1268.8	7.58	126.9	30.3	1.17	9.5
B-21		70.0	20.59	6.325	0.575	1219.8	7.70	122.0	29.0	1.19	9.2
B-22		65.0	19.08	6.250	0.500	1169.5	7.83	117.0	27.9	1.21	8.9
*B-23	18	90.0	26.47	7.245	0.807	1260.4	6.90	140.0	52.0	1.40	14.4
*B-24		85.0	25.00	7.163	0.725	1220.7	6.99	135.6	50.0	1.42	14.0
*B-25		80.0	23.53	7.082	0.644	1181.0	7.09	131.2	48.1	1.43	13.6
*B-26		75.0	22.05	7.000	0.562	1141.3	7.19	126.8	46.2	1.45	13.2
B-27	18	70.0	20.59	6.259	0.719	921.2	6.69	102.4	24.6	1.09	7.9
B-28		65.0	19.12	6.177	0.637	881.5	6.79	97.9	23.5	1.11	7.6
B-29		60.0	17.65	6.095	0.555	841.8	6.91	93.5	22.4	1.13	7.3
B-30		55.0	15.93	6.000	0.460	795.6	7.07	88.4	21.2	1.15	7.1
B-44	15	75.0	22.06	6.292	0.882	691.2	5.60	92.2	30.7	1.18	9.8
B-45		70.0	20.59	6.194	0.784	663.7	5.68	88.5	29.0	1.19	9.4
B-46		65.0	19.12	6.096	0.686	636.1	5.77	84.8	27.4	1.20	9.0
B-47		60.0	17.67	6.000	0.590	609.0	5.87	81.2	26.0	1.21	8.7
B-52	15	55.0	16.18	5.746	0.656	511.0	5.62	68.1	17.1	1.02	5.9
B-53		50.0	14.71	5.648	0.558	483.4	5.73	64.5	16.0	1.04	5.7
B-54		45.0	13.24	5.550	0.460	455.9	5.87	60.8	15.1	1.07	5.4
B-55		42.0	12.48	5.500	0.410	441.8	5.95	58.9	14.6	1.08	5.3

*Proposed Sections—Inserted for reference only.

Properties of Structural Beams

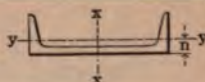
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Section Index	Depth of Beam, In.	Weight per Foot, Lbs.	Area of Section, Sq. In.	Width of Flange, In.	Thickness of Web, In.	AXIS X-X			AXIS Y-Y		
						I	r, In.	S	I	r, In.	S
B-60	12	55.0	16.18	5.611	0.821	321.0	4.45	53.5	17.5	1.04	6.2
B-61		50.0	14.71	5.489	0.699	303.4	4.54	50.6	16.1	1.05	5.9
B-62		45.0	13.24	5.366	0.576	285.7	4.65	47.6	14.9	1.06	5.6
B-63		40.0	11.84	5.250	0.460	269.0	4.77	44.8	13.8	1.08	5.3
B-68	12	35.0	10.29	5.086	0.436	228.3	4.71	38.0	10.1	0.99	4.0
B-69		31.5	9.26	5.000	0.350	215.8	4.83	36.0	9.5	1.01	3.8
B-74	10	40.0	11.76	5.099	0.749	158.7	3.67	31.7	9.5	0.90	3.7
B-75		35.0	10.29	4.952	0.602	146.4	3.77	29.3	8.5	0.91	3.4
B-76		30.0	8.82	4.805	0.455	134.2	3.90	26.8	7.7	0.93	3.2
B-77		25.0	7.37	4.660	0.310	122.1	4.07	24.4	6.9	0.97	3.0
B-82	9	35.0	10.29	4.772	0.732	111.8	3.29	24.8	7.3	0.84	3.1
B-83		30.0	8.82	4.609	0.569	101.9	3.40	22.6	6.4	0.85	2.8
B-84		25.0	7.35	4.446	0.406	91.9	3.54	20.4	5.7	0.88	2.5
B-85		21.0	6.18	4.315	0.275	84.0	3.68	18.7	5.2	0.90	2.4
B-90	8	25.5	7.50	4.271	0.541	68.4	3.02	17.1	4.8	0.80	2.2
B-91		23.0	6.76	4.179	0.449	64.5	3.09	16.1	4.4	0.81	2.1
B-92		20.5	6.03	4.087	0.357	60.6	3.17	15.2	4.1	0.82	2.0
B-93		18.0	5.33	4.000	0.270	56.9	3.27	14.2	3.8	0.84	1.9
B-98	7	20.0	5.88	3.868	0.458	42.2	2.68	12.1	3.2	0.74	1.7
B-99		17.5	5.15	3.763	0.353	39.2	2.76	11.2	2.9	0.76	1.6
B-100		15.0	4.42	3.660	0.250	36.2	2.86	10.4	2.7	0.78	1.5
B-105	6	17.25	5.07	3.575	0.475	26.2	2.27	8.7	2.4	0.68	1.3
B-106		14.75	4.34	3.452	0.352	24.0	2.35	8.0	2.1	0.69	1.2
B-107		12.25	3.61	3.330	0.230	21.8	2.46	7.3	1.9	0.72	1.1
B-112	5	14.75	4.34	3.294	0.504	15.2	1.87	6.1	1.7	0.63	1.0
B-113		12.25	3.60	3.147	0.357	13.6	1.94	5.5	1.5	0.63	0.92
B-114		9.75	2.87	3.000	0.210	12.1	2.05	4.8	1.2	0.65	0.82
B-119	4	10.5	3.09	2.880	0.410	7.1	1.52	3.6	1.0	0.57	0.70
B-120		9.5	2.79	2.807	0.337	6.8	1.55	3.4	0.93	0.58	0.66
B-121		8.5	2.50	2.733	0.263	6.4	1.59	3.2	0.85	0.58	0.62
B-122		7.5	2.21	2.660	0.190	6.0	1.64	3.0	0.77	0.59	0.58
B-127	3	7.5	2.21	2.521	0.361	2.9	1.15	1.9	0.60	0.52	0.48
B-128		6.5	1.91	2.423	0.263	2.7	1.19	1.8	0.53	0.52	0.44
B-129		5.5	1.63	2.330	0.170	2.5	1.23	1.7	0.46	0.53	0.40

JONES & LAUGHLIN STEEL COMPANY

Properties of Structural Channels



Section Index	Depth of Channel, In.	Wgt. per Foot, Lbs.	Area of Section, Sq. In.	Width of Flange, In.	Thickness of Web, In.	Axis X-X			Axis Y-Y			n In.
						I	r In.	S	I	r In.	S	
C-3	15	55.0	16.18	3.818	0.818	430.2	5.16	57.4	12.2	0.87	4.1	0.82
C-4		50.0	14.71	3.720	0.720	402.7	5.23	53.7	11.2	0.87	3.8	0.80
C-5		45.0	13.24	3.622	0.622	375.1	5.32	50.0	10.3	0.88	3.6	0.79
C-6		40.0	11.76	3.524	0.524	347.5	5.43	46.3	9.4	0.89	3.4	0.78
C-7		35.0	10.29	3.426	0.426	319.9	5.53	42.7	8.5	0.91	3.2	0.79
C-8		33.0	9.90	3.400	0.400	312.6	5.62	41.7	8.2	0.91	3.2	0.79
C-23	12	40.0	11.76	3.418	0.758	196.9	4.09	32.8	6.6	0.75	2.5	0.72
C-24		35.0	10.29	3.296	0.636	179.3	4.17	29.9	5.9	0.76	2.3	0.69
C-25		30.0	8.82	3.173	0.513	161.7	4.28	26.9	5.2	0.77	2.1	0.68
C-26		25.0	7.35	3.050	0.390	144.0	4.43	24.0	4.5	0.79	1.9	0.68
C-27		20.5	6.03	2.940	0.280	128.1	4.61	21.4	3.9	0.81	1.7	0.70
C-32	10	35.0	10.29	3.183	0.823	115.5	3.35	23.1	4.7	0.67	1.9	0.70
C-33		30.0	8.82	3.036	0.676	103.2	3.42	20.7	4.0	0.67	1.7	0.65
C-34		25.0	7.35	2.889	0.529	91.0	3.52	18.2	3.4	0.68	1.5	0.62
C-35		20.0	5.88	2.742	0.382	78.7	3.66	15.7	2.9	0.70	1.3	0.61
C-36		15.0	4.46	2.600	0.240	66.9	3.87	13.4	2.3	0.72	1.2	0.64
C-41	9	25.0	7.35	2.815	0.615	70.7	3.10	15.7	3.0	0.64	1.4	0.62
C-42		20.0	5.88	2.652	0.452	60.8	3.21	13.5	2.5	0.65	1.2	0.59
C-43		15.0	4.41	2.488	0.288	50.9	3.40	11.3	2.0	0.67	1.0	0.59
C-44		13.25	3.89	2.430	0.230	47.3	3.49	10.5	1.8	0.67	0.97	0.61
C-49	8	21.25	6.25	2.622	0.582	47.8	2.77	11.9	2.3	0.60	1.1	0.59
C-50		18.75	5.51	2.530	0.490	43.8	2.82	11.0	2.0	0.60	1.0	0.57
C-51		16.25	4.78	2.439	0.399	39.9	2.89	10.0	1.8	0.61	0.95	0.56
C-52		13.75	4.04	2.347	0.307	36.0	2.98	9.0	1.6	0.62	0.87	0.56
C-53		11.25	3.35	2.260	0.220	32.3	3.11	8.1	1.3	0.63	0.79	0.58
C-58	7	19.75	5.81	2.513	0.633	33.2	2.39	9.5	1.9	0.56	0.96	0.58
C-59		17.25	5.07	2.408	0.528	30.2	2.44	8.6	1.6	0.57	0.87	0.56
C-60		14.75	4.34	2.303	0.423	27.2	2.50	7.8	1.4	0.57	0.79	0.54
C-61		12.25	3.60	2.198	0.318	24.2	2.59	6.9	1.2	0.58	0.71	0.53
C-62		9.75	2.85	2.090	0.210	21.1	2.72	6.0	0.98	0.59	0.63	0.55
C-67	6	15.5	4.56	2.283	0.563	19.5	2.07	6.5	1.3	0.53	0.74	0.55
C-68		13.0	3.82	2.160	0.440	17.3	2.13	5.8	1.1	0.53	0.65	0.52
C-69		10.5	3.09	2.038	0.318	15.1	2.21	5.0	0.88	0.53	0.57	0.50
C-70		8.0	2.38	1.920	0.200	13.0	2.34	4.3	0.70	0.54	0.50	0.52
C-75	5	11.5	3.38	2.037	0.477	10.4	1.75	4.2	0.82	0.49	0.54	0.51
C-76		9.0	2.65	1.890	0.330	8.9	1.83	3.6	0.64	0.49	0.45	0.48
C-77		6.5	1.95	1.750	0.190	7.4	1.95	3.0	0.48	0.50	0.38	0.49
C-82	4	7.25	2.13	1.725	0.325	4.6	1.46	2.3	0.44	0.46	0.35	0.46
C-83		6.25	1.84	1.652	0.252	4.2	1.51	2.1	0.38	0.45	0.32	0.46
C-84		5.25	1.55	1.580	0.180	3.8	1.56	1.9	0.32	0.45	0.29	0.46
C-89	3	6.0	1.76	1.602	0.362	2.1	1.08	1.4	0.31	0.42	0.27	0.46
C-90		5.0	1.47	1.504	0.264	1.8	1.12	1.2	0.25	0.42	0.24	0.44
C-91		4.0	1.19	1.410	0.170	1.6	1.17	1.1	0.20	0.41	0.21	0.44

Properties of Ship Channels



Section Index	Depth of Channel, Inches	Weight per foot, Pounds	Area of Section, Square Inches	Thickness of Webb, Inches	Width of Flange, Inches	Moment of Inertia Neutral Axis Perpendicular to Web at Center	Moment of Inertia Neutral Axis Parallel with Center Line of Web	Radius of Gyration Neutral Axis Perpendicular to Web at Center	Radius of Gyration Neutral Axis Parallel with Center Line of Web	Section Factor Neutral Axis Perpendicular to Web at Center	Distance of Center of Grav- ity from Outside of Web
C-12	13	52.5	15.45	.848	4.473	324.2	17.4	4.58	1.06	49.9	0.99
C-13		50.	14.71	.791	4.416	313.8	16.7	4.62	1.07	48.3	0.98
C-14		45.	13.24	.678	4.303	293.1	15.3	4.71	1.08	45.1	0.97
C-15		40.	11.76	.565	4.190	272.3	13.9	4.81	1.09	41.9	0.97
C-16		37.5	11.04	.509	4.134	262.1	13.4	4.87	1.10	40.3	0.98
C-17		35.	10.29	.452	4.077	251.6	12.5	4.95	1.10	38.7	0.99
C-18		32.	9.41	.384	4.009	239.2	11.7	5.04	1.11	36.8	1.01
C-19	10	31.5	9.26	.372	3.997	237.0	11.5	5.06	1.12	36.5	1.01
C-101		27.2	8.00	.500	3.500	109.4	7.8	3.70	0.99	21.9	0.89
C-102		25.0	7.37	.437	3.437	104.1	7.3	3.76	0.99	20.8	0.89
C-105	10	21.8	6.38	.375	3.375	91.3	6.2	3.78	0.99	18.3	0.87
C-107	9	34.7	10.21	.652	4.002	115.5	13.8	3.36	1.16	25.7	1.16
C-108		31.7	9.31	.552	3.902	109.5	12.6	3.43	1.16	24.3	1.17
C-109		28.6	8.41	.450	3.800	103.4	11.4	3.51	1.16	23.0	1.19
C-114	8	26.5	7.80	.602	3.602	67.8	8.2	2.95	1.03	17.0	0.98
C-115		25.2	7.40	.552	3.552	65.7	7.8	2.98	1.03	16.4	0.98
C-116		23.8	7.00	.500	3.500	63.6	7.4	3.01	1.03	15.9	0.99
C-117	8	24.2	7.10	.500	3.600	65.0	8.1	3.03	1.06	16.3	1.02
C-118		22.8	6.70	.450	3.550	62.9	7.6	3.06	1.07	15.7	1.03
C-119		21.4	6.30	.400	3.500	60.7	7.2	3.10	1.07	15.2	1.05
C-121	7	22.1	6.50	.500	3.500	46.0	7.1	2.66	1.05	13.2	1.05
C-122		20.0	5.88	.412	3.412	43.5	6.4	2.72	1.04	12.4	1.06
C-123		18.0	5.30	.328	3.328	41.1	5.8	2.79	1.04	11.7	1.09
C-128	6	18.1	5.33	.563	3.063	25.4	3.5	2.18	0.82	8.5	0.80
C-129		16.8	4.95	.500	3.000	24.3	3.3	2.22	0.82	8.1	0.79
C-130		15.5	4.57	.437	2.936	23.2	3.1	2.25	0.82	7.7	0.79
C-131	6	14.3	4.20	.375	2.874	22.0	2.8	2.29	0.82	7.3	0.80
C-132		13.0	3.83	.313	2.813	20.9	2.6	2.34	0.82	7.0	0.81
C-137		15.0	4.46	.350	3.500	25.0	5.2	2.37	1.08	8.3	1.08

Properties of Angles

Equal Legs

Continued



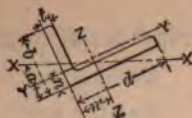
Section Index	Dimensions, Inches $h \times h$	Thickness, Inches t	Weight per Foot, Pounds	Area of Section, Square Inches A	Distance of Center of Gravity from Back of Leg, Inches n	Moment of Inertia, Axis Y-Y I	Section Factor, Axis Y-Y S	Radius of Gyration, Axis Y-Y, Inches r	Least Radius of Gyration, Axis X-X r^x
A-130	$2\frac{1}{2} \times 2\frac{1}{2}$	$\frac{1}{2}$	7.7	2.25	0.81	1.2	0.73	0.74	0.47
A-131	$2\frac{1}{2} \times 2\frac{1}{2}$	$\frac{7}{16}$	6.8	2.00	0.78	1.1	0.65	0.75	0.48
A-132	$2\frac{1}{2} \times 2\frac{1}{2}$	$\frac{3}{8}$	5.9	1.73	0.76	0.98	0.57	0.75	0.48
A-133	$2\frac{1}{2} \times 2\frac{1}{2}$	$\frac{5}{16}$	5.0	1.47	0.74	0.85	0.48	0.76	0.49
A-134	$2\frac{1}{2} \times 2\frac{1}{2}$	$\frac{1}{4}$	4.1	1.19	0.72	0.70	0.39	0.77	0.49
A-135	$2\frac{1}{2} \times 2\frac{1}{2}$	$\frac{3}{16}$	3.07	0.90	0.69	0.55	0.30	0.78	0.49
A-140	$2\frac{1}{2} \times 2\frac{1}{2}$	$\frac{1}{8}$	2.08	0.61	0.67	0.38	0.20	0.79	0.50
A-160	2×2	$\frac{1}{2}$	6.0	1.75	0.68	0.59	0.45	0.58	0.39
A-161	2×2	$\frac{7}{16}$	5.3	1.56	0.66	0.54	0.40	0.59	0.39
A-162	2×2	$\frac{3}{8}$	4.7	1.36	0.64	0.48	0.35	0.59	0.39
A-163	2×2	$\frac{5}{16}$	3.92	1.15	0.61	0.42	0.30	0.60	0.39
A-164	2×2	$\frac{1}{4}$	3.19	0.94	0.59	0.35	0.25	0.61	0.40
A-165	2×2	$\frac{3}{16}$	2.44	0.71	0.57	0.27	0.19	0.62	0.40
A-170	2×2	$\frac{1}{8}$	1.65	0.48	0.55	0.19	0.13	0.63	0.39
A-189	$1\frac{1}{2} \times 1\frac{1}{2}$	$\frac{3}{8}$	3.35	0.98	0.51	0.19	0.19	0.44	0.29
A-190	$1\frac{1}{2} \times 1\frac{1}{2}$	$\frac{5}{16}$	2.86	0.84	0.49	0.16	0.16	0.44	0.29
A-191	$1\frac{1}{2} \times 1\frac{1}{2}$	$\frac{1}{4}$	2.34	0.69	0.47	0.14	0.13	0.45	0.29
A-192	$1\frac{1}{2} \times 1\frac{1}{2}$	$\frac{3}{16}$	1.80	0.53	0.44	0.11	0.10	0.46	0.29
A-197	$1\frac{1}{2} \times 1\frac{1}{2}$	$\frac{1}{8}$	1.23	0.36	0.42	0.08	0.07	0.46	0.30
A-224	1×1	$\frac{1}{4}$	1.49	0.44	0.34	0.04	0.06	0.29	0.19
A-225	1×1	$\frac{3}{16}$	1.16	0.34	0.32	0.03	0.04	0.30	0.19
A-226	1×1	$\frac{1}{8}$	0.80	0.23	0.30	0.02	0.03	0.31	0.19

Properties of Angles

Unequal Legs

Section Index	Dimensions, Inches	Thickness, Inches	Weight per Foot, Pounds	Area of Section, Square Inches	Distance of Center of Gravity from Back of Longer Leg, Inches	Moment of Inertia, Axis Y—Y
	d x b	t		A	n	I
A-233	8 x 6	$1\frac{1}{8}$	49.3	14.50	1.70	42.4
A-234	8 x 6	$1\frac{1}{16}$	46.8	13.77	1.68	40.7
A-235	8 x 6	1	44.2	13.00	1.65	38.8
A-236	8 x 6	$\frac{15}{16}$	41.7	12.25	1.63	36.8
A-237	8 x 6	$\frac{7}{8}$	39.1	11.48	1.61	34.9
A-238	8 x 6	$\frac{13}{16}$	36.5	10.72	1.59	32.8
A-239	8 x 6	$\frac{3}{4}$	33.8	9.94	1.56	30.7
A-240	8 x 6	$\frac{11}{16}$	31.2	9.15	1.54	28.6
A-241	8 x 6	$\frac{5}{8}$	28.5	8.36	1.52	26.3
A-242	8 x 6	$\frac{9}{16}$	25.7	7.56	1.50	24.0
A-243	8 x 6	$\frac{1}{2}$	23.0	6.75	1.47	21.7
A-650	8 x 6	$\frac{7}{16}$	20.2	5.94	1.45	19.4
A-244	7 x $3\frac{1}{2}$	$\frac{7}{8}$	28.7	8.42	0.91	6.8
A-245	7 x $3\frac{1}{2}$	$\frac{13}{16}$	26.8	7.87	0.89	6.5
A-246	7 x $3\frac{1}{2}$	$\frac{3}{4}$	24.9	7.31	0.87	6.1
A-247	7 x $3\frac{1}{2}$	$\frac{11}{16}$	23.0	6.75	0.85	5.7
A-248	7 x $3\frac{1}{2}$	$\frac{5}{8}$	21.0	6.17	0.82	5.3
A-249	7 x $3\frac{1}{2}$	$\frac{9}{16}$	19.1	5.59	0.80	4.9
A-250	7 x $3\frac{1}{2}$	$\frac{1}{2}$	17.0	5.00	0.78	4.4
A-251	7 x $3\frac{1}{2}$	$\frac{7}{16}$	15.0	4.40	0.75	4.0
A-252	7 x $3\frac{1}{2}$	$\frac{3}{8}$	13.0	3.81	0.72	3.6
A-258	6 x 4	$\frac{13}{16}$	25.4	7.47	1.10	9.2
A-259	6 x 4	$\frac{3}{4}$	23.6	6.94	1.08	8.7
A-260	6 x 4	$\frac{11}{16}$	21.8	6.40	1.06	8.1
A-261	6 x 4	$\frac{5}{8}$	20.0	5.86	1.03	7.5
A-262	6 x 4	$\frac{9}{16}$	18.1	5.31	1.01	6.9
A-263	6 x 4	$\frac{1}{2}$	16.2	4.75	0.99	6.3
A-264	6 x 4	$\frac{7}{16}$	14.3	4.18	0.96	5.6
A-265	6 x 4	$\frac{3}{8}$	12.3	3.61	0.94	4.9

JONES & LAUGHLIN STEEL COMPANY



Section Factor Axis Y-Y	Radius of Gyration Axis Y-Y, Inches	Distance of Center of Gravity from Back of Shorter Leg, Inches n'	Moment of Inertia Axis Z-Z	Section Factor Axis Z-Z	Radius of Gyration Axis Z-Z	Least Radius of Gyration Axis X-X, Inches	Section Index
S	r	n'	I'	S'	r'	r''	
9.9	1.71	2.70	88.8	16.7	2.47	1.27	A-233
9.4	1.72	2.68	84.9	15.9	2.48	1.27	A-234
8.9	1.73	2.65	80.8	15.1	2.49	1.28	A-235
8.4	1.73	2.63	76.6	14.3	2.50	1.28	A-236
7.9	1.74	2.61	72.3	13.4	2.51	1.28	A-237
7.4	1.75	2.59	67.9	12.5	2.52	1.29	A-238
6.9	1.76	2.56	63.4	11.7	2.53	1.29	A-239
6.4	1.77	2.54	58.8	10.8	2.54	1.29	A-240
5.9	1.77	2.52	54.1	9.9	2.54	1.30	A-241
5.3	1.78	2.50	49.3	8.9	2.55	1.30	A-242
4.8	1.79	2.47	44.3	8.0	2.56	1.30	A-243
4.3	1.80	2.45	39.4	7.1	2.57	1.31	A-650
2.6	0.90	2.66	40.8	9.4	2.20	0.74	A-244
2.5	0.91	2.64	38.4	8.8	2.21	0.74	A-245
2.3	0.91	2.62	36.0	8.2	2.22	0.74	A-246
2.1	0.92	2.60	33.5	7.6	2.23	0.74	A-247
2.0	0.93	2.57	30.9	7.0	2.24	0.75	A-248
1.8	0.93	2.55	28.2	6.3	2.25	0.75	A-249
1.6	0.94	2.53	25.4	5.7	2.25	0.75	A-250
1.4	0.95	2.50	22.6	5.0	2.26	0.76	A-251
1.2	0.96	2.48	19.8	4.3	2.26	0.77	A-252
3.2	1.11	2.10	26.1	6.7	1.87	0.86	A-258
3.0	1.12	2.08	24.5	6.2	1.88	0.86	A-259
2.8	1.13	2.06	22.8	5.8	1.89	0.86	A-260
2.5	1.13	2.03	21.1	5.3	1.90	0.86	A-261
2.3	1.14	2.01	19.3	4.8	1.90	0.87	A-262
2.1	1.15	1.99	17.4	4.3	1.91	0.87	A-263
1.9	1.16	1.96	15.5	3.8	1.92	0.87	A-264
1.6	1.17	1.94	13.5	3.3	1.93	0.88	A-265

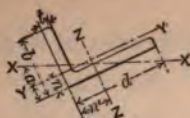
Properties of Angles

Unequal Legs

Continued

Section Index	Dimensions, Inches	Thickness, Inches	Weight per Foot, Pounds	Area of Section, Square Inches	Distance of Center of Gravity from Back of Longer Leg, Inches	Moment of Inertia, Axis Y—Y
	d x b	t		A	n	I
A-274	6 x 3½	¾	22.4	6.56	0.93	5.8
A-275	6 x 3½	11/16	20.6	6.06	0.90	5.5
A-276	6 x 3½	5/8	18.9	5.55	0.88	5.1
A-277	6 x 3½	9/16	17.1	5.03	0.86	4.7
A-278	6 x 3½	1/2	15.3	4.50	0.83	4.3
A-279	6 x 3½	7/16	13.5	3.97	0.81	3.8
A-280	6 x 3½	3/8	11.7	3.42	0.78	3.3
A-286	5 x 4	13/16	22.7	6.65	1.18	8.7
A-287	5 x 4	¾	21.1	6.19	1.16	8.2
A-288	5 x 4	11/16	19.5	5.72	1.14	7.7
A-289	5 x 4	5/8	17.8	5.23	1.12	7.1
A-290	5 x 4	9/16	16.2	4.75	1.10	6.6
A-291	5 x 4	1/2	14.5	4.25	1.07	6.0
A-292	5 x 4	7/16	12.8	3.75	1.05	5.3
A-293	5 x 4	3/8	11.0	3.23	1.03	4.7
A-300	5 x 3½	¾	19.8	5.81	1.00	5.6
A-301	5 x 3½	11/16	18.3	5.37	0.97	5.2
A-302	5 x 3½	5/8	16.8	4.92	0.95	4.8
A-303	5 x 3½	9/16	15.2	4.47	0.93	4.4
A-304	5 x 3½	1/2	13.6	4.00	0.91	4.0
A-305	5 x 3½	7/16	12.0	3.53	0.88	3.6
A-306	5 x 3½	3/8	10.4	3.05	0.86	3.2
A-307	5 x 3½	5/16	8.7	2.56	0.84	2.7
A-315	5 x 3	11/16	17.1	5.03	0.82	3.3
A-316	5 x 3	5/8	15.7	4.61	0.80	3.1
A-317	5 x 3	9/16	14.3	4.18	0.77	2.8
A-318	5 x 3	1/2	12.8	3.75	0.75	2.6
A-319	5 x 3	7/16	11.3	3.31	0.73	2.3
A-320	5 x 3	3/8	9.8	2.86	0.70	2.0
A-321	5 x 3	5/16	8.2	2.40	0.68	1.8

JONES & LAUGHLIN STEEL COMPANY



Section Factor Axis Y—Y	Radius of Gyration Axis Y—Y, Inches	Distance of Center of Gravity from Back Leg, Inches	Moment of Inertia Axis Z—Z	Section Factor Axis Z—Z	Radius of Gyration Axis Z—Z	Least Radius of Gyration Axis X—X, Inches	Section Index
S	r	n'	I'	S'	r'	r''	
2.3	0.94	2.18	23.3	6.1	1.89	0.75	A-274
2.1	0.95	2.15	21.7	5.6	1.89	0.75	A-275
1.9	0.96	2.13	20.1	5.2	1.90	0.75	A-276
1.8	0.96	2.11	18.4	4.7	1.91	0.75	A-277
1.6	0.97	2.08	16.6	4.2	1.92	0.76	A-278
1.4	0.98	2.06	14.8	3.7	1.93	0.76	A-279
1.2	0.99	2.04	12.9	3.3	1.94	0.77	A-280
3.1	1.15	1.68	15.5	4.7	1.53	0.84	A-286
2.9	1.15	1.66	14.6	4.4	1.54	0.84	A-287
2.7	1.16	1.64	13.6	4.1	1.54	0.84	A-288
2.5	1.17	1.62	12.6	3.7	1.55	0.84	A-289
2.3	1.18	1.60	11.6	3.4	1.56	0.85	A-290
2.0	1.18	1.57	10.5	3.1	1.57	0.85	A-291
1.8	1.19	1.55	9.3	2.7	1.58	0.85	A-292
1.6	1.20	1.53	8.1	2.3	1.59	0.86	A-293
2.2	0.98	1.75	13.9	4.3	1.55	0.75	A-300
2.1	0.98	1.72	13.0	4.0	1.56	0.75	A-301
1.9	0.99	1.70	12.0	3.7	1.56	0.75	A-302
1.7	1.00	1.68	11.0	3.3	1.57	0.75	A-303
1.6	1.01	1.66	10.0	3.0	1.58	0.75	A-304
1.4	1.01	1.63	8.9	2.6	1.59	0.76	A-305
1.2	1.02	1.61	7.8	2.3	1.60	0.76	A-306
1.0	1.03	1.59	6.6	1.9	1.61	0.76	A-307
1.5	0.81	1.82	12.3	3.9	1.56	0.64	A-315
1.4	0.81	1.80	11.4	3.5	1.57	0.64	A-316
1.3	0.82	1.77	10.4	3.2	1.58	0.65	A-317
1.1	0.83	1.75	9.5	2.9	1.59	0.65	A-318
1.0	0.84	1.73	8.4	2.6	1.60	0.65	A-319
0.89	0.84	1.70	7.4	2.2	1.61	0.65	A-320
0.75	0.85	1.68	6.3	1.9	1.61	0.66	A-321

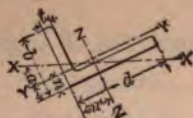
Properties of Angles

Unequal Legs

Continued

Section Index	Dimensions, Inches	Thickness, Inches	Weight per Foot, Pounds	Area of Section, Square Inches	Distance of Center of Gravity from Back of Longer Leg, Inches	Moment of Inertia, Axis Y-Y
	d x b	t		A	n	I
A-328	4 1/2 x 3	11/16	16.0	4.68	0.85	3.2
A-329	4 1/2 x 3	5/8	14.7	4.30	0.83	3.0
A-330	4 1/2 x 3	7/16	13.3	3.90	0.81	2.8
A-331	4 1/2 x 3	1/2	11.9	3.50	0.79	2.5
A-332	4 1/2 x 3	7/16	10.6	3.09	0.76	2.3
A-333	4 1/2 x 3	5/8	9.1	2.67	0.74	2.0
A-334	4 1/2 x 3	7/16	7.7	2.25	0.72	1.7
A-339	4 x 3 1/2	11/16	18.5	5.43	1.11	5.5
A-340	4 x 3 1/2	3/4	17.3	5.06	1.09	5.2
A-341	4 x 3 1/2	7/16	16.0	4.68	1.07	4.9
A-342	4 x 3 1/2	5/8	14.7	4.30	1.04	4.5
A-343	4 x 3 1/2	7/16	13.3	3.90	1.02	4.2
A-344	4 x 3 1/2	1/2	11.9	3.50	1.00	3.8
A-345	4 x 3 1/2	7/16	10.6	3.09	0.98	3.4
A-346	4 x 3 1/2	5/8	9.1	2.67	0.96	3.0
A-347	4 x 3 1/2	7/16	7.7	2.25	0.93	2.6
A-354	4 x 3	11/16	14.8	4.34	0.89	3.1
A-355	4 x 3	5/8	13.6	3.98	0.87	2.9
A-356	4 x 3	9/16	12.4	3.62	0.85	2.7
A-357	4 x 3	1/2	11.1	3.25	0.83	2.4
A-358	4 x 3	7/16	9.8	2.87	0.80	2.2
A-359	4 x 3	5/8	8.5	2.48	0.78	1.9
A-360	4 x 3	7/16	7.2	2.09	0.76	1.7
A-361	4 x 3	1/4	5.8	1.69	0.74	1.4
A-365	3 1/2 x 3	11/16	13.6	4.00	0.94	3.0
A-366	3 1/2 x 3	5/8	12.5	3.67	0.92	2.8
A-367	3 1/2 x 3	9/16	11.4	3.34	0.90	2.5
A-368	3 1/2 x 3	1/2	10.2	3.00	0.88	2.3
A-369	3 1/2 x 3	7/16	9.1	2.65	0.85	2.1
A-370	3 1/2 x 3	5/8	7.9	2.30	0.83	1.8
A-371	3 1/2 x 3	7/16	6.6	1.93	0.81	1.6
A-372	3 1/2 x 3	1/4	5.4	1.56	0.79	1.3

JONES & LAUGHLIN STEEL COMPANY



ion tor is -Y	Radius of Gyration Axis Y-Y, Inches r	Distance of Center of Gravity from Back of Shorter Leg, Inches n'	Moment of Inertia Axis Z-Z I'	Section Factor Axis Z-Z S'	Radius of Gyration Axis Z-Z r'	Least Radius of Gyration Axis X-X, Inches r''	Section Index
5	0.83	1.60	9.1	3.1	1.39	0.64	A-328
4	0.83	1.58	8.4	2.9	1.40	0.64	A-329
3	0.85	1.56	7.8	2.6	1.41	0.64	A-330
1	0.85	1.54	7.0	2.4	1.42	0.65	A-331
0	0.85	1.51	6.3	2.1	1.43	0.65	A-332
88	0.86	1.49	5.5	1.8	1.44	0.66	A-333
75	0.87	1.47	4.7	1.5	1.44	0.66	A-334
3	1.01	1.36	7.8	2.9	1.19	0.72	A-339
1	1.01	1.34	7.3	2.8	1.20	0.72	A-340
0	1.02	1.32	6.9	2.6	1.21	0.72	A-341
3	1.03	1.29	6.4	2.4	1.22	0.72	A-342
7	1.03	1.27	5.9	2.1	1.23	0.72	A-343
5	1.04	1.25	5.3	1.9	1.23	0.72	A-344
3	1.05	1.23	4.8	1.7	1.24	0.72	A-345
2	1.06	1.21	4.2	1.5	1.25	0.73	A-346
0	1.07	1.18	3.6	1.3	1.26	0.73	A-347
5	0.84	1.39	6.5	2.5	1.22	0.64	A-354
4	0.85	1.37	6.0	2.3	1.23	0.64	A-355
2	0.86	1.35	5.6	2.1	1.24	0.64	A-356
1	0.86	1.33	5.0	1.9	1.25	0.64	A-357
0	0.87	1.30	4.5	1.7	1.25	0.64	A-358
87	0.88	1.28	4.0	1.5	1.26	0.64	A-359
74	0.89	1.26	3.4	1.2	1.27	0.65	A-360
60	0.89	1.24	2.8	1.0	1.28	0.65	A-361
4	0.86	1.19	4.4	1.9	1.05	0.62	A-365
3	0.87	1.17	4.1	1.8	1.06	0.62	A-366
2	0.87	1.15	3.8	1.6	1.07	0.62	A-367
1	0.88	1.13	3.5	1.5	1.07	0.62	A-368
98	0.89	1.10	3.1	1.3	1.08	0.62	A-369
85	0.90	1.08	2.7	1.1	1.09	0.62	A-370
72	0.90	1.06	2.3	0.96	1.10	0.63	A-371
58	0.91	1.04	1.9	0.78	1.11	0.63	A-372

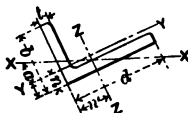
Properties of Angles

Unequal Legs

Continued

Section Index	Dimensions, Inches	Thickness, Inches	Weight per Foot, Pounds	Area of Section, Square Inches	Distance of Center of Gravity from Back of Longer Leg, Inches	Moment of Inertia, Axis Y—Y
	$d \times b$	t		A	n	I
A-379	$3\frac{1}{2} \times 2\frac{1}{2}$	$\frac{9}{16}$	10.4	3.06	0.73	1.5
A-380	$3\frac{1}{2} \times 2\frac{1}{2}$	$\frac{1}{2}$	9.4	2.75	0.70	1.4
A-381	$3\frac{1}{2} \times 2\frac{1}{2}$	$\frac{7}{16}$	8.3	2.43	0.68	1.2
A-382	$3\frac{1}{2} \times 2\frac{1}{2}$	$\frac{3}{8}$	7.2	2.11	0.66	1.1
A-383	$3\frac{1}{2} \times 2\frac{1}{2}$	$\frac{5}{16}$	6.1	1.78	0.64	0.94
A-384	$3\frac{1}{2} \times 2\frac{1}{2}$	$\frac{1}{4}$	4.9	1.44	0.61	0.78
A-405	$3 \times 2\frac{1}{2}$	$\frac{9}{16}$	9.5	2.78	0.77	1.4
A-406	$3 \times 2\frac{1}{2}$	$\frac{1}{2}$	8.5	2.50	0.75	1.3
A-407	$3 \times 2\frac{1}{2}$	$\frac{7}{16}$	7.6	2.21	0.73	1.2
A-408	$3 \times 2\frac{1}{2}$	$\frac{3}{8}$	6.6	1.92	0.71	1.0
A-409	$3 \times 2\frac{1}{2}$	$\frac{5}{16}$	5.6	1.62	0.68	0.90
A-410	$3 \times 2\frac{1}{2}$	$\frac{1}{4}$	4.5	1.31	0.66	0.74
A-415	3×2	$\frac{1}{2}$	7.7	2.25	0.58	0.67
A-416	3×2	$\frac{7}{16}$	6.8	2.00	0.56	0.61
A-417	3×2	$\frac{3}{8}$	5.9	1.73	0.54	0.54
A-418	3×2	$\frac{5}{16}$	5.0	1.47	0.52	0.47
A-419	3×2	$\frac{1}{4}$	4.1	1.19	0.49	0.39
A-420	3×2	$\frac{3}{16}$	3.07	0.91	0.47	0.31
A-425	$2\frac{1}{2} \times 2$	$\frac{1}{2}$	6.8	2.00	0.63	0.64
A-426	$2\frac{1}{2} \times 2$	$\frac{7}{16}$	6.1	1.78	0.60	0.58
A-427	$2\frac{1}{2} \times 2$	$\frac{3}{8}$	5.3	1.55	0.58	0.51
A-428	$2\frac{1}{2} \times 2$	$\frac{5}{16}$	4.5	1.31	0.56	0.45
A-429	$2\frac{1}{2} \times 2$	$\frac{1}{4}$	3.62	1.06	0.54	0.37
A-430	$2\frac{1}{2} \times 2$	$\frac{3}{16}$	2.75	0.81	0.51	0.29

JONES & LAUGHLIN STEEL COMPANY



Section Factor Axis Y—Y	Radius of Gyration Axis Y—Y, Inches	Distance of Center of Gravity from Back of Shorter Leg, Inches	Moment of Inertia Axis Z—Z	Section Factor Axis Z—Z	Radius of Gyration Axis Z—Z	Least Radius of Gyration Axis X—X, Inches	Section Index
S	r	n'	I'	S'	r'	r''	
0.84	0.70	1.23	3.6	1.6	1.08	0.53	A-379
0.76	0.70	1.20	3.2	1.4	1.09	0.53	A-380
0.68	0.71	1.18	2.9	1.3	1.09	0.54	A-381
0.59	0.72	1.16	2.6	1.1	1.10	0.54	A-382
0.50	0.73	1.14	2.2	0.93	1.11	0.54	A-383
0.41	0.74	1.11	1.8	0.75	1.12	0.54	A-384
0.82	0.72	1.02	2.3	1.2	0.91	0.52	A-405
0.74	0.72	1.00	2.1	1.0	0.91	0.52	A-406
0.66	0.73	0.98	1.9	0.93	0.92	0.52	A-407
0.58	0.74	0.96	1.7	0.81	0.93	0.52	A-408
0.49	0.74	0.93	1.4	0.69	0.94	0.53	A-409
0.40	0.75	0.91	1.2	0.56	0.95	0.53	A-410
0.47	0.55	1.08	1.9	1.00	0.92	0.43	A-415
0.42	0.55	1.06	1.7	0.89	0.93	0.43	A-416
0.37	0.56	1.04	1.5	0.78	0.94	0.43	A-417
0.32	0.57	1.02	1.3	0.66	0.95	0.43	A-418
0.25	0.57	0.99	1.1	0.54	0.95	0.43	A-419
0.20	0.58	0.97	0.84	0.41	0.96	0.44	A-420
0.46	0.56	0.88	1.1	0.70	0.75	0.42	A-425
0.41	0.57	0.85	1.0	0.62	0.76	0.42	A-426
0.36	0.58	0.83	0.91	0.55	0.77	0.42	A-427
0.31	0.58	0.81	0.79	0.47	0.78	0.42	A-428
0.25	0.59	0.79	0.65	0.38	0.78	0.42	A-429
0.20	0.60	0.76	0.51	0.29	0.79	0.43	A-430

Properties of Tees

Section Index	Size Flange by Stem, Inches	Weight per Foot, Pounds	Area of Section, Square Inches	Distance of Center of Gravity from Outside of Flange, Inches	Moment of Inertia, Neutral Axis through Center of Gravity Parallel to Flange, I	Least Section Factor, Neutral Axis through Center of Gravity Parallel to Flange, S	Radius of Gyration, Neutral Axis through Center of Gravity Parallel to Flange, r	Moment of Inertia, Neutral Axis through Center of Gravity Coincident with Center of Line of Stem, I'	Section Factor, Neutral Axis through Center of Gravity with Center of Line of Stem, S'	Radius of Gyration, Neutral Axis through Center of Gravity Coincident with Center of Line of Stem, r'
T-3	4 x 4	13.5	3.97	1.178	5.715	2.025	1.2	2.8066	1.4033	.841
T-4	4 x 4	12.1	3.56	1.144	5.166	1.808	1.204	2.4586	1.2293	.831
T-9	3½ x 3½	10.5	3.09	1.022	3.376	1.362	1.045	1.6540	.945	.731
T-10	3½ x 3½	9.2	2.70	.9983	2.996	1.195	1.050	1.3928	.796	.716
T-15	3 x 3	7.8	2.29	.877	1.838	.864	.893	.8918	.599	.625
T-16	3 x 3	6.7	1.97	.847	1.609	.743	.897	.7520	.501	.617
T-17	3 x 3	5.5	1.61	.824	1.325	.609	.905	.6066	.404	.611
T-22	2½ x 2½	6.4	1.88	.756	1.022	.585	.737	.5243	.419	.528
T-23	2½ x 2½	5.5	1.61	.729	.892	.503	.742	.4386	.3508	.521
T-28	2¼ x 2¼	4.7	1.38	.669	.623	.394	.671	.3109	.2764	.474
T-29	2¼ x 2¼	3.83	1.13	.650	.519	.324	.678	.2488	.2211	.469
T-33	2 x 2	4.1	1.20	.613	.4247	.306	.593	.2194	.2194	.426
T-34	2 x 2	3.38	1.00	.588	.3577	.253	.599	.1754	.1754	.420

Properties of Tees Continued

Section Index	Size Flange by Stem, Inches	Weight per Foot, Pounds	Area of Section, Square Inches	Distance of Center of Gravity from Outside of Flange, Inches	Moment of Inertia Neutral Axis through Center of Gravity Parallel to Flange I	Least Section Factor, Neutral Axis through Center of Gravity Parallel to Flange S	Radius of Gyration, Neutral Axis through Center of Gravity Parallel to Flange r	Moment of Inertia, Neutral Axis through Center of Gravity Coincident with Center Line of Stem I'	Section Factor, Neutral Axis through Center of Gravity Coincident with Center Line of Stem S'	Radius of Gyration, Neutral Axis through Center of Gravity Coincident with Center Line of Stem r'
T-39	13/4 x 13/4	2.93	.86	.526	.2315	.189	.518	.1181	.1349	.370
T-40	13/4 x 1 1/4	2.28	.67	.503	.1857	.148	.526	.0887	.1013	.346
T-45	1 1/2 x 1 1/2	2.47	.72	.47	.15	.14	.45	.08	.10	.32
T-46	1 1/2 x 1 1/2	1.94	.57	.44	.11	.11	.45	.06	.08	.32
T-51	1 1/4 x 1 1/4	2.02	.59	.40	.08	.10	.37	.05	.07	.28
T-52	1 1/4 x 1 1/4	1.59	.47	.38	.06	.07	.37	.03	.05	.27
T-57	1 x 1	1.25	.37	.32	.03	.05	.29	.02	.04	.22
T-58	1 x 1	0.89	.26	.29	.02	.03	.30	.01	.02	.21
*T-69	5 x 2 1/2	10.9	3.2	.63	1.5	.78	.68	4.1	1.6	1.14
*T-74	4 1/2 x 3	8.4	2.47	.71	1.8	.78	.85	2.5	1.1	1.01
T-79	4 x 2	7.8	2.29	.48	.60	.40	.52	2.1	1.1	.96
T-80	4 x 2	6.7	1.97	.46	.53	.34	.52	1.8	.88	.95

*Made only by special arrangement.

Properties of Tees

Continued

Section Index	Size Flange by Stem, Inches	Weight per Foot, Pounds	Area of Section, Square Inches	Distance of Center of Gravity from Outside of Flange, Inches	Moment of Inertia, Neutral Axis through Center of Gravity Parallel to Flange	Least Section Factor, Neutral Axis through Center of Gravity Parallel to Flange	Radius of Gyration, Neutral Axis through Center of Gravity Parallel to Flange	Moment of Inertia, Neutral Axis through Center of Gravity Coincident with Center Line of Stem	Section Factor, Neutral Axis through Center of Gravity Coincident with Center Line of Stem	Radius of Gyration, Neutral Axis through Center of Gravity Coincident with Center Line of Stem
T-85	3½x 4	12.6	3.70	1.24	5.5	2.0	1.21	1.9	1.1	.72
T-86	3½x 4	9.8	2.88	1.19	4.3	1.5	1.23	1.4	.81	.70
T-91	3½x 3	9.7	2.85	.845	2.1667	1.005	.8719	1.649	.942	.760
T-92	3½x 3	8.5	2.50	.83	1.9	.89	.88	1.4	.81	.75
T-96	3 x 3½	10.8	3.17	1.12	3.5	1.5	1.06	1.2	.80	.62
T-97	3 x 3½	9.7	2.85	1.10	3.2	1.3	1.06	1.0	.69	.61
T-98	3 x 3½	8.5	2.50	1.07	2.8	1.2	1.07	.93	.62	.60
T-103	2½x 2	4.7	1.38	.554	.4576	.316	.575	.4234	.3387	.5535
T-108	2½x 1¾	3.6	1.06	.4529	.2596	.2000	.494	.3392	.271	.565
T-112	2½x 2¼	3.65	1.07	.6507	.4678	.2902	.661	.1775	.1747	.407

Properties of Zees

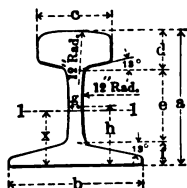
Section Index	Depth of Web, Inches	Width of Flange, Inches	Thickness of Metal, Inches	Weight per Foot, Pounds	Area of Section, Square Inches	Moments of Inertia		Section Factors		Radii of Gyration		
						I	I'	S	S'	r	r'	r ²
						Neutral Axis through Center of Gravity Perpendicular to Web	Neutral Axis through Center of Gravity Coincident with Web	Neutral Axis through Center of Gravity Perpendicular to Web	Neutral Axis through Center of Gravity Coincident with Web	Neutral Axis through Center of Gravity Perpendicular to Web	Neutral Axis through Center of Gravity Coincident with Web	Least Radius of Neutral Axis Diagonal
Z-70	5 1/8	3 3/8	1 1/16	28.4	8.33	28.7	14.4	11.2	4.8	1.86	1.31	0.76
Z-71	5 1/16	3 1/16	3/4	26.0	7.64	26.2	12.8	10.3	4.4	1.85	1.30	0.74
Z-72	5	3 1/4	1 1/16	23.7	6.96	23.7	11.4	9.5	3.9	1.84	1.28	0.73
Z-73	5 1/8	3 3/8	5/8	22.6	6.64	24.5	12.1	9.6	3.9	1.92	1.35	0.76
Z-74	5 1/16	3 1/16	1 1/16	20.2	5.94	21.8	10.5	8.6	3.5	1.91	1.33	0.75
Z-75	5	3 1/4	1 1/2	17.9	5.25	19.2	9.1	7.7	3.0	1.91	1.31	0.74
Z-76	5 1/8	3 3/8	1 1/16	16.4	4.81	19.1	9.2	7.4	2.9	1.99	1.38	0.77
Z-77	5 1/16	3 1/16	3/8	14.0	4.10	16.2	7.7	6.4	2.5	1.99	1.37	0.76
Z-78	5	3 1/4	1 1/16	11.6	3.40	13.4	6.2	5.3	2.0	1.98	1.35	0.75
Z-80	4 1/8	3 1/16	3/4	23.0	6.75	15.0	11.2	7.3	4.0	1.49	1.29	0.68
Z-81	4 1/16	3 1/8	1 1/16	20.9	6.14	13.5	10.0	6.7	3.6	1.48	1.27	0.67
Z-82	4	3 1/16	5/8	18.9	5.55	12.1	8.7	6.1	3.2	1.48	1.25	0.66
Z-83	4 1/8	3 1/16	3/4	18.0	5.27	12.7	9.3	6.2	3.2	1.55	1.33	0.68
Z-84	4 1/16	3 1/8	1 1/2	15.9	4.66	11.2	8.0	5.5	2.8	1.55	1.31	0.67
Z-85	4	3 1/16	1 1/16	13.8	4.05	9.7	6.7	4.8	2.4	1.55	1.29	0.66

Properties of Zees

Continued

Section Index	Depth of Web, Inches	Width of Flange, Inches	Thickness of Metal, Inches	Weight per Foot, Pounds	Area of Section, Square Inches	Momenta of Inertia		Section Factors		Radii of Gyration		
						I	I'	β	β'	r	r'	r ²
						Neutral Axis through Center of Gravity Perpendicular to Web	Neutral Axis through Center of Gravity Coincident with Web	Neutral Axis Through Center of Gravity Perpendicular to Web	Neutral Axis Through Center of Gravity Coincident with Web	Neutral Axis Through Center of Gravity Perpendicular to Web	Neutral Axis Through Center of Gravity Coincident with Web	Least Radius of Neutral Axis Diagonal
Z-86	4 $\frac{1}{8}$	3 $\frac{1}{16}$	3 $\frac{3}{8}$	12.5	3.66	9.6	6.8	4.7	2.3	1.02	1.36	0.69
Z-87	4 $\frac{1}{8}$	3 $\frac{1}{8}$	3 $\frac{1}{2}$	10.3	3.03	7.9	5.5	3.9	1.8	1.02	1.34	0.68
Z-88	4	3 $\frac{1}{8}$	1 $\frac{1}{4}$	8.2	2.41	6.3	4.2	3.1	1.4	1.02	1.33	0.67
Z-3	3 $\frac{1}{8}$	2 $\frac{3}{4}$	1 $\frac{1}{2}$	14.3	4.18	5.3	5.7	3.4	2.3	1.12	1.17	0.54
Z-4	3	2 $\frac{1}{8}$	1 $\frac{1}{2}$	12.6	3.69	4.6	4.9	3.1	2.0	1.12	1.15	0.53
Z-7	3 $\frac{1}{8}$	2 $\frac{3}{4}$	1 $\frac{1}{2}$	11.5	3.36	4.6	4.8	3.0	1.9	1.17	1.19	0.55
Z-8	3	2 $\frac{1}{8}$	1 $\frac{1}{2}$	9.8	2.86	3.9	3.9	2.6	1.6	1.16	1.17	0.54
Z-11	3 $\frac{1}{8}$	2 $\frac{3}{4}$	1 $\frac{1}{2}$	8.5	2.48	3.6	3.6	2.4	1.4	1.21	1.21	0.56
Z-12	3	2 $\frac{1}{8}$	1 $\frac{1}{2}$	6.7	1.97	2.9	2.8	1.9	1.1	1.21	1.19	0.55
Z-18	3	1 $\frac{1}{2}$	1 $\frac{1}{2}$	3.59	1.06	1.396	.35	.933	.248	1.149	.574	.358

Properties of A. S. C. E. and Light Rails

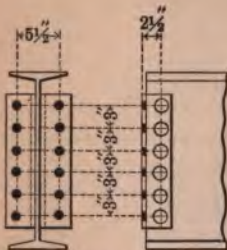


Section Index	Weight per Yard	Area of Section	DIMENSIONS								Axis 1-1			
			a	b	c	d	e	f	g	h	I	r	S	x
	Pounds	Sq. In.	In.	In.	In.	In.	In.	In.	In.	In.				
....	110	10.80	6 1/8	6 1/8	2 7/8	1 1/4	3 1/4	1	1 1/4	2 1/4	55.2	2.26	17.2	2.92
....	100	9.84	5 3/4	5 3/4	2 3/4	1 1/4	3 1/4	1 1/4	1 1/4	2 1/4	44.0	2.11	14.6	2.73
....	95	9.28	5 7/8	5 7/8	2 1/4	1 1/4	2 1/4	1 1/4	1 1/4	2 1/4	38.8	2.05	13.3	2.65
....	90	8.83	5 3/8	5 3/8	2 3/8	1 1/4	2 1/4	1 1/4	1 1/4	2 1/4	34.4	1.97	12.2	2.55
....	85	8.33	5 1/8	5 1/8	2 1/8	1 1/4	2 1/4	1 1/4	1 1/4	2 1/4	30.1	1.90	11.1	2.47
....	80	7.86	5	5	2 1/2	1 1/4	2 1/4	1 1/4	1 1/4	2 1/4	26.4	1.83	10.1	2.38
....	75	7.33	4 1/2	4 1/2	2 1/4	1 1/4	2 1/4	1 1/4	1 1/4	2 1/4	22.9	1.77	9.1	2.30
....	70	6.81	4 3/8	4 3/8	2 1/8	1 1/4	2 1/4	1 1/4	1 1/4	2 1/4	19.7	1.70	8.2	2.22
....	65	6.33	4 1/8	4 1/8	2 1/4	1 1/4	2 1/4	1 1/4	1 1/4	2 1/4	16.9	1.63	7.4	2.14
....	60	5.93	4 1/4	4 1/4	2 3/8	1 1/4	2 1/4	1 1/4	1 1/4	2 1/4	14.6	1.57	6.6	2.05
....	55	5.38	4 1/8	4 1/8	2 1/4	1 1/4	2 1/4	1 1/4	1 1/4	2 1/4	12.0	1.50	5.7	1.97
....	50	4.87	3 7/8	3 7/8	2 1/8	1 1/4	2 1/4	1 1/4	1 1/4	2 1/4	9.9	1.43	5.0	1.88
....	45	4.40	3 1/4	3 1/4	2	1 1/4	1 1/4	1 1/4	1 1/4	2 1/4	8.1	1.36	4.3	1.78
R-40	40	3.94	3 1/2	3 1/2	1 7/8	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	6.6	1.29	3.6	1.68
R-35	35	3.44	3 1/8	3 1/8	1 3/4	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	5.2	1.23	3.0	1.60
R-30	30	3.00	3 1/8	3 1/8	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	4.1	1.16	2.5	1.52
R-25	25	2.39	2 3/4	2 3/4	1 1/2	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	2.5	1.02	1.8	1.33
R-20	20	2.00	2 3/8	2 3/8	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	1.9	0.99	1.4	1.27
R-16	16	1.55	2 3/8	2 3/8	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	1.2	0.89	1.0	1.15
....	14	1.34	2 1/8	2 1/8	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	0.76	0.75	0.73	1.02
R-12	12	1.18	2	2	1	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	0.66	0.75	0.63	0.96
....	10	0.96	1 3/4	1 3/4	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	0.40	0.65	0.46	0.87
R-8	8	0.77	1 1/8	1 1/8	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	1 1/4	0.26	0.58	0.32	0.75

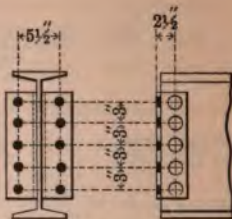
Only sections carrying Index Numbers made by Jones & Laughlin Steel Company.

Beam and Channel Connections

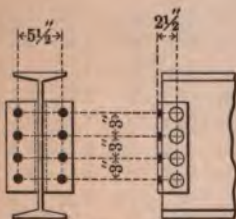
All Rivets $\frac{3}{4}$ " Diameter



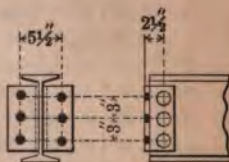
24" 2-4" x 4" x $\frac{1}{2}$ " Angles-1'-5 1/2"



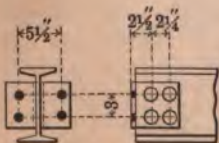
20"-18" 2-4" x 4" x $\frac{1}{2}$ " Angles-1'-2 1/2"



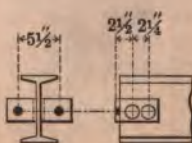
15" 2-4" x 4" x $\frac{1}{16}$ " Angles-0'-11 1/2"



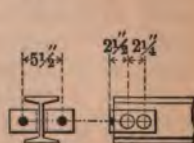
12" 2-4" x 4" x $\frac{1}{16}$ " Angles-0'-8 1/2"



10"-9"-8"
2-6" x 4" x $\frac{3}{8}$ " Angles-0'-5 1/2"



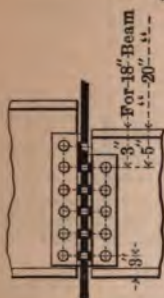
7"-6"-5"
2-6" x 4" x $\frac{3}{8}$ " Angles-0'-3"



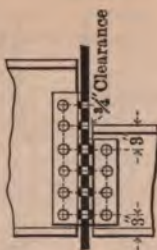
4"-3"
2-6" x 4" x $\frac{3}{8}$ " Angles-0'-2"

Location of Connection Angles

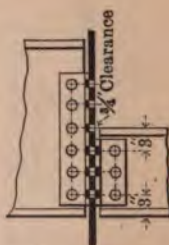
For Different Depths of Beams Framing Opposite Bottoms or Tops Being Flush



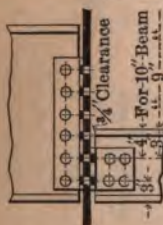
24" Beam to $\begin{cases} 18" \text{ Beam} \\ 20" \text{ Beam} \end{cases}$



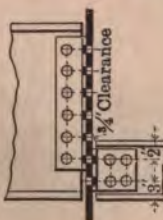
24" Beam to 15" Beam



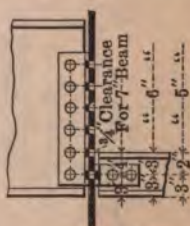
24" Beam to 12" Beam



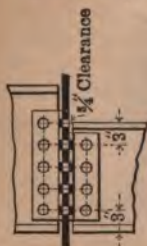
24" Beam to $\left\{ \begin{array}{l} 10'' \text{ Beam} \\ 9'' \text{ Beam} \end{array} \right.$



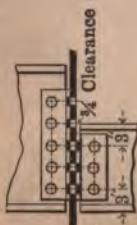
24" Beam to 8" Beam



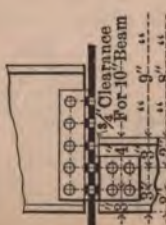
24" Beam to $\begin{cases} 7'' \text{ Beam} \\ 6'' \text{ Beam} \\ 5'' \text{ Beam} \end{cases}$



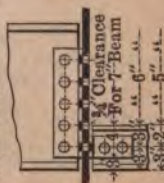
18" }
20" } to 15" Beam



18" } to 12" Beam
20" }



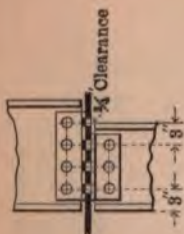
18" } to { 9" Beam
20" } 10" Beam
8" Beam



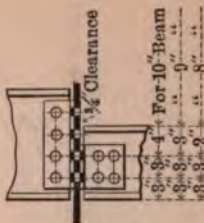
18" } to { 7" Beam
20" } { 6" Beam
 { 5" Beam

Location of Connection Angles

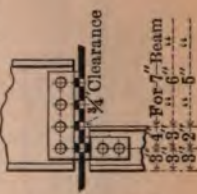
For Different Depths of Beams Framing Opposite Bottoms or Tops Being Flush



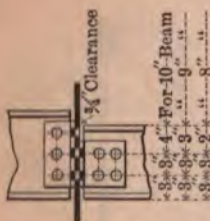
15" Beam to 12" Beam



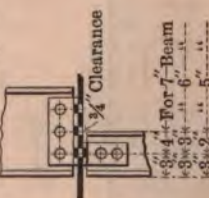
15" Beam to { 10" Beam
9" Beam
8" Beam



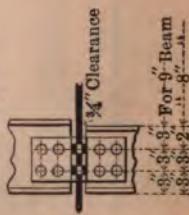
15" Beam to $\begin{cases} 7'' \text{ Beam} \\ 6'' \text{ Beam} \\ 5'' \text{ Beam} \end{cases}$



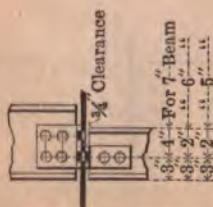
12" Beam to { 10" Beam
9" Beam
8" Beam



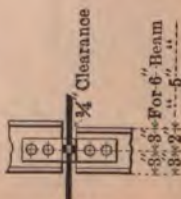
12" Beam to $\begin{cases} 7'' \text{ Beam} \\ 6'' \text{ Beam} \\ 5'' \text{ Beam} \end{cases}$



10" Beam to $\begin{cases} 9'' \text{ Beam} \\ 8'' \text{ Beam} \end{cases}$



10" Beam	} to {	7" Beam
9" Beam		6" Beam
8" Beam		5" Beam



7" Beam to $\begin{cases} 6" \text{ Beam} \\ 5" \text{ Beam} \end{cases}$

Limiting Values of Beam Connections

I-Beams		Value of Web Connection	Values of Outstanding Legs of Connection Angles					
			Field Rivets			Field Bolts		
Depth, Inches	Weight per Foot, Pounds	Shop Rivets in Enclosed Bearing, Pounds	$\frac{3}{4}$ " Rivets or Turned Bolts, Single Shear, Pounds	Minimum Allowable Span, Uniform Load, Feet	t, In.	$\frac{3}{4}$ " Rough Bolts, Single Shear, Pounds	Minimum Allowable Span, Uniform Load, Feet	t, In.
24	80	67,500	53,000	17.5	$\frac{5}{8}$	42,400	21.9	$\frac{5}{8}$
20	65	56,200	44,200	14.2	$\frac{5}{8}$	35,300	17.6	$\frac{5}{8}$
18	55	51,800	44,200	10.7	$\frac{5}{8}$	35,300	13.4	$\frac{5}{8}$
15	42	36,900	35,300	8.9	$\frac{5}{8}$	28,300	11.2	$\frac{5}{8}$
12	31 $\frac{1}{2}$	23,800	26,500	7.1	$\frac{1}{2}$	21,200	9.0	$\frac{5}{8}$
10	25	27,900	17,700	7.4	$\frac{5}{8}$	14,100	9.2	$\frac{5}{8}$
9	21	26,100	17,700	5.7	$\frac{5}{8}$	14,100	7.1	$\frac{5}{8}$
8	18	24,300	17,700	4.3	$\frac{5}{8}$	14,100	5.4	$\frac{5}{8}$
7	15	11,300	8,800	6.2	$\frac{5}{8}$	7,100	7.8	$\frac{5}{8}$
6	12 $\frac{1}{4}$	10,400	8,800	4.4	$\frac{5}{8}$	7,100	5.5	$\frac{5}{8}$
5	9 $\frac{3}{4}$	9,500	8,800	2.9	$\frac{5}{8}$	7,100	3.6	$\frac{5}{8}$

Allowable Unit Stress in Pounds per Square Inch

Single Shear		Bearing	
Rivets.....	Shop 12,000	Rivets—enclosed.....	Shop 30,000
Rivets and Turned Bolts...	Field 16,000	Rivets—one side.....	Shop 24,000
Rough Bolts.....	Field 8,000	Rivets and Turned Bolts..	Field 20,000
		Rough Bolts.....	Field 16,000

t—Web Thickness, in bearing to develop maximum allowable reactions, when beams frame opposite.


Connections are figured for bearing and shear (no moment considered).

The above values agree with tests made on beams under ordinary conditions of use.

Special connections should be used when any of the limiting conditions given above are exceeded such as end reactions from loaded beam being greater than value of connection; shorter span with beam fully loaded; or a less thickness of web when maximum allowable reactions are used.

Cast Separators for Beams Separators with Two Bolts

Separators with 120 Bolts


DESIGNATION OF BEAM		DISTANCES		BOLTS		WEIGHTS				
Depth, Inches	Weight, Pounds	Out to Out of Beam Flanges, Inches	Center to Center of Beams, Inches	Size, Inches		Length for Minimum Width Separator, Inches	Bolts and Nuts, Pounds	Add to Bolts for Each Inch Additional Spread of Beams, Pounds	Separator, Pounds	Add to Separator for Each Inch Additional Spread of Beams, Pounds
					S					
24	105	16 1/2	8 5/8	3 3/4	12	10 1/4	3 3/4	0.25	35	4 1/4
24	80	14 3/4	7 3/4	3 3/4	12	9 1/4	3 1/2	0.25	32	4 1/4
20	80	14 3/4	7 3/4	3 3/4	10	9 1/4	3 1/2	0.25	28	3 1/8
20	65	13 1/4	7	3 3/4	10	8 1/2	3 1/4	0.25	25	3 1/8
18	55	12 3/4	6 3/4	3 3/4	9	8 1/2	3 1/4	0.25	16	2 3/4
15	60	12 3/4	6 3/4	3 3/4	7	8 1/2	3 1/4	0.25	15	1 3/4
15	42	11 3/4	6 1/4	3 3/4	7	7 3/4	3	0.25	15	1 3/4
12	40	11 1/4	6	3 3/4	6 1/2	7 1/2	3	0.25	11	1 1/2
12	31 1/2	10 3/4	5 3/4	3 3/4	6 1/2	7 1/4	3	0.25	11	1 1/2

Separators for 18", 20" and 24" beams are made of $\frac{3}{8}$ " metal.

Separators for 6" to 15" beams are made of $\frac{1}{4}$ " metal.

Minimum widths given. Separators can be made wider.

Cast Separators for Beams Separators with One Bolt

DESIGNATION OF BEAM		DISTANCES		BOLTS		WEIGHTS			
Depth, Inches	Weight, Pounds	Out to Out of Beam Flanges, Inches	Center to Center of Beams, Inches	Size, Inches	 Spacing, Inches	Length for Minimum Width Separator, Inches	Bolts and Nuts, Pounds	Add to Bolts for Each Inch Additional Spread of Beams, Pounds	Add to Separator for Each Inch Additional Spread of Beams, Pounds
12	40	11 1/4	6	3/4	...	7 1/2	1 1/2	0.12	1 1/2
12	31 1/2	10 3/4	5 3/4	3/4	...	7 1/4	1 1/2	0.12	1 1/2
10	25	10 1/2	5 5/8	3/4	...	7	1 1/2	0.12	1 1/2
10	21	9 3/8	5	3/4	...	6 1/4	1 3/8	0.12	1 1/4
9	18	8 3/4	4 3/4	3/4	...	6	1 1/4	0.12	1
8	15	8 1/4	4 1/2	3/4	...	5 3/4	1 1/4	0.12	4 1/2
7	12 1/4	7 1/8	3 3/4	3/4	...	5	1 1/4	0.12	4
6	9 3/4	6 3/8	3 1/2	3/4	...	4 3/4	1 3/8	0.12	3
5	7 1/2	5 1/8	3 1/4	3/4	...	4 1/2	1 1/8	0.12	3
4	5 1/2	5 1/4	3	3/4	...	4	1	0.12	2
3									1 1/4

Separators for 6" to 15" beams are made of 1/4" metal.

Separators for 5" beams and under are made of 3/8" metal.

Minimum widths given. Separators can be made wider.

Standard Bearing Plates

For Beams and Channels Resting on Good Brick Work
Laid in Cement Mortar or High Class Concrete

Depth of Beam or Channel, Inches	Bearing on Wall, Inches	Size of Bearing Plates, Inches	Weight of Bearing Plate, Pounds	Safe Load on Bearing Plates, Tons
6 and less	6	6 x 6 x $\frac{3}{8}$	4	3.6
7 and 8	8	8 x 8 x $\frac{1}{2}$	9	6.4
9 and 10	8	8 x 12 x $\frac{1}{2}$	20	9.6
12	12	12 x 12 x $\frac{3}{4}$	31	14.4
15	12	12 x 16 x $\frac{3}{4}$	41	19.2
18	16	16 x 16 x 1	73	25.6
20	16	16 x 16 x 1	73	25.6
24	16	16 x 16 x 1	73	25.6

Bearing plates are used under the ends of steel beams and channels resting on walls to distribute the pressure on the latter, and must be of sufficient size so that the allowable safe pressure on the wall will not be exceeded.

Beams and girders having greater end reactions than the safe loads given in the above table will require plates of increased size. In such cases the sizes of bearing plates must be determined by the kind of masonry upon which the beams rest; the thickness to be obtained by the following formula:

$$t = \frac{1}{2} (w-b) \sqrt{\frac{3p}{s}}, \text{ in which}$$

t = thickness of plate, in inches.

w = width of plate perpendicular to beam, in inches.

b = width of flange of beam or channel, in inches.

p = allowable pressure on wall, in pounds per square inch.

s = allowable fiber stress in plate, in pounds per square inch.

The maximum allowable pressure on the different kinds of masonry is as follows:

Brick work laid in lime mortar . . .	100 pounds per square inch
Brick work laid in cement mortar . .	200 pounds per square inch
Good stone work	250 pounds per square inch
Portland cement concrete	200 pounds per square inch

Loads on Beams

The determination of the proper size of a rolled beam to use at some given point in a structure is probably the most common task of the designer of structural steel. To determine this it is necessary to know, first, the amount of the loads to which the beam will be subject; second, the character of the loads; and third, the ability of the metal in the beams to resist such loads.

In addition to the above, there will frequently arise a fourth factor to influence the decision, and that is the deformation of the beam under the loading, and the conditions of use, for no beam is or can be perfectly rigid, and the deflection or distortion of the beam under stress can readily be so great as to make the use of a given section inadvisable.

In order to produce static equilibrium, it is necessary in every case that the load on any beam be resisted by corresponding forces acting at the points of support known as the reactions. In the case of a simple beam, uniformly loaded and supported at the ends, the reaction at each end of the beam would be equal to one-half of the load. Where the load is not uniformly distributed then the reactions will vary directly as the intensity of the loading, but in all cases the sum of the reactions will equal the total load to be carried.

As a result of the loads and the accompanying reactions on the beam, there are created forces in the beam tending to shear or cut the beam across in a direction at right angles to its axis. These stresses are known as shearing stresses, and the shear at either support is always equal to the reaction at that support; the shear at any intermediate point in a beam between the supports is always equal to the reaction at the support minus the total load coming on the beam between that support and the point at which it is desired to ascertain the shear.

In the case of the above mentioned simple beam, resting on two supports and carrying a uniform load, the shear or reaction at each support is equal to one-half of the total load on the beam, and the shear decreases uniformly to zero at the center of the span. In the case of a beam loaded with a concentrated load at the center of the span, the reaction at the points of support will also be one-half of the total load. The shear, however, will not decrease towards the center but will remain uniform throughout the entire length of the beam, and would amount to one-half of the total load.

Another effect in the beam, due to the loading and its supporting reaction, is the creation of certain bending stresses in the beam. Taking any point in the length of the beam there will be found

Lloads on Beams

Continued

certain moments due to the loading, and certain counter moments due to the reactions; and the difference between these moments will be the measure of the strength that will have to be supplied by the beam in order that the structure may be in static equilibrium.

This bending moment varies for different points in the length of the beam, and attains a maximum value at that point where the shear mentioned above either becomes zero or changes its sign from positive to negative or from negative to positive.

In the case of a uniformly loaded beam, the point of maximum moment will be at the center of the span, as is also the case of a beam carrying a concentrated load at the center. Where loads are concentrated at several points, the maximum bending moment will always be found at the point of application of one of the loads, the particular load being that which is so located that the sum of all the loads coming on the beam between one of the supports up to and including that load is equal to or greater than the reaction of that support.

The stress in a beam caused by these bending moments, produces flexure in the beam, and the deflection, or the amount of departure of the beam from its unloaded position, is the measure of the deformation which the beam has undergone in its resistance to the bending stresses. This deformation should always be considered as it can readily be a sufficient amount to cause serious difficulties with other materials or other parts of the structure that are dependent on the beam under consideration for their support.

In calculations made for determining the sizes of beams, the loads are usually expressed in pounds, the length of the span and the distance between loads in feet and tenths of a foot, and the resulting bending moments in terms of foot pounds. This promotes convenience in handling figures, although it is necessary to convert these foot pounds into inch pounds before consulting tables of properties for the selection of the desired section.

The section modulus of the desired section is readily obtained by dividing the maximum bending moment, expressed in inch pounds, by the maximum allowed stress in the extreme fiber of the section, as expressed in pounds per square inch. Care should always be taken, however, in such cases to see that the neutral axis of the section is perpendicular to the line of action of the load. Should this not be the case careful investigation should be made so that due provision for the eccentricity of the loading can be made.

Explanation of Tables of Structural Sections Used as Beams

The tables on pages 147 to 166 give the safe loads of beams, channels, angles, tees, and zeos when used under a uniformly distributed transverse load. These loads are expressed in thousands of pounds for the more usual spans and are based upon the customary fiber stress of 16,000 pounds per square inch used in building construction.

These tables also give the length of span at which the safe load, based on 16,000 pounds per square inch extreme fiber stress, will result in a deflection amounting to $1/360$ of the length of the span in feet. The loads given in all cases include the weight of the beam itself, which weight should be deducted from the gross capacity of the beam to determine the net load, should the accuracy of the calculation require such refinement.

It has been assumed in all cases in these tables that the loads are applied perpendicular to the beam and in the plane of their webs.

Should the conditions under which the loads are applied to the beam involve the necessity of resisting forces outside of this assumption, it will not be safe to use these tabular loads, and the required section would then have to be obtained by the application of the general theory of flexure.

For angles and zeos and other unsymmetrical sections, it will be necessary to see that the section is so secured as to prevent any twisting, as otherwise, on account of the shape of the section, failure would occur with a much lower load.

In building construction, where beams carry ceilings having a plastered finish, experience has indicated that vertical deflection of the beams should be limited to not more than $1/360$ of the span in length, or as it is sometimes expressed, $1/30$ of an inch for each foot of span.

This limit is indicated in the tables by the lower zigzag line and beams should not be used for a greater span than is thus indicated *unless the tabular safe loads exceed the actual load to be carried on the beam.*

Explanation of Tables of Structural Sections Used as Beams

Continued

For the purpose of readily determining the deflection there will be found in these tables coefficients of deflection based on the loads given. These coefficients correspond to extreme fiber stresses of 16,000 pounds per square inch and are constant for all depths of beams. The deflection can readily be found for any span at the tabular load by dividing this coefficient by the depth of the beam in inches. To find the deflection under tabular load of sections unsymmetrical to the neutral axis such as angles and tees, divide the corresponding coefficient by twice the distance from neutral axis to extreme fiber. This distance can readily be obtained from the tables of properties of sections.

To find the deflection under any other fiber stress than of the 16,000 pounds per square inch used in the tables, it will be necessary to multiply the tabular coefficient of deflection for the span in question by the proposed fiber stress and divide the product by 16,000. This will give a new coefficient from which the desired deflection can be obtained.

The safe loads given in these tables are further based on the assumption that the compression flanges of the section will be secured against lateral deflection. The better class of construction specifications usually provide that no beam shall be used in which the compression flange is without lateral support for a distance exceeding forty times its width, and that the unit stress should be reduced whenever the unsupported width exceeds ten times the flange width. Placed in tabular form this reduction should be as follows:

10 times flange width	Full tabular load
15 times flange width	90% tabular load
20 times flange width	81% tabular load
25 times flange width	71% tabular load
30 times flange width	62% tabular load
35 times flange width	53% tabular load
40 times flange width	43% tabular load

The expert designer will readily recognize the danger arising from the use of a long narrow beam without lateral support, and while

Explanation of Tables of Structural Sections Used as Beams

Continued

there may be conditions under which the use of such a beam would be justified, for all ordinary cases the specification limit of forty times the flange width for the unsupported length should be adhered to. Particularly as, in addition to the tendency to lateral deflection due to vertical loading, there is always the possibility of developing other lateral influences through the action of floor arches, wind stresses or other incidental loadings that are frequently neglected or lost sight of in designing.

It is further assumed that all loads are static. Where moving loads are to be cared for, it will be necessary to reduce the stress in the material, either by reducing the allowable unit stresses used in designing or else by increasing the theoretical loads. Where loads are suddenly applied, the resulting stresses are greater than would be due to the same load carried as a static load. These stresses increase as the time of application of the load is decreased. When the load is applied instantaneously, the stresses due to that load are double the stress due to a quiescent load of the same amount.

Where the loading is such as to produce impact or percussion, the stresses resulting therefrom are dynamic and are to be measured by the laws governing the energy of bodies in motion. There are certain empirical formulae that may be used in determining the approximate fiber stress, also the deflection due to a load applied with impact at the center of a beam supported at both ends. These are as follows:

$$fd = f \left(1 + \sqrt{\frac{2mh}{D}} + 1 \right) \text{ and } Dd = D + \sqrt{2mhD + D^2}$$

in which formulae the following symbols are used:

W = Weight of load, in pounds.

W_1 = Weight of beam, in pounds.

h = Height of fall, in inches.

f = Extreme fiber stress due to static load, $W + W_1$, in pounds per square inch.

fd = Extreme fiber stress due to dynamic load, W , in pounds per square inch.

Explanation of Tables of Structural Sections Used as Beams

Continued

D = Deflection due to static load, $W + W_1$, in inches.

Dd = Deflection due to dynamic load, W , in inches.

$$m = \frac{35 W}{35 W + 17 W_1}$$

On account of the excess metal required in the webs of beams and channels to satisfy rolling conditions, the safe loads for beams and channels are computed almost solely with reference to the stresses due to flexure, and, under uniformly distributed loads, the spans given will not produce a shearing stress in the webs greater than 10,000 pounds per square inch, which is within that allowed by the majority of good construction specifications. Conditions can arise, however, for instance with beams subjected to heavy loads that are concentrated near the supports, or when beams with short spans are loaded with a uniformly distributed load, that would absorb their full carrying capacity as regards flexure. It can be readily seen that under these conditions bending moments developed may be small as compared with the reactions at the supports, so that while the beam may be amply strong to resist bending it may be in a precarious condition as regards shearing stresses, or may buckle the webs as a result of vertical stresses in the webs.

For such conditions the safe carrying capacity of the beam is limited by the capacity to resist shearing or buckling of the web rather than by the ability of the flanges to resist bending.

In the consideration of the loading of beams, there remains one other point to be considered, and that is the possibility of the buckling or crippling of the webs, either at points of concentrated loading or under the influence of the reactions from the supports.

The resistance of a beam to such crippling is largely a question of web thickness and the safe end reaction may be expressed by the

formula $R = fb \times t \left(a + \frac{d}{4} \right)$ and the crippling under an inter-

Explanation of Tables of Structural Sections Used as Beams

Continued

mediate concentrated load may be expressed by the formula

$W = 2fb \times t \left(a' + \frac{d}{4} \right)$. In which formulae R represents the end

reaction, W the intermediate concentrated load, t the thickness of web, d the depth of the beam, a' half the distance over which the concentrated load is distributed, a the distance which the end of the beam rests upon the supports, and fb the safe carrying capacity of the web against buckling, for which the usual column formulae of

$16,000 - 70 \frac{l}{r}$ can be used, modifying it, however, so that in place

of l there is used one-half the depth of the beam.

Continued on next page.

Explanation of Tables of Structural Sections Used as Beams

Continued

Placed in tabular form the capacity of beams to resist shear buckling and end reaction is as follows:

Depth of Beam, Inches	Weight per Foot, Pounds	Thickness of Web, Inches	Total Allowable Web Shear at 10,000 Pounds per Square Inch, Pounds	Allowable Buckling Stress (f_b), Pounds per Square Inch	Maximum End Reaction, Assuming $3\frac{1}{4}$ " Bearing, Pounds
24	115.0	.750	180,000	12,120	86,360
24	80.0	.500	120,000	10,180	48,360
20	100.0	.884	176,800	13,260	99,640
20	65.0	.500	100,000	11,150	47,390
18	90.0	.807	145,260	13,300	85,870
18	55.0	.460	82,800	11,260	41,420
15	75.0	.882	132,300	13,940	89,140
15	42.0	.410	61,500	11,570	34,390
12	55.0	.821	98,520	14,230	75,940
12	31.5	.350	42,000	11,840	26,940
10	40.0	.749	74,900	14,380	64,620
10	25.0	.310	31,000	12,090	22,490
9	35.0	.732	65,880	14,510	61,070
9	21.0	.275	24,750	12,080	19,100
8	25.5	.541	43,280	14,210	42,280
8	18.0	.270	21,600	12,410	18,430
7	20.0	.458	32,060	14,150	34,020
7	15.0	.250	17,500	12,600	16,540
6	17.25	.475	28,500	14,470	34,370
6	12.25	.230	13,800	12,840	14,770
5	14.75	.504	25,200	14,800	35,430
5	9.75	.210	10,500	13,110	13,080
4	10.5	.410	16,400	14,820	27,340
4	7.5	.190	7,600	13,460	11,510
3	7.5	.361	10,830	15,000	23,020
3	5.5	.170	5,100	13,860	10,010

Bending Moments and Deflection of Beams

Various Systems of Loading

Notation in Formulae

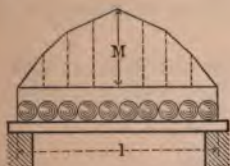
- A = Area of section, in square inches.
 n = Distance from center line of gravity to extreme fiber, in inches.
 I = Moment of inertia about center line of gravity, in inches.
 M_s = Static moment, in inches.
 S = Section modulus = I/n , in inches.
 r = Radius of gyration = $\sqrt{I/A}$, in inches.
 f = Bending stress in extreme fiber, in pounds per square inch.
 fb = Resistance of web, in pounds per square inch.
 E = Modulus of elasticity, in pounds per square inch, about 29,000,000.
 L = Length of section, in feet.
 l = Length of section, in inches.
 d = Depth of section, in inches.
 b = Width of section, in inches.
 t = Thickness of section, in inches.
 W, W_1, W_2 = Superimposed loads supported by beam, in pounds.
 w = Superimposed load, in pounds per unit length of area.
 W_{max} = Maximum safe load at point given, in pounds.
 R, R_1 = Reactions at points of support, in pounds.
 V = Vertical shear, in pounds.
 M, M_1, M_2 = Bending moments at points given, in inch pounds.
 M_{max} = Maximum bending moment, in inch pounds.
 Mr = Maximum resisting moment, in inch pounds = $f I/n = f S$.
 D, D_1 = Deflections at points given, in inches.
 D_{max} = Maximum deflection at point given, in inches.

Bending Moments and Deflections of Beams

Various Systems of Loading

Continued

1. Beam supported at both ends and uniformly loaded.



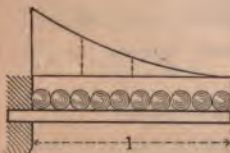
$$\begin{aligned} \text{Max. shear} &= \frac{W}{2} \\ M \text{ max. at center} &= \frac{Wl}{8} \\ W \text{ max.} &= \frac{8fs}{l} \\ D \text{ max.} &= \frac{Wl^3}{78.6EI} \end{aligned}$$

2. Beam supported at both ends with load concentrated at the middle.



$$\begin{aligned} \text{Max. shear} &= \frac{W}{2} \\ M \text{ max., at point of load} &= \frac{Wl}{4} \\ W \text{ max.} &= \frac{4fs}{l} \\ D \text{ max.} &= \frac{Wl^3}{48EI} \end{aligned}$$

3. Beam fixed at one end, unsupported at the other and uniformly loaded.



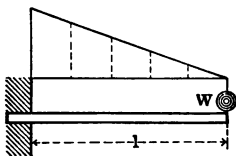
$$\begin{aligned} \text{Max. shear} &= W \\ M \text{ max., at point of support} &= \frac{Wl}{2} \\ W \text{ max.} &= \frac{2fs}{l} \\ D \text{ max.} &= \frac{Wl^3}{8EI} \end{aligned}$$

Bending Moments and Deflections of Beams

Various Systems of Loading

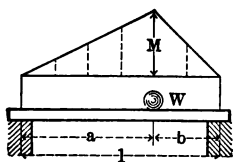
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4. Beam fixed at one end, unsupported at the other, with load concentrated at the free end.



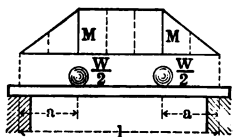
$$\begin{aligned} \text{Max. shear} &= W \\ M \text{ max., at point of support} &= W l \\ W \text{ max.} &= \frac{f s}{l} \\ D \text{ max.} &= \frac{W l^3}{3 E I} \end{aligned}$$

5. Beam supported at both ends with load concentrated at any point.



$$\begin{aligned} \text{Max. shear if } b \text{ is greater than } a &= \frac{W b}{l} \\ \text{Max. shear if } a \text{ is greater than } b &= \frac{W a}{l} \\ M \text{ max., at point of load} &= \frac{W a b}{l} \\ W \text{ max.} &= \frac{f s l}{a b} \\ D \text{ max.} &= \frac{W a b (a + 2 b) \sqrt{3 a (a + 2 b)}}{27 E I l} \end{aligned}$$

6. Beam supported at both ends with two symmetrical loads.



$$\begin{aligned} \text{Max. shear} &= \frac{W}{2} \\ M \text{ max. at and between loads} &= \frac{W a}{2} \\ W \text{ max.} &= \frac{2 f s}{a} \\ D \text{ max.} &= \frac{W a}{48 E I} (3 l^3 - 4 a^3) \end{aligned}$$

Bending Moments and Deflections of Beams

Various Systems of Loading

Continued

7. Beam supported at both ends with loads concentrated at various points.



$$R = \frac{Wb + W_1b_1 + W_2b_2}{l}$$

$$R_1 = \frac{Wa + W_1a_1 + W_2a_2}{l}$$

M at $W = Ra$

Max. if $W =$ or is greater than R

M at $W_1 = Ra_1 - W(a_1 - a)$

M max. if $W_1 + W = R$ or is greater than R

M max. if $W_1 + W_2 = R_1$ or is greater than R_1

M at $W_2 = Ra_2 - W(a_2 - a) - W_1(a_2 - a_1)$

M max. if $W_2 = R_1$ or is greater than R_1

8. Beam fixed at both ends and uniformly loaded.

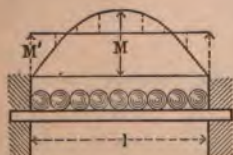
Distance of points of extra flexure from supports = $.2113 \times l$

Max. bending mom. at points of support = $\frac{Wl}{12}$

Bending mom. at middle of beam = $\frac{Wl}{24}$

Max. shear at points of support = $\frac{W}{2}$

D max. = $\frac{Wl^3}{384EI}$

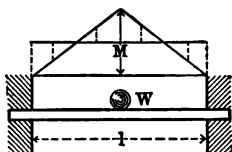


Bending Moments and Deflections of Beams

Various Systems of Loading

Continued

9. Beam fixed at both ends with load concentrated at the middle.
Distance of points of contra-flexure



$$\text{from supports} = \frac{1}{4} l$$

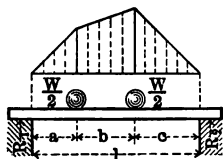
$$\text{Max. bending mom. at points of support} = \frac{P l}{8}$$

$$\text{Bending mom. at middle of beam} = \frac{P l}{8}$$

$$\text{Max. shear at points of support} = \frac{P}{2}$$

$$\text{Max. deflection} = \frac{P l^3}{192 E I}$$

10. Beam supported at both ends with two unsymmetrical loads concentrated at various points.



$$R_1 \text{ max. shear if } a = \frac{W}{2l} (l - a + c) \text{ is less than } c$$

$$R_2 = \frac{W}{2l} (l + a - c)$$

$$M \text{ max. distance } c \text{ (when } c \text{ is less than } a) = R_1 C = \frac{W c}{2l} (l + a - c)$$

$$W \text{ max. (when } c \text{ is less than } a) = \frac{2 l f s}{c (l + a - c)}$$

Bending Moments and Deflections of Beams

Various Systems of Loading

Continued

11. Beam supported at both ends with a uniform load partially distributed.



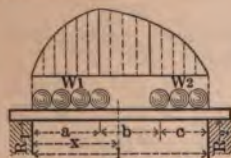
$$R_1 \text{ max. shear if } a \text{ is less than } c = \frac{W(2c + b)}{2l}$$

$$R_2 = \frac{W(2a + b)}{2l}$$

$$M \text{ max. dist. } a + \frac{R_1 b}{W} = \frac{W(2c + b)[4al + b(2c + b)]}{8l^2}$$

$$W \text{ max.} = \frac{8l^2 f s}{(2c + b)[4al + b(2c + b)]}$$

12. Beam supported at both ends with a uniform load partially discontinued.



$$R_1 \text{ max. shear if } W_1 \text{ is greater than } W_2 = \frac{W_1(2l - a) + W_1 c}{2l}$$

$$R_2 = \frac{W_2(2l - c) + W_1 a}{2l}$$

$$M \text{ max. dist. } \times \frac{2W_1 a l - W_1 a^2 + W_2 c a}{2W_1 l} = \frac{R^2 a}{2W}$$

$$W \text{ max. when } W_1 a \text{ is greater than } W_2 c = \frac{R^2 a}{2 f s}$$

Structural Beams

Allowable Uniform Loads in Thousands of Pounds

Extreme Fiber Stress, 16,000 Pounds per Square Inch
Safe Loads Include Weight of Beam

Span in Feet	DEPTH AND WEIGHT OF SECTIONS								Co- efficient of Deflec- tion
	24-Inch								
	115 lbs.	110 lbs.	105 lbs.	100 lbs.	95 lbs.	90 lbs.	85 lbs.	80 lbs.	
6				361.9					0.60
7	360.0	330.2		352.5	332.6	302.9			0.80
8	328.4	320.4	300.0	302.2	293.2	284.2	273.6	240.0	1.06
9	291.9	284.8		264.4	256.6	248.7	240.9	231.9	1.34
10	262.7	256.3		235.0	228.0	221.1	214.1	206.1	1.66
11	238.8	233.0		211.5	205.2	199.0	192.7	185.5	2.00
12	218.9	213.6		192.3	186.6	180.9	175.2	168.7	2.38
13	202.1	197.2		176.3	171.0	165.8	160.6	154.6	2.80
14	187.7	183.1		162.7	157.9	153.1	148.2	142.7	3.24
15	187.7	183.1		151.1	146.6	142.1	137.6	132.5	3.72
16	175.1	170.9		141.0	136.8	132.6	128.5	123.7	4.24
17	164.2	160.2		132.2	128.3	124.4	120.4	116.0	4.78
18	154.5	150.8		124.4	120.7	117.0	113.4	109.1	5.36
19	146.0	142.4		138.8	117.5	114.0	110.5	107.1	5.98
20	138.3	134.9		131.5	111.3	108.0	104.7	101.4	6.62
21	131.4	128.2		125.0	105.8	102.6	99.5	96.3	7.30
22	125.1	122.1		119.0	100.7	97.7	94.7	91.8	8.01
23	119.4	116.5		113.6	96.1	93.3	90.4	87.6	8.76
24	114.2	111.4		108.7	92.0	89.2	86.5	83.8	9.53
25	109.5	106.8		104.1	88.1	85.5	82.9	80.3	10.35
26	105.1	102.5		100.0	84.6	82.1	79.6	77.1	11.19
27	101.0	98.6		96.1	81.4	78.9	76.5	74.1	12.07
28	97.3	94.9		92.6	78.3	76.0	73.7	71.4	12.98
29	93.8	91.5		89.3	75.5	73.3	71.1	68.8	13.92
30	90.6	88.4		86.2	72.9	70.8	68.6	66.4	14.90
31	87.6	85.4		83.3	70.5	68.4	66.3	64.2	15.91
32	84.7	82.7		80.6	68.2	66.2	64.2	62.2	16.95
33	82.1	80.1		78.1	66.1	64.1	62.2	60.2	18.03
34	79.6	77.7		75.7	64.1	62.2	60.3	58.4	19.13
35	77.3	75.4		73.5	62.2	60.4	58.5	56.7	20.28
36	75.1	73.2		71.4	60.4	58.6	56.8	55.1	21.45
37	73.0	71.2		69.4	58.8	57.0	55.3	53.5	22.66
38	71.0	69.3		67.5	57.2	55.5	53.8	52.1	23.90
39	69.1	67.5		65.8	55.7	54.0	52.4	50.7	25.18
40	67.4	65.7		64.1	54.2	52.6	51.0	49.4	26.48
41	65.7	64.1		62.5	52.9	51.3	49.7	48.2	27.82
42	64.1	62.5		61.0	51.6	50.1	48.5	47.0	29.20
43	62.6	61.0		59.5	50.4	48.9	47.4	45.9	30.60
44	61.1	59.6		58.1	49.2	47.7	46.3	44.8	32.04
45	59.7	58.3		56.8	48.1	46.6	45.2	43.8	33.52
46	58.4	57.0		55.5	47.0	45.6	44.2	42.8	35.02
47	57.1	55.7		54.3	46.0	44.6	43.3	41.9	36.56
48	55.9	54.1		53.2	45.0	43.7	42.3	41.0	38.14
49	54.7	53.4		52.1	44.1	42.8	41.5	40.1	39.74
50	53.6	52.3		51.0	43.2	41.9	40.6	39.3	41.38
50	52.5	51.3		50.0	42.3	41.0	39.8	38.5	43.04

Loads above horizontal lines will produce maximum allowable shear in webs.
Loads below dotted lines will produce excessive deflections.
For maximum safe loads, see page 140.

Structural Beams

Allowable Uniform Loads in Thousands of Pounds

Continued

Extreme Fiber Stress, 16,000 Pounds per Square Inch
Safe Loads Include Weight of Beam

Span in Feet	DEPTH AND WEIGHT OF SECTIONS												Co- efficient of Deflec- tion
	20-Inch								18-Inch				
	100 lbs.	95 lbs.	90 lbs.	85 lbs.	80 lbs.	75 lbs.	70 lbs.	65 lbs.	90 lbs.	85 lbs.	80 lbs.	75 lbs.	
5	353.6 353.2												0.4
6		324.0	294.8			259.6	239.0		290.5	261.0			0.60
7	294.3	285.6	276.9	265.2	240.0	225.6	216.8	200.0	249.0	241.1	231.8	202.3	0.81
8	252.3	244.8	237.7	229.9	223.4	193.3	185.9	178.2	213.4	206.7	200.0	193.2	1.06
9	220.7	214.2	207.7	201.1	195.5	169.2	162.6	155.9	186.7	180.8	175.0	169.1	1.34
10	196.2	190.4	184.6	178.8	173.8	150.4	144.6	138.6	166.0	160.7	155.5	150.3	1.66
	176.6	171.4	166.1	160.9	156.4	135.3	130.1	124.7	149.4	144.7	140.0	135.3	
11	160.5	155.8	151.0	146.3	142.2	123.0	118.3	113.4	135.8	131.5	127.2	123.0	2.00
12	147.2	142.8	138.5	134.1	130.3	112.8	108.4	104.0	124.5	120.6	116.6	112.7	2.38
13	135.8	131.8	127.8	123.8	120.3	104.1	100.1	96.0	114.9	111.3	107.7	104.1	2.80
14	126.1	122.4	118.7	114.9	111.7	96.7	92.9	89.1	106.7	103.3	100.0	96.6	3.24
15	117.7	114.2	110.8	107.3	104.3	90.2	86.7	83.2	99.6	96.4	93.3	90.2	3.72
16	110.4	107.1	103.8	100.6	97.7	84.6	81.3	78.0	93.4	90.4	87.5	84.5	4.24
17	103.9	100.8	97.7	94.1	92.0	79.6	76.5	73.4	87.9	85.1	82.3	79.6	4.78
18	98.1	95.2	92.3	89.4	86.9	76.3	72.3	69.3	83.0	80.4	77.8	75.1	5.36
19	92.9	90.2	87.4	84.7	82.3	71.2	68.5	65.7	78.6	76.1	73.7	71.2	5.98
20	88.3	85.7	83.1	80.5	78.2	67.7	65.1	62.4	74.7	72.3	70.0	67.6	6.62
21	84.1	81.6	79.1	76.6	74.5	64.4	62.0	59.4	71.1	68.9	66.7	64.4	7.30
22	80.3	77.9	75.5	73.1	71.1	61.5	59.1	56.7	67.9	65.8	63.6	61.5	8.01
23	76.8	74.5	72.2	70.0	68.0	58.8	56.6	54.2	64.9	62.9	60.9	58.8	8.76
24	73.6	71.4	69.2	67.0	65.2	56.4	54.2	52.0	62.2	60.3	58.3	56.4	9.53
25	70.6	68.5	66.5	64.4	62.6	54.1	52.0	49.9	59.8	57.9	56.0	54.1	10.35
26	67.9	65.9	63.9	61.9	60.2	52.1	50.0	48.0	57.5	55.6	53.8	52.0	11.19
27	65.4	63.5	61.5	59.6	57.9	50.1	48.2	46.2	55.3	53.6	51.8	50.1	12.07
28	63.1	61.2	59.3	57.5	55.9	48.3	46.5	44.6	53.3	51.7	50.0	48.3	12.98
29	60.9	59.1	57.3	55.5	53.9	46.7	44.9	43.0	51.5	49.9	48.3	46.6	13.92
30	58.9	57.1	55.4	53.6	52.1	45.1	43.4	41.6	49.8	48.2	46.7	45.1	14.90
31	57.0	55.3	53.6	51.9	50.5	43.7	42.0	40.2	48.2	46.7	45.2	43.6	15.91
32	55.2	53.6	51.9	50.3	48.9	42.3	40.7	39.0	46.7	45.2	43.7	42.3	16.95
33	53.5	51.9	50.4	48.8	47.4	41.0	39.4	37.8	45.3	43.8	42.4	41.0	18.03
34	51.9	50.4	48.9	47.3	46.0	39.8	38.3	36.7	43.9	42.6	41.2	39.8	19.13
35	50.5	49.0	47.5	46.0	44.7	38.7	37.2	35.6	42.7	41.3	40.0	38.6	20.28
36	49.1	47.6	46.2	44.7	43.4	37.6	36.1	34.7	41.5	40.2	38.9	37.6	21.45
37	47.7	46.3	44.9	43.5	42.3	36.6	35.2	33.7	40.4	39.1	37.8	36.6	22.66
38	46.5	45.1	43.7	42.3	41.2	35.6	34.2	32.8	39.3	38.1	36.8	35.6	23.90
39	45.3	43.9	42.6	41.3	40.1	34.7	33.4	32.0					25.18
40	44.1	42.8	41.5	40.2	39.1	33.8	32.5	31.2					26.48
41	43.1	41.8	40.5	39.2	38.1	33.0	31.7	30.4					27.82
42	42.0	40.8	39.6	38.3	37.2	32.2	31.0	29.7					29.20

Loads above horizontal lines will produce maximum allowable shear in webs.
Loads below dotted lines will produce excessive deflections.
For maximum safe loads, see page 140.

Structural Beams

Allowable Uniform Loads in Thousands of Pounds

Continued

Extreme Fiber Stress, 16,000 Pounds per Square Inch

Safe Loads Include Weight of Beam

Span in Feet	DEPTH AND WEIGHT OF SECTIONS												Co- efficient of Deflec- tion
	18 Inch				15 Inch								
	70 lbs.	65 lbs.	60 lbs.	55 lbs.	75 lbs.	70 lbs.	65 lbs.	60 lbs.	55 lbs.	50 lbs.	45 lbs.	42 lbs.	
					264.6				196.8				
4	258.8	229.3	199.8		245.8	235.2	205.8	177.0	181.7	167.4	138.0		0.27
5	218.4	208.9	199.5		196.6	188.8	180.9	173.2	145.4	137.5	129.7		0.41
				165.6								123.0	
6	182.0	174.1	166.3	157.1	163.8	157.3	150.8	144.4	121.1	114.6	108.1	104.8	0.60
7	156.0	149.2	142.5	134.7	140.4	134.8	129.2	123.7	103.8	98.2	92.6	89.8	0.81
8	136.5	130.6	124.7	117.9	122.9	118.0	113.1	108.3	90.8	85.9	81.0	78.5	1.06
9	121.3	116.1	110.9	104.8	109.2	104.9	100.5	96.2	80.8	76.4	72.0	69.8	1.34
10	109.2	104.5	99.8	94.3	98.3	94.4	90.5	86.6	72.7	68.8	64.8	62.8	1.66
11	99.3	95.0	90.7	85.7	89.4	85.8	82.2	78.7	66.1	62.5	58.9	57.1	2.00
12	91.0	87.1	83.1	78.6	81.9	78.7	75.4	72.2	60.6	57.3	54.0	52.4	2.38
13	84.0	80.4	76.7	72.5	75.6	72.6	69.6	66.6	55.9	52.9	49.9	48.3	2.80
14	78.0	74.6	71.3	67.3	70.2	67.4	64.6	61.9	51.9	49.1	46.3	44.9	3.24
15	72.8	69.6	66.5	62.9	65.5	62.9	60.3	57.7	48.5	45.8	43.2	41.9	3.72
16	68.2	65.3	62.4	58.9	61.4	59.0	56.5	54.1	45.4	43.0	40.5	39.3	4.24
17	64.2	61.5	58.7	55.5	57.8	55.5	53.2	50.9	42.8	40.4	38.1	37.0	4.78
18	60.7	58.0	55.4	52.4	54.6	52.4	50.3	48.1	40.4	38.2	36.0	34.9	5.36
19	57.5	55.0	52.5	49.6	51.7	49.7	47.6	45.6	38.3	36.2	34.1	33.1	5.98
20	54.6	52.2	49.9	47.1	49.2	47.2	45.2	43.3	36.3	34.4	32.4	31.4	6.62
21	52.0	49.7	47.5	44.9	46.8	44.9	43.1	41.2	34.6	32.7	30.9	29.9	7.30
22	49.6	47.5	45.3	42.9	44.7	42.9	41.1	39.4	33.0	31.3	29.5	28.6	8.01
23	47.5	45.4	43.4	41.0	42.7	41.0	39.3	37.7	31.6	29.9	28.2	27.3	8.76
24	45.5	43.5	41.6	39.3	41.0	39.3	37.7	36.1	30.3	28.6	27.0	26.2	9.53
25	43.7	41.8	39.9	37.7	39.3	37.8	36.2	34.6	29.1	27.5	25.9	25.1	10.35
26	42.0	40.2	38.4	36.3	37.8	36.3	34.8	33.3	28.0	26.4	24.9	24.2	11.19
27	40.4	38.7	37.0	34.9	36.4	35.0	33.5	32.1	26.9	25.5	24.0	23.3	12.07
28	39.0	37.3	35.6	33.7	35.1	33.7	32.3	30.9	26.0	24.6	23.2	22.4	12.98
29	37.6	36.0	34.4	32.5	33.9	32.5	31.2	29.9	25.1	23.7	22.4	21.7	13.92
30	36.4	34.8	33.3	31.4	32.8	31.5	30.2	28.9	24.2	22.9	21.6	20.9	14.90
31	35.2	33.7	32.2	30.4	31.7	30.4	29.2	27.9	23.4	22.2	20.9	20.3	15.91
32	34.1	32.6	31.2	29.5	30.7	29.5	28.3	27.1	22.7	21.5	20.3	19.6	16.95
33	33.1	31.7	30.2	28.6									18.03
34	32.1	30.7	29.3	27.7									19.13
35	31.2	29.8	28.5	26.9									20.28
36	30.3	29.0	27.7	26.2									21.45
37	29.5	28.2	27.0	25.5									22.66
38	28.7	27.5	26.3	24.8									23.90

Loads above horizontal lines will produce maximum allowable shear in webs.
 Loads below dotted lines will produce excessive deflections.
 For maximum safe loads, see page 140.

Structural Beams

Allowable Uniform Loads in Thousands of Pounds

Continued

Extreme Fiber Stress, 16,000 Pounds per Square Inch

Safe Loads Include Weight of Beam

Span in Feet	DEPTH AND WEIGHT OF SECTIONS										Co- efficient of Deflec- tion
	12 Inch						10 Inch				
	55 lbs.	50 lbs.	45 lbs.	40 lbs.	35 lbs.	31½ lbs.	40 lbs.	35 lbs.	30 lbs.	25 lbs.	
3	197.0						149.8	120.4			
4	190.2	167.8	138.2		104.6		112.8	104.1	91.0		0.15
5	142.7	134.8	127.0	110.4	101.5	84.0	84.6	78.1	71.6	62.0	0.27
6	114.1	107.9	101.6	95.6	81.2	76.7	67.7	62.5	57.2	52.1	0.41
7	95.1	89.9	84.7	79.7	67.6	63.9	56.4	52.1	47.7	43.4	0.60
8	81.5	77.0	72.6	68.3	58.0	54.8	48.4	44.6	40.9	37.2	0.81
9	71.3	67.4	63.5	59.8	50.7	48.0	42.3	39.0	35.8	32.6	1.06
10	63.4	59.9	56.4	53.1	45.1	42.6	37.6	34.7	31.8	28.9	1.34
11	57.1	53.9	50.8	47.8	40.6	38.4	33.9	31.2	28.6	26.0	1.66
12	51.9	49.0	46.2	43.5	36.9	34.9	30.8	28.4	26.0	23.7	2.00
13	47.6	44.9	42.3	39.8	33.8	32.0	28.2	26.0	23.9	21.7	2.38
14	43.9	41.5	39.1	36.8	31.2	29.5	26.0	24.0	22.0	20.0	2.80
15	40.8	38.5	36.3	34.2	29.0	27.4	24.2	22.3	20.4	18.6	3.24
16	38.0	36.0	33.9	31.9	27.1	25.6	22.6	20.8	19.1	17.4	3.72
17	35.7	33.7	31.7	29.9	25.4	24.0	21.2	19.5	17.9	16.3	4.24
18	33.6	31.7	29.9	28.1	23.9	22.6	19.9	18.4	16.8	15.3	4.78
19	31.7	30.0	28.2	26.6	22.5	21.3	18.8	17.4	15.9	14.5	5.36
20	30.0	28.4	26.7	25.2	21.4	20.2	17.8	16.4	15.1	13.7	5.98
21	28.5	27.0	25.4	23.9	20.3	19.2	16.9	15.6	14.3	13.0	6.62
22	27.2	25.7	24.2	22.8	19.3	18.3	16.1	14.9	13.6	12.4	7.30
23	25.9	24.5	23.1	21.7	18.4	17.4	15.4	14.2	13.0	11.8	8.01
24	24.8	23.4	22.1	20.8	17.6	16.7					8.76
25	23.8	22.5	21.2	19.9	16.9	16.0					9.53
26	22.8	21.6	20.3	19.1	16.2	15.3					10.35
27	21.9	20.7	19.5	18.4	15.6	14.8					11.19
28											12.07
29											12.98
30											13.92
31											14.90
32											15.91
											16.95

Loads above horizontal lines will produce maximum allowable shear in webs.
 Loads below dotted lines will produce excessive deflections.
 For maximum safe loads, see page 140.

Structural Beams

Allowable Uniform Loads in Thousands of Pounds

Continued

Extreme Fiber Stress, 16,000 Pounds per Square Inch
Safe Loads Include Weight of Beam

Span in Feet	DEPTH AND WEIGHT OF SECTIONS											Coeffi- cient of Deflec- tion
	9 Inch				8 Inch				7 Inch			
	35 lbs.	30 lbs.	25 lbs.	21 lbs.	25½ lbs.	23 lbs.	20½ lbs.	18 lbs.	20 lbs.	17½ lbs.	15 lbs.	
	131.8	102.4	73.1		86.6	71.8	57.1		64.1	49.4		
3	88.3	80.5	72.6		60.8	57.3	53.9	43.2	42.9	39.8	35.0	0.15
4	66.2	60.4	54.5	49.5	45.6	43.0	40.4	37.9	32.1	29.9	27.6	0.27
5	53.0	48.3	43.6	39.9	36.5	34.4	32.3	30.3	25.7	23.9	22.1	0.41
6	44.2	40.2	36.3	33.2	30.4	28.7	26.9	25.3	21.4	19.9	18.4	0.60
7	37.9	34.5	31.1	28.5	26.1	24.6	23.1	21.7	18.4	17.1	15.8	0.81
8	33.1	30.2	27.2	24.9	22.8	21.5	20.2	19.0	16.1	14.9	13.8	1.06
9	29.4	26.8	24.2	22.2	20.3	19.1	18.0	16.9	14.3	13.3	12.3	1.34
10	26.5	24.1	21.8	19.9	18.2	17.2	16.2	15.2	12.9	11.9	11.0	1.66
11	24.1	22.0	19.8	18.1	16.6	15.6	14.7	13.8	11.7	10.9	10.0	2.00
12	22.1	20.1	18.2	16.6	15.2	14.3	13.5	12.6	10.7	10.0	9.2	2.38
13	20.4	18.6	16.8	15.3	14.0	13.2	12.4	11.7	9.9	9.2	8.5	2.80
14	18.9	17.2	15.6	14.2	13.0	12.3	11.5	10.8	9.2	8.5	7.9	3.24
15	17.7	16.1	14.5	13.3	12.2	11.5	10.8	10.1	8.6	8.0	7.4	3.72
16	16.6	15.1	13.6	12.5	11.4	10.8	10.1	9.5	8.0	7.5	6.9	4.24
17	15.6	14.2	12.8	11.7	10.7	10.1	9.5	8.9				4.78
18	14.7	13.4	12.1	11.1	10.1	9.6	9.0	8.4				5.36
19	13.9	12.7	11.5	10.5								5.98
20	13.3	12.1	10.9	10.0								6.62

Span in Feet	DEPTH AND WEIGHT OF SECTIONS												Coeffi- cient of Deflec- tion	
	6 Inch			5 Inch			4 Inch				3 Inch			
	17¼ lbs.	14¾ lbs.	12¼ lbs.	14¾ lbs.	12¼ lbs.	9¾ lbs.	10½ lbs.	9½ lbs.	8½ lbs.	7½ lbs.	7½ lbs.	6½ lbs.		5½ lbs.
1	57.0			50.4	35.7		32.8	27.0	21.0		21.7			0.02
2	46.6	42.2	27.6	32.3	29.1	21.0	19.0	18.0	16.9	15.2	10.4	9.6	8.8	0.07
3	31.0	28.4	25.8	21.5	19.4	17.2	12.7	12.0	11.3	10.6	6.9	6.4	5.9	0.15
4	23.3	21.3	19.4	16.2	14.5	12.9	9.5	9.0	8.5	8.0	5.2	4.8	4.4	0.27
5	18.6	17.1	15.5	12.9	11.6	10.3	7.6	7.2	6.8	6.4	4.1	3.8	3.5	0.41
6	15.5	14.2	12.9	10.8	9.7	8.6	6.3	6.0	5.6	5.3	3.5	3.2	2.9	0.60
7	13.3	12.2	11.1	9.2	8.3	7.4	5.4	5.1	4.8	4.5	3.0	2.7	2.5	0.81
8	11.6	10.7	9.7	8.1	7.3	6.4	4.8	4.5	4.2	4.0	2.6	2.4	2.2	1.06
9	10.3	9.5	8.6	7.2	6.5	5.7	4.2	4.0	3.8	3.5				1.34
10	9.3	8.5	7.7	6.5	5.8	5.2	3.8	3.6	3.4	3.2				1.66
11	8.5	7.8	7.0	5.9	5.3	4.7								2.00
12	7.8	7.1	6.5	5.4	4.8	4.3								2.38
13	7.2	6.6	6.0											2.80
14	6.7	6.1	5.5											3.24

Loads above horizontal lines will produce maximum allowable shear in webs.
Loads below dotted lines will produce excessive deflections.
For maximum safe loads, see page 140.

Structural Beams

Allowable Uniform Loads in Pounds per Foot

Safe Loads Include Weight of Beam

Depth, Inches	Pounds per Foot	SPAN IN FEET																28	30
		10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25		
24	115	26270	21710	18240	15550	13400	11680	10260	9090	8110	7380	6570	5960	5430	4970	4560	4200	3890	3620
	110	25630	21180	17800	15170	13080	11390	10010	8870	7910	7100	6410	5810	5300	4850	4450	4100	3790	3520
	105	24990	20660	17360	14790	12760	11110	9760	8660	7710	6920	6250	5670	5160	4720	4340	4000	3700	3430
	100	21150	17480	14690	12520	10790	9400	8260	7320	6530	5890	5390	4900	4370	4000	3670	3380	3130	2900
	95	20520	16960	14250	12150	10470	9120	8020	7100	6340	5690	5130	4650	4240	3880	3560	3280	3040	2820
20	85	19900	16440	13820	11770	10150	8840	7770	6880	6140	5510	4970	4510	4110	3760	3450	3180	2940	2730
	80	19270	15830	13380	11400	9830	8560	7530	6670	5950	5340	4820	4370	3980	3640	3350	3080	2850	2640
	75	18550	15330	12880	10980	9470	8250	7250	6420	5730	5140	4640	4210	3830	3510	3220	2970	2750	2550
	70	17660	14560	12260	10450	9010	7850	6900	6110	5450	4890	4420	4000	3650	3340	3070	2830	2610	2420
	65	17140	14160	11900	10140	8740	7620	6680	5930	5290	4750	4280	3890	3540	3240	2980	2740	2540	2350
18	95	16610	13730	11540	9830	8480	7380	6490	5750	5130	4600	4150	3770	3430	3140	2880	2660	2460	2280
	90	16090	13300	11170	9520	8210	7150	6290	5570	4970	4460	4020	3650	3320	3040	2790	2570	2380	2210
	85	15640	12930	10860	9260	7980	6950	6110	5410	4830	4330	3910	3550	3230	2960	2720	2500	2310	2150
	80	15330	11180	9400	8010	6910	6020	5290	4680	4180	3750	3380	3070	2800	2560	2350	2170	2000	1860
	75	15010	10750	9040	7700	6640	5780	5080	4500	4020	3600	3250	2950	2690	2460	2260	2080	1920	1790
15	65	12450	10310	8660	7380	6370	5440	4870	4320	3850	3460	3120	2830	2580	2360	2170	2000	1850	1710
	60	11940	12350	10370	8840	7620	6640	5840	5170	4610	4130	3730	3390	3090	2820	2590	2390	2210	2050
	55	11470	11960	10050	8560	7380	6430	5650	5010	4470	4010	3620	3280	2990	2740	2510	2310	2140	1980
	50	11000	11570	9720	8280	7140	6220	5470	4840	4320	3850	3500	3170	2890	2650	2430	2240	2070	1920
	45	10580	11180	9390	8000	6900	6010	5280	4680	4180	3750	3380	3070	2800	2560	2350	2160	2000	1860

Structural Beams

Allowable Uniform Loads in Pounds per Foot

Continued

Safe Loads Include Weight of Beam

Depth, Inches	Pounds per Foot	SPAN IN FEET																			25	26
		6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24		
15	75	27310	20060	15360	12140	9830	8120	6830	5820	5020	4370	3840	3400	3030	2720	2460	2230	2030	1860	1710	1570	1450
	70	26220	19260	14750	11650	9440	7800	6560	5560	4820	4200	3690	3270	2910	2610	2360	2140	1950	1780	1640	1510	1400
	65	25130	18460	14140	11170	9050	7480	6280	5350	4620	4020	3530	3130	2790	2510	2260	2050	1870	1710	1570	1450	1340
	60	24030	17680	13330	10690	8660	7160	6010	5130	4420	3850	3380	3000	2670	2400	2170	1960	1790	1640	1500	1380	1280
	55	20190	14830	11360	8970	7270	6010	5050	4300	3710	3230	2840	2520	2240	2010	1820	1650	1500	1370	1260	1160	1080
12	50	19100	14030	10740	8490	6880	5680	4780	4070	3510	3060	2690	2380	2120	1910	1720	1560	1420	1300	1190	1100	1020
	45	18010	13230	10130	8000	6480	5360	4500	3840	3310	2880	2530	2240	2000	1800	1620	1470	1340	1230	1130	1040	960
	40	17450	12820	9820	7760	6280	5190	4360	3720	3210	2790	2450	2170	1940	1740	1570	1430	1300	1190	1090	1010	930
	35	15850	11650	8920	7050	5710	4720	3960	3380	2910	2540	2230	1980	1760	1580	1430	1290	1180	1080	990	910	840
	30	14980	11010	8430	6660	5390	4460	3750	3190	2750	2400	2110	1870	1660	1490	1350	1220	1110	1020	940	860	800
10	45	14110	10370	7940	6270	5080	4200	3530	3010	2590	2260	1960	1760	1570	1410	1270	1150	1050	960	880	810	750
	40	13280	9760	7470	5900	4780	3950	3320	2830	2440	2130	1870	1650	1480	1330	1200	1080	990	900	830	770	710
	35	11270	8280	6340	5010	4060	3350	2820	2400	2070	1800	1580	1400	1250	1120	1020	920	840	770	700	650	600
	30	10660	7830	6000	4740	3840	3170	2660	2270	1960	1710	1500	1330	1180	1060	960	870	790	730	670	610	570
	25	9400	6910	5290	4180	3390	2800	2350	2000	1730	1500	1320	1170	1040	940	850	770	700	650	590	540	
9	35	8680	6380	4880	3860	3120	2580	2170	1850	1590	1390	1220	1080	960	870	780	710	650	590			
	30	7950	5840	4470	3530	2860	2370	1990	1690	1460	1270	1120	990	880	790	720	650	590				
	25	7240	5320	4070	3220	2610	2150	1810	1540	1330	1160	1020	900	800	720	650	590					
	35	7360	5410	4140	3270	2650	2190	1840	1570	1350	1180	1040	920	820	730	660						
	30	6710	4930	3770	2980	2420	2000	1680	1430	1230	1070	940	840	750	670	600						
21	25	6050	4450	3410	2690	2180	1800	1510	1290	1110	970	850	750	670	600	540						
	21	5590	4110	3150	2490	2010	1660	1400	1190	1030	900	790	700	620	560	500						

Loads below dotted lines will
produce excessive deflection.

Structural Beams
Allowable Uniform Loads in Pounds per Foot
Continued
Safe Loads Include Weight of Beam

Depth, Inches		Pounds per Foot	SPAN IN FEET																						
			2	2½	3	3½	4	4½	5	5½	6	6½	7	8	9	10	11	12	13	14	15	16	17	18	
8	25.5	43250	29200	20280	14900	11410	9010	7300	6030	5070	4320	3720	2850	2250	1830	1510	1270	1080	930	810	710	630	560		
	23.	35920	27520	19110	14040	10750	8490	6880	5690	4780	4070	3510	2690	2120	1720	1420	1190	1020	880	760	670	600	530		
	20.5	28560	22340	17950	13190	10100	7980	6460	5340	4490	3820	3300	2520	1990	1620	1340	1120	960	820	720	630	560	500		
	18.	21600	17280	14400	12340	9480	7490	6070	5010	4210	3590	3100	2370	1870	1520	1250	1050	900	770	670	590	530	470		
7	20.	32060	20570	14280	10490	8040	6350	5140	4250	3570	3040	2620	2010	1590	1290	1060	890	760	660	570	500				
	17.5	24710	19100	13270	9750	7460	5900	4780	3950	3320	2830	2440	1870	1470	1190	990	830	710	610	530	470				
	15.	17500	14000	11700	9010	6900	5450	4420	3650	3070	2610	2250	1730	1360	1100	910	770	650	560	490	430				
6	17.25	23280	14900	10350	7600	5820	4600	3720	3080	2590	2200	1900	1450	1150	930	770	650	550	480						
	14.75	21120	13650	9470	6960	5330	4210	3410	2820	2370	2020	1740	1330	1050	850	700	590	500	440						
	12.25	13800	11040	8610	6320	4840	3830	3100	2560	2150	1830	1580	1210	960	780	640	540	460	400						
5	14.75	16160	10340	7180	5280	4040	3190	2590	2140	1800	1530	1320	1010	800	650	530	450								
	12.25	14530	9300	6460	4740	3630	2870	2320	1920	1610	1380	1190	910	720	580	480	400								
	9.75	10500	8250	5790	4210	3220	2550	2060	1710	1430	1220	1050	810	640	520	430	360								
4	10.5	9520	6090	4230	3110	2380	1880	1520	1260	1060	900	780	590	470	380										
	9.5	9000	5760	4000	2940	2250	1790	1440	1190	1000	850	730	560	440	360										
	8.5	8470	5420	3770	2770	2120	1670	1360	1120	940	800	690	530	420	340										
3	7.5	7600	5090	3530	2600	1990	1570	1270	1050	880	750	650	500	390	320										
	7.5	5180	3310	2300	1690	1290	1020	830	680	580	490	420													
	6.5	4780	3060	2130	1560	1200	940	770	630	530	450	390													
5.5	4410	2820	1960	1440	1100	870	710	580	490	420	360														

Loads within heavy lines will produce excessive shear in webs.
 Loads below dotted lines will produce excessive deflections.

Structural Channels

Allowable Uniform Loads in Thousands of Pounds

Extreme Fiber Stress, 16,000 Pounds per Square Inch

Safe Loads Include Weight of Channel

Span in Feet	DEPTH AND WEIGHT OF SECTIONS						Coefficient of Deflection
	15 Inch						
	55 lbs.	50 lbs.	45 lbs.	40 lbs.	35 lbs.	33 lbs.	
	245.4	216.0	186.6				
3	204.0	190.9	177.8	157.2	127.8	120.0	0.15
4	153.0	143.2	133.4	123.6	113.8	111.1	0.27
5	122.4	114.5	106.7	98.9	91.0	88.9	0.41
6	102.0	95.4	88.9	82.4	75.8	74.1	0.60
7	87.4	81.8	76.2	70.6	65.0	63.5	0.81
8	76.5	71.6	66.7	61.8	56.9	55.6	1.06
9	68.0	63.6	59.3	54.9	50.6	49.4	1.34
10	61.2	57.3	53.3	49.4	45.5	44.5	1.66
11	55.6	52.1	48.5	44.9	41.4	40.4	2.00
12	51.0	47.7	44.5	41.2	37.9	37.0	2.38
13	47.1	44.1	41.0	38.0	35.0	34.2	2.80
14	43.7	40.9	38.1	35.3	32.5	31.8	3.24
15	40.8	38.2	35.6	33.0	30.3	29.6	3.72
16	38.2	35.8	33.3	30.9	28.4	27.8	4.24
17	36.0	33.7	31.4	29.1	26.8	26.1	4.78
18	34.0	31.8	29.6	27.5	25.3	24.7	5.36
19	32.2	30.1	28.1	26.0	23.9	23.4	5.98
20	30.6	28.6	26.7	24.7	22.8	22.3	6.62
21	29.1	27.3	25.4	23.5	21.7	21.2	7.30
22	27.8	26.0	24.3	22.5	20.7	20.2	8.01
23	26.6	24.9	23.2	21.5	19.8	19.3	8.76
24	25.5	23.9	22.2	20.6	19.0	18.5	9.53
25	24.5	22.9	21.3	19.8	18.2	17.8	10.35
26	23.5	22.0	20.5	19.0	17.5	17.1	11.19
27	22.7	21.2	19.8	18.3	16.9	16.5	12.07
28	21.9	20.5	19.1	17.7	16.3	15.9	12.98
29	21.1	19.7	18.4	17.0	15.7	15.3	13.92
30	20.4	19.1	17.8	16.5	15.2	14.8	14.90
31	19.7	18.5	17.2	15.9	14.7	14.3	15.91
32	19.1	17.9	16.7	15.4	14.2	13.9	16.95

Loads above horizontal lines will produce maximum allowable shear in webs.

Loads below dotted lines will produce excessive deflections.

Structural Channels

Allowable Uniform Loads in Thousands of Pounds

Continued

Extreme Fiber Stress, 16,000 Pounds per Square Inch
Safe Loads Include Weight of Channel

Span in Feet	DEPTH AND WEIGHT OF SECTIONS										Co- efficient of Deflec- tion
	12 Inch					10 Inch					
	40 lbs.	35 lbs.	30 lbs.	25 lbs.	20½ lbs.	35 lbs.	30 lbs.	25 lbs.	20 lbs.	15 lbs.	
	181.9					164.6	135.2	105.8			
2	175.1	152.6	123.1	93.6		123.2	110.1	97.0	76.4	48.0	0.07
3	116.7	106.2	95.8	85.3	67.2	82.1	73.4	64.7	56.0	47.6	0.15
4	87.5	79.7	71.8	64.0	56.9	61.6	55.1	48.5	42.0	35.7	0.27
5	70.0	63.7	57.5	51.2	45.5	49.3	44.0	38.8	33.6	28.5	0.41
6	58.4	53.1	47.9	42.7	38.0	41.1	36.7	32.3	28.0	23.8	0.60
7	50.0	45.5	41.1	36.6	32.5	35.2	31.5	27.7	24.0	20.4	0.81
8	43.8	39.8	35.9	32.0	28.5	30.8	27.5	24.3	21.0	17.8	1.06
9	38.9	35.4	31.9	28.4	25.3	27.4	24.5	21.6	18.7	15.9	1.34
10	35.0	31.9	28.7	25.6	22.8	24.6	22.0	19.4	16.8	14.3	1.66
11	31.8	29.0	26.1	23.3	20.7	22.4	20.0	17.6	15.3	13.0	2.00
12	29.2	26.6	23.9	21.3	19.0	20.5	18.4	16.2	14.0	11.9	2.38
13	26.9	24.5	22.1	19.7	17.5	19.0	16.9	14.9	12.9	11.0	2.80
14	25.0	22.8	20.5	18.3	16.3	17.6	15.7	13.9	12.0	10.2	3.24
15	23.3	21.2	19.2	17.1	15.2	16.4	14.7	12.9	11.2	9.5	3.72
16	21.9	19.9	18.0	16.0	14.2	15.4	13.8	12.1	10.5	8.9	4.24
17	20.6	18.7	16.9	15.1	13.4	14.5	13.0	11.4	9.9	8.4	4.78
18	19.5	17.7	16.0	14.2	12.7	13.7	12.2	10.8	9.3	7.9	5.36
19	18.4	16.8	15.1	13.5	12.0	13.0	11.6	10.2	8.8	7.5	5.98
20	17.5	15.9	14.4	12.8	11.4	12.3	11.0	9.7	8.4	7.1	6.62
21	16.7	15.2	13.7	12.2	10.8	11.7	10.5	9.2	8.0	6.8	7.30
22	15.9	14.5	13.1	11.6	10.4	11.2	10.0	8.8	7.6	6.5	8.01
23	15.2	13.9	12.5	11.1	9.9						8.76
24	14.6	13.3	12.0	10.7	9.5						9.53
25	14.0	12.8	11.5	10.2	9.1						10.35
26	13.5	12.3	11.1	9.8	8.8						11.19

Loads above horizontal lines will produce maximum allowable shear in webs.

Loads below dotted lines will produce excessive deflections.

Structural Channels

Allowable Uniform Loads in Thousands of Pounds

Continued

Extreme Fiber Stress, 16,000 Pounds per Square Inch
Safe Loads Include Weight of Channel

Span in Feet	DEPTH AND WEIGHT OF SECTIONS														Coeffi- cient of Deflec- tion
	9 Inch				8 Inch					7 Inch					
	25 lbs.	20 lbs.	15 lbs.	13½ lbs.	21½ lbs.	18¾ lbs.	16¼ lbs.	13¾ lbs.	11¼ lbs.	19¾ lbs.	17¼ lbs.	14¾ lbs.	12¼ lbs.	9¾ lbs.	
	110.7	81.4			93.1	78.4	63.8	49.1		88.6	73.9	59.2	44.5		
2	83.8	72.0	51.8	41.4	63.7	58.5	53.2	48.0	35.2	50.6	46.0	41.4	36.8	29.4	0.07
3	55.9	48.0	40.2	37.4	42.5	39.0	35.5	32.0	28.7	33.7	30.7	27.6	24.6	21.4	0.15
4	41.9	36.0	30.1	28.0	31.8	29.2	26.6	24.0	21.5	25.3	23.0	20.7	18.4	16.1	0.27
5	33.5	28.8	24.1	22.4	25.5	23.4	21.3	19.2	17.2	20.2	18.4	16.6	14.7	12.9	0.41
6	27.9	24.0	20.1	18.7	21.2	19.5	17.7	16.0	14.4	16.9	15.3	13.8	12.3	10.7	0.60
7	23.9	20.6	17.2	16.0	18.2	16.7	15.2	13.7	12.3	14.4	13.1	11.8	10.5	9.2	0.81
8	20.9	18.0	15.1	14.0	15.9	14.6	13.3	12.0	10.8	12.6	11.5	10.4	9.2	8.0	1.06
9	18.6	16.0	13.4	12.5	14.2	13.0	11.8	10.7	9.6	11.2	10.2	9.2	8.2	7.1	1.34
10	16.8	14.4	12.1	11.2	12.7	11.7	10.6	9.6	8.6	10.1	9.2	8.3	7.4	6.4	1.66
11	15.2	13.1	11.0	10.2	11.6	10.6	9.7	8.7	7.8	9.2	8.4	7.5	6.7	5.8	2.00
12	14.0	12.0	10.1	9.3	10.6	9.7	8.9	8.0	7.2	8.4	7.7	6.9	6.1	5.4	2.38
13	12.9	11.1	9.3	8.6	9.8	9.0	8.2	7.4	6.6	7.8	7.1	6.4	5.7	4.9	2.80
14	12.0	10.3	8.6	8.0	9.1	8.4	7.6	6.9	6.2	7.2	6.6	5.9	5.3	4.6	3.24
15	11.2	9.6	8.0	7.5	8.5	7.8	7.1	6.4	5.7	6.7	6.1	5.5	4.9	4.3	3.72
16	10.5	9.0	7.5	7.0	8.0	7.3	6.7	6.0	5.4	6.3	5.7	5.2	4.6	4.0	4.24
17	9.9	8.5	7.1	6.6	7.5	6.9	6.3	5.6	5.1						4.78
18	9.3	8.0	6.7	6.2	7.1	6.5	5.9	5.3	4.8						5.36
19	8.8	7.6	6.3	5.9											5.98
20	8.4	7.2	6.0	5.6											6.62

Span in Feet	DEPTH AND WEIGHT OF SECTIONS												Coeffi- cient of Deflec- tion	
	6 Inch				5 Inch			4 Inch			3 Inch			
	15½ lbs.	13 lbs.	10½ lbs.	8 lbs.	11½ lbs.	9 lbs.	6½ lbs.	7¼ lbs.	6¼ lbs.	5¼ lbs.	6 lbs.	5 lbs.	4 lbs.	
1	67.6	52.8	38.2	24.0	47.7	44.4	33.0	19.0	24.4	20.2	14.4	21.7	15.8	0.02
2	34.7	30.8	26.9	23.1	22.2	18.9	15.8	12.2	11.1	10.1	7.4	6.6	5.8	0.07
3	23.2	20.5	17.9	15.4	14.8	12.6	10.5	8.1	7.4	6.7	4.9	4.4	3.9	0.15
4	17.4	15.4	13.4	11.6	11.1	9.5	7.9	6.1	5.6	5.1	3.7	3.3	2.9	0.27
5	13.9	12.3	10.8	9.2	8.9	7.6	6.3	4.9	4.5	4.1	2.9	2.6	2.3	0.41
6	11.6	10.3	9.0	7.7	7.4	6.3	5.3	4.1	3.7	3.4	2.5	2.2	1.9	0.60
7	9.9	8.8	7.7	6.6	6.3	5.4	4.5	3.5	3.2	2.9	2.1	1.9	1.7	0.81
8	8.7	7.7	6.7	5.8	5.5	4.7	4.0	3.0	2.8	2.5	1.8	1.6	1.5	1.06
9	7.7	6.8	6.0	5.1	4.9	4.2	3.5	2.7	2.5	2.2				1.34
10	6.9	6.2	5.4	4.6	4.4	3.8	3.2	2.4	2.2	2.0				1.66
11	6.3	5.6	4.9	4.2	4.0	3.4	2.9							2.00
12	5.8	5.1	4.5	3.9	3.7	3.2	2.6							2.38
13	5.3	4.7	4.1	3.6										2.80
14	5.0	4.4	3.8	3.3										3.24

Loads above horizontal lines will produce maximum allowable shear in webs.
 Loads below dotted lines will produce excessive deflections.

Structural Channels

Allowable Uniform Loads in Pounds per Foot

Safe Loads Include Weight of Channel

Depth, Inches	Pounds per Foot	SPAN IN FEET																			Loads below dotted lines will produce excessive deflections.		
		6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24			
15	55	17000	12490	9560	7550	6120	5060	4250	3620	3120	2720	2390	2120	1890	1690	1530	1390	1260	1160	1060	980	910	
	50	15910	11690	8950	7070	5730	4730	3980	3390	2920	2550	2240	1980	1770	1590	1430	1300	1180	1080	990	920	850	
	45	14820	10890	8340	6590	5330	4410	3700	3160	2720	2370	2080	1850	1650	1480	1330	1210	1100	1010	930	850	790	
	40	13730	10090	7720	6100	4940	4080	3430	2920	2520	2200	1930	1710	1530	1370	1240	1120	1020	930	860	790	730	
	35	12640	9290	7110	5620	4550	3760	3160	2690	2320	2020	1780	1570	1400	1260	1140	1030	940	860	790	730	670	
12	33	12350	9070	6950	5490	4450	3670	3090	2630	2270	1980	1740	1540	1370	1230	1110	1010	920	840	770	710	660	
	40	9730	7150	5470	4320	3500	2890	2430	2070	1790	1560	1370	1210	1080	970	880	790	720	660	610	560	520	
	35	8850	6500	4980	3940	3190	2630	2210	1890	1630	1420	1250	1100	980	880	800	720	660	600	550	510	470	
	30	7980	5860	4490	3550	2870	2380	2000	1700	1470	1280	1120	1000	890	800	720	650	590	540	500	460	430	
	25	7110	5220	4000	3160	2560	2120	1780	1520	1310	1140	1000	890	790	710	640	580	530	480	440	410	380	
10	20.5	6330	4650	3560	2810	2280	1890	1580	1350	1160	1010	890	780	700	630	570	520	470	430	400	360	340	
	35	6840	5030	3850	3040	2460	2040	1710	1460	1260	1100	960	850	760	680	620	560	510					
	30	6120	4490	3440	2730	2200	1820	1530	1300	1120	980	860	760	680	610	550	500	460					
	25	5390	3960	3030	2400	1940	1600	1350	1150	990	860	760	670	600	540	490	440	400					
	20	4670	3430	2620	2070	1680	1390	1170	990	860	750	660	580	520	470	420	380	350					
9	15	3960	2910	2230	1760	1430	1180	990	840	730	630	560	490	440	400	360	320	290					
	25	4660	3420	2620	2070	1680	1390	1160	990	860	750	650	580	520	460	420			Loads below dotted lines will produce excessive deflections.				
	20	4000	2940	2250	1780	1440	1190	1000	850	740	640	560	500	450	400	360							
	15	3350	2460	1880	1490	1210	1000	840	710	620	540	470	420	370	330	300							
	13.25	3120	2290	1750	1380	1120	930	780	660	570	500	440	390	350	310	280							

Structural Channels
Allowable Uniform Loads in Pounds per Foot
Continued
Safe Loads Include Weight of Channel

Depth, Inches.	Pounds per Foot	SPAN IN FEET																18					
		2	2½	3	3½	4	4½	5	5½	6	6½	7	8	9	10	11	12		13	14	15	16	17
8	21.25	31840	20380	14150	10400	7960	6290	5090	4210	3540	3010	2600	1990	1570	1270	1050	880	750	650	570	500	440	390
	18.75	29230	18710	12990	9540	7310	5770	4680	3860	3250	2720	2390	1830	1440	1170	970	810	690	600	520	460	410	360
	16.25	26610	17030	11830	8690	6650	5260	4260	3530	2960	2520	2170	1660	1310	1060	880	740	630	540	470	420	370	330
	13.75	24000	15360	10670	7840	6000	4740	3840	3170	2670	2270	1960	1500	1190	960	790	670	570	490	430	370	330	300
	11.25	17600	13780	9570	7030	5380	4250	3450	2850	2390	2040	1760	1350	1060	860	710	600	510	440	380	340	300	270
7	19.75	25280	16180	11230	8250	6320	4990	4040	3340	2810	2390	2080	1580	1250	1010	840	700	600	520	450	400		
	17.25	22900	14710	10230	7510	5750	4540	3680	3040	2550	2180	1880	1440	1140	920	760	640	540	470	410	360		
	14.75	20700	13250	9200	6760	5180	4090	3310	2740	2300	1940	1690	1290	1020	830	680	580	490	420	370	320		
	12.25	18410	11780	8180	6010	4600	3640	2950	2430	2050	1740	1500	1150	910	740	610	510	440	380	330	290		
	9.75	14700	10280	7140	5250	4020	3170	2570	2120	1790	1520	1310	1000	790	640	530	450	380	330	290	250		
6	15.5	17360	11110	7720	5670	4340	3430	2780	2300	1930	1640	1420	1090	860	690	570	480	410	350				
	13.0	15400	9860	6840	5030	3850	3040	2460	2040	1710	1460	1260	960	760	620	510	430	360	310				
	10.5	13440	8600	5970	4390	3360	2650	2150	1780	1490	1270	1100	840	660	540	440	370	320	270				
	8.0	11550	7390	5180	3770	2890	2280	1850	1530	1280	1090	940	720	570	460	380	320	270	240				
5	11.5	11100	7100	4930	3620	2770	2190	1780	1470	1230	1050	910	690	550	440	370	310						
	9.0	9460	6060	4210	3090	2370	1870	1510	1250	1050	900	770	590	470	380	310	260						
	6.5	7910	5060	3520	2580	1980	1560	1270	1050	880	750	650	490	390	320	260	220						
4	7.25	6090	3900	2710	1990	1530	1200	980	810	680	580	500	380	300	240								
	6.25	5570	3570	2480	1820	1390	1100	890	740	620	530	460	350	280	220								
	5.25	5060	3240	2250	1650	1260	1000	810	670	560	480	410	320	250	200								
3	6.0	3680	2350	1630	1200	920	730	590	490	410	350	300											
	5.0	3290	2100	1460	1070	820	650	530	430	370	310	270											
	4.0	2910	1860	1290	950	730	570	470	380	320	280	240											

Loads within heavy lines will produce excessive shear in web.
Loads below dotted lines will produce excessive deflections.

Loads within heavy lines will produce excessive shear in web.
Loads below dotted lines will produce excessive deflections.

Angles with Equal Legs

Allowable Uniform Loads in Thousands of Pounds

Extreme Fiber Stress, 16,000 Pounds per Square Inch

Safe Loads Include Weight of Angle

Neutral Axis Through Center of

Gravity Parallel to One Leg

Size of Angle, Inches	SPAN IN FEET									
	1	2	3	4	5	6	7	8	9	10
8 x 8 x $\frac{1}{8}$	186.98	93.48	62.32	46.74	37.40	31.16	26.72	23.38	20.78	18.70
8 x 8 x $\frac{1}{2}$	89.28	44.64	29.76	22.32	17.86	14.88	12.76	11.16	9.92	8.92
6 x 6 x 1	91.41	45.71	30.47	22.85	18.28	15.26	13.06	11.43	10.16	9.14
6 x 6 x $\frac{3}{8}$	37.65	18.83	12.55	9.41	7.53	6.28	5.38	4.71	4.18	3.77
5 x 5 x $\frac{1}{8}$	58.56	29.28	19.52	14.64	11.71	9.76	8.36	7.32	6.51	5.86
5 x 5 x $\frac{3}{8}$	25.81	12.90	8.60	6.45	5.16	4.30	3.69	3.23	2.87	2.58
4 x 4 x $\frac{1}{8}$	32.12	16.06	10.71	8.03	6.42	5.35	4.50	4.02	3.57	3.21
4 x 4 x $\frac{1}{4}$	11.20	5.60	3.73	2.80	2.24	1.87	1.60	1.40	1.24	1.12
3½ x 3½ x $\frac{3}{4}$	22.51	11.26	7.50	5.63	4.50	3.75	3.22	2.81	2.50	2.25
3½ x 3½ x $\frac{1}{4}$	8.43	4.22	2.81	2.11	1.68	1.41	1.20	1.05	0.94	0.84
3 x 3 x $\frac{3}{8}$	13.87	6.94	4.62	3.47	2.77	2.31	1.98	1.73	1.54	1.39
3 x 3 x $\frac{1}{4}$	6.18	3.09	2.06	1.54	1.24	1.03	0.88	0.77	0.69	0.62
2½ x 2½ x $\frac{1}{2}$	7.78	3.88	2.60	1.94	1.56	1.30	1.12	0.98	0.86	0.78
2½ x 2½ x $\frac{3}{8}$	2.13	1.07	0.71	0.53	0.43	0.36	0.30	0.27	0.24	0.21
2 x 2 x $\frac{1}{2}$	4.80	2.40	1.60	1.20	0.96	0.80	0.69	0.60	0.53	0.48
2 x 2 x $\frac{3}{8}$	1.60	0.80	0.54	0.40	0.32	0.26	0.22	0.20	0.18	0.16
1½ x 1½ x $\frac{3}{8}$	2.06	1.04	0.68	0.52	0.42	0.34	0.30	0.26	0.22	0.20
1½ x 1½ x $\frac{1}{8}$	0.82	0.42	0.28	0.20	0.16	0.14	0.12	0.10	0.10	0.08
1 x 1 x $\frac{1}{4}$	0.60	0.30	0.20	0.15	0.12	0.10	0.086	0.075	0.067	0.06
1 x 1 x $\frac{3}{8}$	0.34	0.17	0.114	0.084	0.068	0.056	0.048	0.042	0.038	0.034

For safe loads to the right of heavy line the deflection will be greater than allowable for plastered ceiling.

Angles with Unequal Legs

Long Leg Vertical

Allowable Uniform Loads in Thousands of Pounds

Extreme Fiber Stress 16,000 Pounds per Square Inch

Safe Loads Include Weight of Angle

Neutral Axis Through Center of

Gravity Parallel to Short Leg

Size of Angle, Inches	SPAN IN FEET									
	1	2	3	4	5	6	7	8	9	10
8 x 6 x $1\frac{1}{8}$	179.32	89.66	59.77	44.83	35.86	29.89	25.62	22.42	19.92	17.93
8 x 6 x $\frac{1}{2}$	85.55	42.77	28.52	21.39	17.11	14.26	12.22	10.69	9.50	8.56
7 x $3\frac{1}{2}$ x $\frac{7}{8}$	100.48	50.24	33.49	25.12	20.10	16.75	14.35	12.56	11.16	10.05
7 x $3\frac{1}{2}$ x $\frac{1}{4}$	53.44	26.72	17.81	13.36	10.68	8.91	7.63	6.68	5.94	5.34
6 x 4 x $\frac{1}{2}$	71.52	35.76	23.84	17.88	14.30	11.92	10.22	8.94	7.95	7.15
6 x 4 x $\frac{3}{8}$	35.42	17.70	11.82	8.86	7.10	5.90	5.06	4.42	3.92	3.54
6 x $3\frac{1}{2}$ x $\frac{3}{4}$	65.17	32.59	21.72	16.29	13.03	10.86	9.31	8.15	7.24	6.52
6 x $3\frac{1}{2}$ x $\frac{3}{8}$	34.66	17.34	11.54	8.66	6.94	5.78	4.96	4.34	3.84	3.46
5 x 4 x $\frac{1}{2}$	49.93	24.96	16.64	12.48	9.99	8.32	7.13	6.24	5.54	4.99
5 x 4 x $\frac{3}{8}$	25.06	12.53	8.35	6.26	5.01	4.18	3.58	3.13	2.78	2.51
5 x $3\frac{1}{2}$ x $\frac{3}{4}$	45.69	22.84	15.23	11.42	9.14	7.61	6.53	5.71	5.08	4.57
5 x $3\frac{1}{2}$ x $\frac{1}{4}$	20.69	10.35	6.89	5.17	4.14	3.45	2.96	2.59	2.30	2.07
5 x 3 x $\frac{1}{2}$	41.19	20.60	13.73	10.30	8.24	6.87	5.88	5.15	4.58	4.12
5 x 3 x $\frac{1}{4}$	20.16	10.08	6.72	5.04	4.03	3.36	2.88	2.52	2.24	2.02
$4\frac{1}{2}$ x 3 x $\frac{1}{2}$	33.47	16.74	11.16	8.37	6.69	5.58	4.78	4.18	3.72	3.35
$4\frac{1}{2}$ x 3 x $\frac{1}{4}$	16.42	8.22	5.48	4.10	3.28	2.74	2.34	2.06	1.82	1.64
4 x $3\frac{1}{2}$ x $\frac{1}{2}$	29.12	14.56	9.70	7.28	5.82	4.86	4.16	3.66	3.22	2.90
4 x $3\frac{1}{2}$ x $\frac{1}{4}$	13.44	6.72	4.48	3.36	2.69	2.24	1.92	1.68	1.49	1.34
4 x 3 x $\frac{1}{2}$	26.52	13.26	8.84	6.63	5.30	4.42	3.79	3.32	2.95	2.65
4 x 3 x $\frac{1}{4}$	10.67	5.33	3.56	2.67	2.14	1.78	1.52	1.33	1.19	1.07
$3\frac{1}{2}$ x 3 x $\frac{1}{2}$	20.37	10.19	6.79	5.09	4.07	3.40	2.91	2.55	2.26	2.04
$3\frac{1}{2}$ x 3 x $\frac{1}{4}$	8.32	4.16	2.77	2.08	1.66	1.39	1.19	1.04	0.92	0.83
$3\frac{1}{2}$ x $2\frac{1}{2}$ x $\frac{3}{8}$	16.68	8.34	5.56	4.17	3.34	2.78	2.38	2.09	1.85	1.67
$3\frac{1}{2}$ x $2\frac{1}{2}$ x $\frac{1}{4}$	8.00	4.00	2.67	2.00	1.60	1.33	1.14	1.00	0.89	0.80
3 x $2\frac{1}{2}$ x $\frac{3}{8}$	12.28	6.14	4.09	3.07	2.46	2.05	1.75	1.54	1.36	1.23
3 x $2\frac{1}{2}$ x $\frac{1}{4}$	5.98	2.98	2.00	1.50	1.20	1.00	0.86	0.76	0.66	0.58
3 x 2 x $\frac{1}{2}$	10.66	5.32	3.54	2.66	2.14	1.78	1.52	1.34	1.18	1.06
3 x 2 x $\frac{1}{4}$	3.50	1.74	1.16	0.88	0.70	0.58	0.50	0.44	0.38	0.34
$2\frac{1}{2}$ x 2 x $\frac{1}{2}$	7.58	3.78	2.52	1.90	1.52	1.26	1.08	0.94	0.84	0.76
$2\frac{1}{2}$ x 2 x $\frac{1}{4}$	3.10	1.54	1.04	0.78	0.62	0.50	0.44	0.38	0.34	0.32

For safe loads to the right of heavy line the deflection will be greater than allowable for plastered ceilings.

Angles With Unequal Legs

Short Leg Vertical

Allowable Uniform Loads in Thousands of Pounds

Extreme Fiber Stress, 16,000 Pounds per Square Inch

Safe Loads Include Weight of Angle

Neutral Axis Through Center of Gravity Parallel to Long Leg

Size of Angle, Inches	SPAN IN FEET									
	1	2	3	4	5	6	7	8	9	10
8 x 6 x $1\frac{1}{8}$	105.61	52.80	35.20	26.40	21.12	17.60	15.09	13.20	11.73	10.56
8 x 6 x $\frac{1}{2}$	51.09	25.55	17.03	12.77	10.22	8.51	7.30	6.38	5.68	5.11
7 x $3\frac{1}{2}$ x $\frac{7}{8}$	28.16	14.08	9.39	7.04	5.63	4.69	4.02	3.52	3.13	2.82
7 x $3\frac{1}{2}$ x $\frac{1}{4}$	15.36	7.68	5.12	3.84	3.07	2.56	2.19	1.92	1.71	1.54
6 x 4 x $\frac{1}{4}$	33.95	16.97	11.32	8.49	6.79	5.66	4.85	4.24	3.77	3.39
6 x 4 x $\frac{1}{2}$	17.06	8.54	5.68	4.26	3.42	2.86	2.44	2.14	1.90	1.70
6 x $3\frac{1}{2}$ x $\frac{3}{4}$	24.24	12.12	8.08	6.06	4.85	4.04	3.46	3.03	2.69	2.42
6 x $3\frac{1}{2}$ x $\frac{1}{2}$	13.12	6.56	4.38	3.28	2.62	2.18	1.88	1.64	1.46	1.32
5 x 4 x $\frac{1}{4}$	33.06	16.53	11.02	8.26	6.61	5.51	4.72	4.13	3.67	3.31
5 x 4 x $\frac{1}{2}$	16.74	8.38	5.58	4.18	3.36	2.80	2.40	2.10	1.86	1.68
5 x $3\frac{1}{2}$ x $\frac{3}{4}$	23.68	11.84	7.89	5.92	4.74	3.95	3.38	2.96	2.63	2.37
5 x $3\frac{1}{2}$ x $\frac{1}{4}$	10.88	5.44	3.63	2.72	2.18	1.81	1.55	1.36	1.21	1.09
5 x 3 x $\frac{1}{4}$	16.10	8.05	5.37	4.02	3.22	2.68	2.30	2.01	1.79	1.61
5 x 3 x $\frac{1}{2}$	8.00	4.00	2.67	2.00	1.60	1.33	1.14	1.00	0.89	0.80
$4\frac{1}{2}$ x 3 x $\frac{1}{4}$	15.83	7.91	5.28	3.96	3.17	2.64	2.26	1.98	1.76	1.58
$4\frac{1}{2}$ x 3 x $\frac{1}{2}$	8.10	4.06	2.70	2.02	1.62	1.36	1.16	1.02	0.90	0.82
4 x $3\frac{1}{2}$ x $\frac{1}{4}$	22.72	11.36	7.58	5.68	4.54	3.78	3.24	2.82	2.54	2.28
4 x $3\frac{1}{2}$ x $\frac{1}{2}$	10.67	5.33	3.56	2.67	2.13	1.78	1.52	1.33	1.12	1.06
4 x 3 x $\frac{1}{4}$	15.57	7.79	5.19	3.89	3.11	2.58	2.22	1.95	1.73	1.56
4 x 3 x $\frac{1}{2}$	6.40	3.20	2.13	1.60	1.28	1.07	0.91	0.80	0.71	0.64
$3\frac{1}{2}$ x 3 x $\frac{1}{4}$	15.36	7.68	5.12	3.84	3.07	2.56	2.19	1.92	1.70	1.53
$3\frac{1}{2}$ x 3 x $\frac{1}{2}$	6.19	3.10	2.06	1.54	1.24	1.03	0.88	0.77	0.69	0.62
$3\frac{1}{2}$ x $2\frac{1}{2}$ x $\frac{3}{8}$	8.98	4.49	2.99	2.25	1.80	1.50	1.28	1.12	1.00	0.90
$3\frac{1}{2}$ x $2\frac{1}{2}$ x $\frac{1}{4}$	4.38	2.18	1.46	1.10	0.88	0.72	0.62	0.56	0.48	0.44
3 x $2\frac{1}{2}$ x $\frac{3}{8}$	8.76	4.38	2.92	2.19	1.75	1.46	1.25	1.09	0.97	0.88
3 x $2\frac{1}{2}$ x $\frac{1}{4}$	4.26	2.14	1.42	1.06	0.86	0.72	0.64	0.54	0.48	0.42
3 x 2 x $\frac{1}{2}$	5.02	2.50	1.68	1.26	1.00	0.84	0.72	0.64	0.56	0.50
3 x 2 x $\frac{3}{8}$	2.14	1.06	0.72	0.54	0.42	0.36	0.30	0.26	0.24	0.22
$2\frac{1}{2}$ x 2 x $\frac{1}{2}$	4.98	2.50	1.66	1.24	1.00	0.82	0.72	0.62	0.56	0.50
$2\frac{1}{2}$ x 2 x $\frac{3}{8}$	2.02	1.02	0.66	0.50	0.40	0.34	0.30	0.26	0.22	0.20

For safe loads to the right of heavy line the deflection will be greater than allowable for plastered ceilings.

Tees With Equal Legs

Allowable Uniform Loads in Thousands of Pounds

Extreme Fiber Stress, 16,000 Pounds per Square Inch

Safe Loads Include Weight of Tee

Section Index	Size Flange by Stem, Inches	SPAN IN FEET									
		1	2	3	4	5	6	7	8	9	10
T-3	4 x 4	23.34	11.66	7.78	5.84	4.66	3.90	3.34	2.90	2.58	2.34
T-4	4 x 4	20.56	10.30	6.86	5.14	4.10	3.44	2.94	2.56	2.30	2.06
T-9	3½ x 3½	14.74	7.38	4.90	3.68	2.96	2.46	2.10	1.84	1.62	1.48
T-10	3½ x 3½	12.78	6.38	4.26	3.20	2.56	2.14	1.84	1.60	1.42	1.28
T-15	3 x 3	9.54	4.78	3.18	2.40	1.92	1.60	1.36	1.20	1.06	0.96
T-16	3 x 3	8.22	4.10	2.74	2.06	1.66	1.36	1.18	1.02	0.90	0.82
T-17	3 x 3	6.60	3.30	2.20	1.64	1.32	1.10	0.94	0.82	0.74	0.66
T-22	2½ x 2½	6.50	3.26	2.16	1.62	1.30	1.10	0.94	0.80	0.72	0.64
T-23	2½ x 2½	5.58	2.78	1.86	1.38	1.12	0.94	0.80	0.70	0.62	0.56
T-28	2¼ x 2¼	4.26	2.14	1.42	1.06	0.86	0.72	0.62	0.54	0.48	0.42
T-29	2¼ x 2¼	3.50	1.74	1.18	0.88	0.70	0.58	0.50	0.42	0.40	0.34
T-33	2 x 2	3.16	1.58	1.05	0.79	0.63	0.52	0.45	0.40	0.35	0.32
T-34	2 x 2	2.72	1.36	0.90	0.68	0.54	0.46	0.40	0.34	0.30	0.28
T-39	1½ x 1½	2.06	1.02	0.70	0.52	0.40	0.34	0.30	0.26	0.24	0.20
T-40	1½ x 1½	1.36	0.68	0.46	0.34	0.26	0.24	0.18	0.16	0.16	0.14
T-45	1½ x 1½	1.46	0.74	0.48	0.38	0.30	0.24	0.22	0.18	0.16	0.14
T-46	1½ x 1½	1.22	0.62	0.40	0.30	0.24	0.22	0.18	0.16	0.14	0.12
T-51	1¼ x 1¼	1.04	0.52	0.34	0.26	0.22	0.18	0.16	0.14	0.12	0.10
T-52	1¼ x 1¼	0.78	0.40	0.26	0.20	0.16	0.14	0.10	0.10	0.08	0.08
T-57	1 x 1	0.50	0.26	0.16	0.14	0.10	0.08	0.08	0.06	0.06	0.06
T-58	1 x 1	0.38	0.18	0.12	0.10	0.08	0.06	0.06	0.06	0.04	0.04

For safe loads to the right of heavy line the deflection will be greater than allowable for plastered ceilings.

Tees With Unequal Legs

Allowable Uniform Loads in Thousands of Pounds

Extreme Fiber Stress, 16,000 Pounds per Square Inch

Safe Loads Include Weight of Tee

Section Index	Size Flange by Stem, Inches	SPAN IN FEET									
		1	2	3	4	5	6	7	8	9	10
*T-69	5 x 2½	9.18	4.58	3.06	2.30	1.84	1.52	1.32	1.14	1.02	0.92
*T-74	4½ x 3	8.64	4.32	2.88	2.16	1.72	1.44	1.24	1.08	0.96	0.86
T-79	4 x 2	4.27	2.14	1.42	1.07	0.86	0.71	0.61	0.53	0.47	0.43
T-80	4 x 2	3.63	1.81	1.21	0.91	0.73	0.60	0.52	0.45	0.40	0.36
T-85	3½ x 4	21.12	10.56	7.04	5.28	4.22	3.52	3.02	2.64	2.34	2.10
T-86	3½ x 4	16.54	8.26	5.52	4.14	3.30	2.74	2.38	2.08	1.84	1.66
T-91	3½ x 3	10.90	5.44	3.62	2.72	2.18	1.82	1.54	1.36	1.20	1.10
T-92	3½ x 3	9.44	4.72	3.14	2.36	1.90	1.58	1.36	1.18	1.04	0.94
T-96	3 x 3½	15.89	7.95	5.30	3.97	3.18	2.65	2.29	1.98	1.76	1.59
T-97	3 x 3½	14.38	7.18	4.80	3.60	2.88	2.40	2.06	1.78	1.60	1.44
T-98	3 x 3½	12.46	6.22	4.16	3.12	2.48	2.08	1.78	1.56	1.38	1.26
T-103	2½ x 2	3.38	1.70	1.12	0.84	0.66	0.56	0.48	0.42	0.38	0.34
T-108	2½ x 1¾	2.06	1.04	0.70	0.52	0.40	0.34	0.30	0.26	0.24	0.20
T-112	2¼ x 2¼	3.00	1.50	1.00	0.75	0.60	0.50	0.43	0.38	0.33	0.30

For safe loads to the right of heavy line the deflection will be greater than allowable for plastered ceilings.

*Made only by special arrangement.

Zeas

Allowable Uniform Loads in Thousands of Pounds

Extreme Fiber Stress, 16,000 Pounds per Square Inch

Safe Loads Include Weight of Zee

Section Index	Size Depth, Inches	Size Flange, Inches	Weight per Foot, Pounds	SPAN IN FEET										
				4	5	6	7	8	9	10	12	14	16	
Z-70	5 $\frac{1}{8}$	3 $\frac{3}{8}$	28.4	29.81	23.89	19.91	17.07	14.93	13.27	11.95	9.96	8.53	7.47	
Z-71	5 $\frac{1}{8}$	3 $\frac{1}{8}$	26.0	27.57	22.06	18.38	15.76	13.78	12.25	11.03	9.19	7.87	6.89	
Z-72	5	3 $\frac{1}{4}$	23.7	25.25	20.20	16.83	14.43	12.62	11.22	10.10	8.41	7.21	6.31	
Z-73	5 $\frac{1}{8}$	3 $\frac{3}{8}$	22.6	25.52	20.41	17.01	14.58	12.76	11.34	10.21	8.50	7.29	6.38	
Z-74	5 $\frac{1}{8}$	3 $\frac{1}{8}$	20.2	22.99	18.39	15.32	13.13	11.49	10.21	9.20	7.66	6.56	5.74	
Z-75	5	3 $\frac{1}{4}$	17.9	20.48	16.38	13.65	11.70	10.24	9.10	8.19	6.83	5.85	5.12	
Z-76	5 $\frac{1}{8}$	3 $\frac{3}{8}$	16.4	19.84	15.87	13.22	11.33	9.92	8.82	7.93	6.61	5.66	4.96	
Z-77	5 $\frac{1}{8}$	3 $\frac{1}{8}$	14.0	17.04	13.63	11.36	9.73	8.52	7.57	6.81	5.68	4.86	4.26	
Z-78	5	3 $\frac{1}{4}$	11.6	14.24	11.39	9.49	8.13	7.12	6.33	5.69	4.74	4.06	3.56	
Z-80	4 $\frac{1}{8}$	3 $\frac{3}{8}$	23.0	19.36	15.49	12.90	11.06	9.68	8.60	7.74	6.45	5.53	4.84	
Z-81	4 $\frac{1}{8}$	3 $\frac{1}{8}$	20.9	17.73	14.18	11.82	10.13	8.86	7.88	7.09	5.91	5.06	4.43	
Z-82	4	3 $\frac{1}{4}$	18.9	16.13	12.90	10.74	9.22	8.06	7.17	6.45	5.37	4.61	4.03	
Z-83	4 $\frac{1}{8}$	3 $\frac{3}{8}$	18.0	16.48	13.18	10.98	9.41	8.24	7.32	6.59	5.49	4.70	4.12	
Z-84	4 $\frac{1}{8}$	3 $\frac{1}{8}$	15.9	14.66	11.73	9.78	8.38	7.33	6.52	5.86	4.89	4.19	3.66	
Z-85	4	3 $\frac{1}{4}$	13.8	12.88	10.30	8.58	7.36	6.44	5.72	5.15	4.29	3.68	3.22	
Z-86	4 $\frac{1}{8}$	3 $\frac{3}{8}$	12.5	12.45	9.96	8.30	7.11	6.22	5.53	4.98	4.15	3.55	3.11	
Z-87	4 $\frac{1}{8}$	3 $\frac{1}{8}$	10.3	10.43	8.34	6.94	5.96	5.21	4.63	4.17	3.47	2.98	2.60	
Z-88	4	3 $\frac{1}{4}$	8.2	8.37	6.70	5.58	4.78	4.18	3.72	3.35	2.79	2.39	2.09	
Z-3	3 $\frac{1}{8}$	2 $\frac{3}{4}$	14.3	9.15	7.32	6.09	5.22	4.57	4.06	3.66	3.05	2.61	2.28	
Z-4	3	2 $\frac{1}{4}$	12.6	8.16	6.53	5.44	4.66	4.08	3.62	3.26	2.72	2.32	2.04	
Z-7	3 $\frac{1}{8}$	2 $\frac{3}{4}$	11.5	7.95	6.36	5.29	4.54	3.97	3.53	3.18	2.65	2.27	1.98	
Z-8	3	2 $\frac{1}{4}$	9.8	6.85	5.48	4.57	3.91	3.42	3.04	2.74	2.28	1.95	1.71	
Z-11	3 $\frac{1}{8}$	2 $\frac{3}{4}$	8.5	6.35	5.08	4.23	3.63	3.17	2.82	2.54	2.11	1.81	1.58	
Z-12	3	2 $\frac{1}{4}$	6.7	5.12	4.09	3.41	2.92	2.56	2.27	2.05	1.70	1.46	1.28	
Z-18	3	1 $\frac{1}{2}$	3.59	2.72	2.18	1.81	1.55	1.36	1.21	1.09	0.91	0.78	0.68	

Zees

Continued

Allowable Uniform Loads in Thousands of Pounds

Extreme Fiber Stress, 16,000 Pounds per Square Inch

Safe Loads Include Weight of Zee


Neutral Axis Parallel to Flanges

SIZE			Weight per Foot, Pounds	1 FOOT SPAN	MAXIMUM SPAN 360 x DEFLECTION	
Depth, Inches	Flanges, Inches	Thickness, Inches		Safe Load	Safe Load	Length, Feet
5½	3¾	11	28.4	119.47	1.16	10.3
5½	3¾	11	26.0	110.39	1.08	10.2
5	3¾	11	23.7	101.01	1.00	10.1
5½	3¾	5	22.6	102.08	0.99	10.3
5½	3¾	5	20.2	91.95	0.90	10.2
5	3¾	5	17.9	81.92	0.81	10.1
5½	3¾	5	16.4	79.36	0.77	10.3
5½	3¾	5	14.0	68.16	0.67	10.2
5	3¾	5	11.6	56.96	0.57	10.1
4½	3¾	5	23.0	77.44	0.93	8.3
4½	3¾	5	20.9	70.93	0.87	8.2
4	3¾	5	18.9	64.53	0.80	8.1
4½	3¾	5	18.0	65.92	0.79	8.3
4½	3¾	5	15.9	58.67	0.72	8.2
4	3¾	5	13.8	51.52	0.64	8.1
4½	3¾	5	12.5	49.81	0.60	8.3
4½	3¾	5	10.3	41.71	0.51	8.2
4	3¾	5	8.2	33.49	0.41	8.1
3½	2¾	5	14.3	36.59	0.59	6.2
3	2¾	5	12.6	32.64	0.54	6.1
3½	2¾	5	11.5	31.79	0.51	6.2
3	2¾	5	9.8	27.41	0.45	6.1
3½	2¾	5	8.5	25.39	0.41	6.2
3	2¾	5	6.7	20.48	0.34	6.1
3	1½	5	3.59	10.89	0.18	2.7
2	1½	5	3.80	11.60	0.20	3.0
1½	1½	5	4.2	12.73	0.21	3.2

Beam Box Girders

Allowable Uniform Loads in Thousands of Pounds

The values below are based on extreme fiber stress of 16,000 pounds per square inch, $\frac{13}{16}$ " rivet holes deducted. Weights correspond to length, center to center of bearings.

Distance, Center to Center of Bearings, Feet	<div style="display: flex; justify-content: space-around; align-items: center;"> <div style="text-align: center;"> <p>2-10" Beams 25 Pounds per Foot</p>  </div> <div style="text-align: center;"> <p>2-12" x 1/2" Steel Plates</p> </div> </div>					
	Safe Load, includ- ing Weight of Girder	Weight of Girder, Pounds	Add to Safe Load for 5 Pounds In- crease in Weight of Beam	Add to Safe Load for 1/4" Increase in Thickness of Plates	Add to Weight of Girder for 5 Pounds Increase in Weight of Beam	Add to Weight of Girder for 1/4" Increase in Thickness of Plates
12	80.0	1,114	3.84	5.78	120	61
13	73.8	1,206	3.54	5.34	130	66
14	68.6	1,299	3.28	4.96	140	71
15	64.0	1,392	3.08	4.62	150	77
16	60.0	1,485	2.88	4.32	160	82
17	56.4	1,578	2.70	4.08	170	87
18	53.4	1,670	2.56	3.86	180	92
19	50.6	1,763	2.40	3.64	190	97
20	48.0	1,856	2.28	3.46	200	102
21	45.6	1,949	2.18	3.28	210	107
22	43.4	2,042	2.08	3.14	220	112
23	41.8	2,134	2.00	3.02	230	117
24	40.0	2,227	1.92	2.88	240	122
25	38.4	2,320	1.84	2.78	250	128
26	37.0	2,413	1.78	2.66	260	133
27	35.6	2,506	1.68	2.56	270	138
28	34.2	2,598	1.64	2.48	280	143
29	33.0	2,691	1.58	2.38	290	148
30	32.0	2,784	1.52	2.32	300	153
31	31.0	2,877	1.48	2.24	310	158
32	30.0	2,970	1.42	2.16	320	163
33	29.0	3,062	1.40	2.08	330	168
34	28.2	3,155	1.36	2.04	340	173
35	27.4	3,248	1.30	2.00	350	179
36	26.6	3,341	1.28	1.92	360	184
37	26.0	3,434	1.24	1.86	370	189
38	25.2	3,526	1.20	1.72	380	194

Beam Box Girders

Continued

Allowable Uniform Loads in Thousands of Pounds

The values below are based on extreme fiber stress of 16,000 pounds per square inch, $\frac{11}{16}$ " rivet holes deducted. Weights correspond to lengths, center to center of bearings.

Distance, Center to Center of Bearings, Feet	2-18" Beams 70 Pounds per Foot			2-16" Beams 55 Pounds per Foot			Add to Safe Load for $\frac{1}{16}$ " Increase in Thickness of Plates	Add to Weight of Girder for $\frac{1}{16}$ " Increase in Thickness of Plates
	Safe Load, including Weight of Girder	Weight of Girder, Pounds	Add to Safe Load for $\frac{1}{16}$ " Increase in Thickness of Plates	Safe Load, including Weight of Girder	Weight of Girder, Pounds	Add to Safe Load for $\frac{1}{16}$ " Increase in Weight of Beam		
12	325.2	2,712	13.36	302.6	2,352	7.84	13.36	82
13	300.2	2,938	12.34	279.4	2,548	7.24	12.34	88
14	278.8	3,164	11.46	259.4	2,744	6.72	11.46	95
15	260.2	3,390	10.70	242.2	2,940	6.28	10.70	102
16	243.8	3,616	10.02	227.0	3,136	5.88	10.02	109
17	229.6	3,842	9.44	213.6	3,332	5.54	9.44	116
18	216.8	4,068	8.90	201.8	3,528	5.22	8.90	122
19	205.4	4,294	8.44	191.2	3,724	4.94	8.44	129
20	195.0	4,520	8.02	181.6	3,920	4.70	8.02	136
21	185.8	4,746	7.64	173.0	4,116	4.48	7.64	143
22	177.4	4,972	7.28	163.4	4,312	4.28	7.28	150
23	169.6	5,198	6.98	157.8	4,508	4.08	6.98	156
24	162.6	5,424	6.68	151.4	4,704	3.92	6.68	163
25	156.0	5,650	6.42	145.2	4,900	3.76	6.42	170
26	150.0	5,876	6.16	139.6	5,096	3.62	6.16	177
27	144.4	6,102	5.94	134.4	5,292	3.48	5.94	184
28	139.4	6,328	5.72	129.6	5,488	3.36	5.72	190
29	134.6	6,554	5.52	125.2	5,684	3.24	5.52	197
30	130.0	6,780	5.34	121.0	5,880	3.14	5.34	204
31	125.8	7,006	5.16	117.2	6,076	3.04	5.16	211
32	122.0	7,232	5.00	113.4	6,272	2.94	5.00	218
33	118.2	7,458	4.86	109.0	6,468	2.84	4.86	224
34	114.8	7,684	4.72	106.8	6,664	2.76	4.72	231
35	111.4	7,910	4.58	103.8	6,860	2.68	4.58	238
36	108.4	8,136	4.46	100.8	7,056	2.60	4.46	245
37	105.4	8,362	4.34	98.2	7,252	2.52	4.34	252
38	102.6	8,588	4.22	95.6	7,448	2.46	4.22	258

Beam Box Girders

Continued

Allowable Uniform Loads in Thousands of Pounds

The values below are based on extreme fiber stress of 16,000 pounds per square inch, $\frac{1}{4}$ " rivet holes deducted. Weights correspond to lengths, center to center of bearings.



Distance, Center to Center of Bearings, Feet	<div> <div>2-20" Steel Beams 65 Pounds per Foot</div>  <div>2-16" x 3/4" Steel Plates</div> </div>				<div> <div>2-24" Steel Beams 80 Pounds per Foot</div>  <div>2-16" x 3/4" Steel Plates</div> </div>				Add to Weight of Girder for $\frac{1}{4}$ " Increase in Thickness of Plates
	Safe Load, including Weight of Girder	Weight of Girder, Pounds	Add to Safe Load for 5 Pounds Increase in Weight of Beam	Add to Safe Load for $\frac{1}{4}$ " Increase in Thickness of Plates	Safe Load, including Weight of Girder	Weight of Girder, Pounds	Add to Safe Load for 5 Pounds Increase in Weight of Beam	Add to Safe Load for $\frac{1}{4}$ " Increase in Thickness of Plates	
12	366.0	2,563	8.72	16.00	513.2	2,923	10.46	19.16	82
13	337.6	2,777	8.04	14.76	473.6	3,167	9.66	17.68	88
14	313.6	2,990	7.48	13.70	439.8	3,410	8.96	16.42	95
15	292.8	3,204	6.96	12.80	410.4	3,654	8.36	15.32	102
16	274.4	3,418	6.52	12.00	384.8	3,898	7.84	14.36	109
17	258.4	3,631	6.04	11.28	362.2	4,141	7.40	13.52	116
18	244.0	3,845	5.80	10.66	342.0	4,385	6.98	12.78	122
19	231.0	4,058	5.52	10.10	324.2	4,628	6.60	12.10	129
20	219.6	4,272	5.24	9.60	307.8	4,872	6.28	11.50	136
21	209.0	4,486	5.00	9.12	293.2	5,116	5.98	10.94	143
22	199.6	4,699	4.76	8.72	279.8	5,359	5.70	10.44	150
23	190.8	4,913	4.56	8.34	267.8	5,603	5.46	10.00	156
24	183.0	5,126	4.36	8.00	256.6	5,846	5.22	9.58	163
25	175.6	5,340	4.16	7.68	246.2	6,090	5.02	9.20	170
26	168.8	5,554	4.00	7.38	236.8	6,334	4.82	8.84	177
27	162.6	5,767	3.84	7.10	228.0	6,577	4.64	8.50	184
28	156.8	5,981	3.72	6.86	219.8	6,821	4.48	8.20	190
29	151.4	6,194	3.60	6.62	212.2	7,064	4.32	7.92	197
30	146.4	6,408	3.48	6.40	205.2	7,308	4.18	7.66	204
31	141.6	6,622	3.36	6.18	198.6	7,552	4.04	7.42	211
32	137.2	6,835	3.24	6.00	192.4	7,795	3.92	7.18	218
33	133.0	7,049	3.16	5.82	186.6	8,039	3.80	6.96	224
34	129.2	7,262	3.04	5.64	181.0	8,282	3.70	6.76	231
35	125.4	7,476	2.92	5.48	176.0	8,526	3.58	6.56	238
36	122.0	7,690	2.80	5.32	171.0	8,770	3.48	6.38	245
37	118.6	7,903	2.76	5.18	166.4	9,013	3.40	6.20	252
38	115.4	8,117	2.72	5.04	162.0	9,257	3.30	6.04	258

Plate Box Girders

Allowable Uniform Loads in Thousands of Pounds

The values below are founded on the moments of inertia of the sections using an extreme fiber stress of 16,000 pounds per square inch for steel; $\frac{11}{16}$ " rivet holes in both flanges deducted. Weight of girders correspond to lengths, center to center of bearings and include rivet heads, stiffeners and fillers.

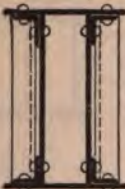



Distance, Center to Center of Bearings, Feet	 30" x $\frac{1}{2}$ " Web Plates 16" x $\frac{3}{8}$ " Flange Plates 3 $\frac{1}{2}$ " x 3 $\frac{1}{2}$ " x $\frac{1}{2}$ " Angles				 33" x $\frac{1}{2}$ " Web Plates 20" x $\frac{1}{4}$ " Flange Plates 3 $\frac{1}{2}$ " x 3 $\frac{1}{2}$ " x $\frac{1}{2}$ " Angles			
	Safe Load, including Weight of Girder	Weight of Girder, Pounds	Increase in Safe Load for $\frac{1}{8}$ " Increase in Thickness of Flange Plates	Increase in Weight of Girder for $\frac{1}{8}$ " Increase in Thickness of Flange Plates	Safe Load, including Weight of Girder	Weight of Girder, Pounds	Increase in Safe Load for $\frac{1}{8}$ " Increase in Thickness of Flange Plates	Increase in Weight of Girder for $\frac{1}{8}$ " Increase in Thickness of Flange Plates
20	240.00	4.26	14.08	.07	320.4	4.88	19.08	.09
21	228.56	4.46	13.40	.07	315.2	5.10	18.16	.09
22	218.18	4.64	12.80	.08	291.2	5.32	17.34	.09
23	208.68	4.90	12.24	.08	278.6	5.60	16.58	.10
24	200.00	5.08	11.72	.08	267.0	5.82	15.90	.10
25	192.00	5.28	11.26	.09	256.4	6.06	15.26	.11
26	184.60	5.48	10.82	.09	246.4	6.28	14.68	.11
27	177.76	5.66	10.42	.09	237.4	6.50	14.14	.12
28	171.42	5.86	10.06	.10	228.8	6.72	13.64	.12
29	165.52	6.12	9.70	.10	221.0	7.00	13.16	.12
30	160.00	6.32	9.38	.10	213.6	7.22	12.72	.13
31	154.84	6.50	9.08	.11	206.6	7.44	12.30	.13
32	150.00	6.70	8.80	.11	200.2	7.66	11.92	.14
33	145.44	7.00	8.52	.11	194.2	7.90	11.56	.14
34	141.18	7.08	8.28	.12	188.4	8.12	11.20	.14
35	137.14	7.28	8.04	.12	183.0	8.34	10.88	.15
36	133.32	7.52	7.82	.12	178.0	8.62	10.58	.15
37	129.72	7.72	7.60	.13	173.2	8.82	10.28	.16
38	126.32	7.90	7.40	.13	168.6	9.06	10.02	.16
39	122.08	8.10	7.22	.13	164.2	9.30	9.76	.17
40	120.00	8.30	7.04	.14	160.2	9.52	9.54	.17

Plate Box Girders

Continued

Allowable Uniform Loads in Thousands of Pounds

The values below are founded on the moments of inertia of the sections using an extreme fiber stress of 16,000 pounds per square inch for steel; $\frac{11}{16}$ " rivet holes in both flanges deducted. Weights of girders correspond to lengths, center to center of bearings and include rivet heads, stiffeners and fillers.

Distance, Center to Center of Bearings, Feet	 30" x $\frac{1}{2}$ " Web Plates 24" x $\frac{1}{8}$ " Flange Plates 4" x 3 $\frac{1}{2}$ " x $\frac{1}{2}$ " Angles				 42" x $\frac{1}{2}$ " Web Plates 30" x $\frac{1}{8}$ " Flange Plates 5" x 4" x $\frac{1}{2}$ " Angles			
	Safe Load, including Weight of Girder	Weight of Girder, Pounds	Increase in Safe Load for $\frac{1}{16}$ " Increase in Thickness of Flange Plates	Increase in Weight of Girder for $\frac{1}{16}$ " Increase in Thickness of Flange Plates	Safe Load, including Weight of Girder	Weight of Girder, Pounds	Increase in Safe Load for $\frac{1}{16}$ " Increase in Thickness of Flange Plates	Increase in Weight of Girder for $\frac{1}{16}$ " Increase in Thickness of Flange Plates
20	455.0	5.84	25.84	.10	710.0	7.56	38.46	.13
21	433.4	6.12	24.60	.11	676.2	7.90	37.00	.13
22	413.8	6.38	23.48	.11	645.6	8.26	35.32	.14
23	395.8	6.72	22.46	.12	617.4	8.68	33.78	.15
24	379.2	6.98	21.52	.12	592.0	9.04	32.38	.15
25	364.0	7.26	20.66	.13	568.0	9.38	31.08	.16
26	350.0	7.52	19.88	.13	546.2	9.74	29.88	.17
27	337.0	7.78	19.14	.14	526.0	10.08	28.78	.17
28	325.2	8.06	18.44	.14	507.2	10.42	27.76	.18
29	313.8	8.30	17.82	.15	489.6	10.86	26.80	.19
30	303.4	8.66	17.22	.15	473.4	11.22	25.90	.19
31	293.6	8.90	16.66	.16	458.0	11.56	25.06	.20
32	284.4	9.20	16.14	.16	443.8	11.90	24.28	.20
33	275.8	9.48	15.66	.17	430.4	12.24	23.54	.21
34	267.6	9.74	15.20	.17	417.6	12.58	22.86	.22
35	260.0	10.00	14.76	.18	405.8	12.94	22.20	.22
36	252.8	10.34	14.34	.18	394.4	13.38	21.58	.23
37	246.0	10.62	13.96	.19	383.8	13.72	21.00	.24
38	239.4	10.88	13.60	.19	373.6	13.88	20.44	.24
39	233.4	11.16	13.24	.20	364.2	14.40	19.92	.25
40	227.6	11.42	12.92	.20	355.0	14.76	19.42	.26

Columns and Struts

Members in a structure subject to compression are termed—Columns, Posts or Struts. Theory offers no exact formulae from which the strength of these members, under various conditions of loading may be figured. Empirical formulae, based on the assumption that the members under stress may fail by direct compression, by combined compression and bending, or bending alone, practically agree with results obtained by experiment on full sized members. These experiments show that steel columns of ordinary sizes and lengths fail at nearly a constant stress which corresponds to the yield point of that material, and that the load which will cause the column to fail decreases in the ratio of its length to its least radius of gyration.

Strength of Columns

Columns are dependent upon their area and shape of cross section for their strength. Long columns will fail by bending under less load than will short columns. Of two columns having the same sectional area, the one having the material in the section distributed farthest from the central axis of the column will be stronger than the one having the bulk of material located near the center. If all the material composing the cross section of a column could be located at a distance from the center equal to the radius of gyration, the column would possess the same strength to resist flexure as though the material was distributed over the cross section. Therefore, in formulae for calculating the strength of columns, both the radius of gyration and the length must be taken into consideration.

Design of Columns

Hollow round columns are the most economical in material, and single web columns are the most accessible for painting and inspection. Columns should be so designed as to facilitate connecting floor beams or girders on all sides. Connections to columns should be carefully designed and provided with sufficient rivets, to avoid failure of the connections by shearing of the rivets. It is the common practice to space rivets not more than 3 inches, center to center, at the ends of columns for a distance equal to twice the width of the column. The distance between rivets from center to center, in a direction parallel with the line of strain, should not exceed 16 times the least thickness of the thinnest outside plate; and the distance from center to center between the rivets at right angles to the line of strain, should not exceed 32 times the least thickness of metal.

Tabulated Column Sections

On pages 182 to 203 will be found the safe loads in thousands of pounds for column sections, not exceeding lengths of 150 radii, which are typical of present day use.

Columns

Continued

Formulae for Safe Loads

Columns subject to eccentric loading may be figured for safe carrying capacity by the following formulae:

$$A = \frac{W}{P} + \frac{w d e}{P r^2}$$

P = Working unit stress (pounds square inch)

A = Area of column (square inches)

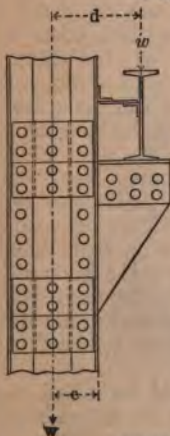
W = Total direct and eccentric loads (pounds)

w = Eccentric load (pounds)

d = Eccentricity of w (inches)

r = Radius of gyration in direction of eccentricity (inches)

e = Distance from center of column to outer fiber in direction of eccentricity (inches)



EXAMPLE:

Required the sectional area of a 12" plate and angle column 18' 0" long necessary to sustain safely a direct load of 100,000 pounds, and an eccentric load of 20,000 pounds located at a distance of 12" from center of column in the direction of web.

From the column tables on page 188, we find the safe working unit stress for a 12" column 18' 0" long to be about 10,000 pounds.

The trial radius of gyration may be taken as 5, which corresponds to the radius about the y - y axis for one of the 12" columns.

The required area of the cross section of column may be computed as follows:

$$\begin{aligned} A &= \frac{100,000 + 20,000}{10,000} + \frac{20,000 \times 12 \times 6\frac{1}{4}}{10,000 \times 25} \\ &= 12\Box'' + 6\Box'' \\ &= 18\Box'' \end{aligned}$$

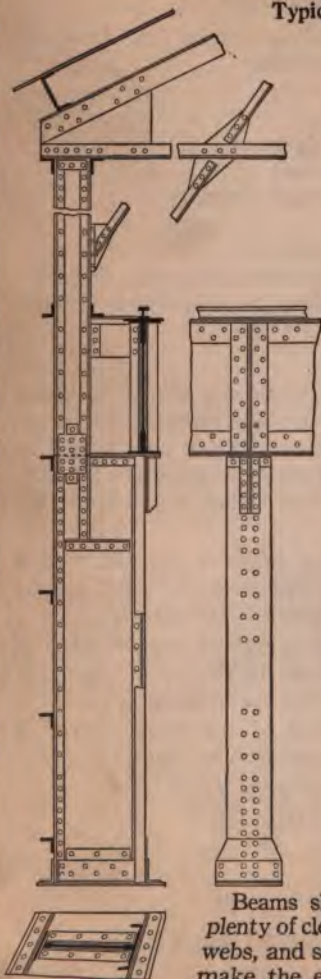
And the following column section may be used:

4 - 6" × 4" × 3/8" angles 1 - 12" × 3/8" plate	}	Area 18.94 square inches.
---	---	---------------------------

Columns

Continued

Typical Details



In designing and detailing mill and office buildings, it is desirable to have the loads transmitted from the trusses, girders and beams directly to the columns and eliminate bending or secondary stresses.

For the most economical construction, simplicity in details is very essential, and the number of connecting pieces, rivets or bolts should be reduced to a minimum.

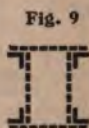
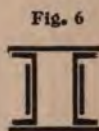
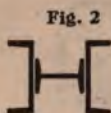
The typical column details shown on these pages cover a few examples of the most modern practice in structural work, as met with in the ordinary mill and office building construction.

When columns rest on masonry, gusset plates may be required to distribute the load. Where they rest on steel slabs or cast iron bases, the loads are transmitted directly into the footing, and base angles only are required to fasten columns to slabs or bases.

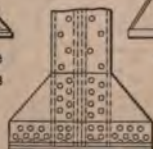
Column should be milled to accurately bear at splices and base, to have splice plates of sufficient size with the necessary rivets to hold the section in line and to resist the stresses due to bending.

Beams should be framed to columns with plenty of clearance especially when framing into webs, and sufficient rivets countersunk so as to make the erection as simple as possible.

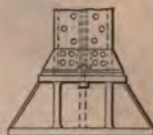
Columns
Continued
Typical Built Sections



Column Base
for light loads
Fig. 13



Built up Column Base
for heavy loads
Fig. 14



Column Base with
Cast Iron or
Cast Steel Base
Fig. 15

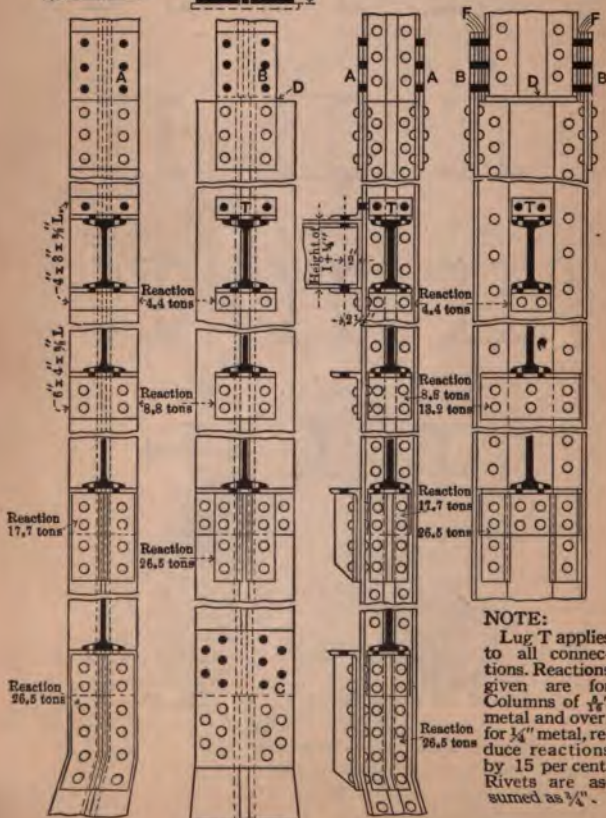
Dotted lines indicate lattice

Columns Continued



General Details of Splices

And of Connections for I Beams
to Plate and Angle Columns.

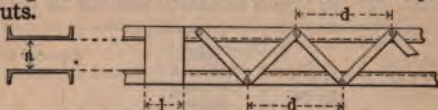


Columns

Continued

Lattice Bars and Tie Plates

Table giving minimum sizes of lattice bars and tie plates used for channel struts.



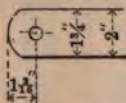
Depth of Channel, Inches	Back to Back of Channel "a," Inches	Section of Lattice Bars, Inches	Thickness of Tie Plates, Inches	Size of Rivet, Inches	Length of Tie Plates "l," Inches	Rivet Spacing "d"			
						Maximum		Minimum	
						Feet	Inches	Feet	Inches
6	4	1½ x ¼	¼	½	7½	0	11½	0	6⅝
7	4¾	1¾ x ¼	¼	⅝	10	1	1½	0	7⅝
8	5½	2 x ⅝	⅝	¾	10	1	3	0	8⅞
9	6	2 x ⅝	⅝	¾	12	1	4½	0	9½
10	6¾	2 x ¾	¾	¾	12	1	6½	0	10⅞
12	8¼	2½ x ¾	¾	¾	15	1	10½	1	1
15	10¼	2½ x ¾	¾	¾	15	2	2½	1	3⅝

Sketches showing finished ends of lattice bars and clearance between same when cut from long bars.

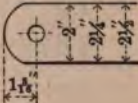
½" Rivet



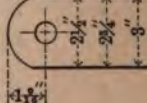
⅝" Rivet



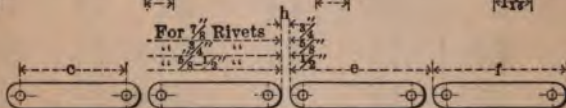
¾" Rivet



⅞" Rivet



For ⅞ Rivets



c = distance center to center of rivet holes.

f = $c + 2$ distances as per sketch above.

e = $f + h$.

In struts and columns carrying calculated stresses, the tie plates should be placed as near the ends as practicable, and at intermediate points where the lattice bars are not continuous. The end tie plates should have a length at least equal to the distance between lines of rivets connecting them to the flanges. These lattice bars should be capable of resisting a shearing stress equal to 2 per cent. of the direct stress. The thickness of lattice bars for single lattice should be at least 2½ per cent. of the distance between end rivets.

Rule for Latticing of Channels and Angles

d = Maximum length between lattice bars

L = Total length of strut or column

r = Least radius of gyration for a single channel

R = Least radius of gyration for the whole section

$$d = \frac{rL}{R}$$

Columns

Continued

Allowed stresses per square inch.
14,000 pounds for lengths less than 30 radii.

16,000—70 $\frac{1}{r}$ for lengths between 30 radii and 150 radii.

Depth of Beam, Inches	Weight per Foot, Pounds	Area, Square Inches	Least Radius of Gyration, Inches	LENGTH IN FEET		
				3	4	5
24	100	29.41	1.28	393.4	374.1
24	80	23.32	1.36	315.5	301.1
20	100	29.41	1.34	396.8	378.4
20	80	23.73	1.39	322.3	308.0
20	65	19.08	1.21	252.3	239.1
18	70	20.59	1.09	281.8	266.0	250.1
18	55	15.93	1.15	220.0	208.3	196.7
15	60	17.67	1.21	233.7	221.4
15	42	12.48	1.08	170.6	160.9	151.1
12	55	16.18	1.04	219.7	206.6	193.5
12	40	11.84	1.08	161.8	152.6	143.4
12	31½	9.26	1.01	125.1	117.4	109.7
10	40	11.76	0.90	155.2	144.3	133.3
10	25	7.37	0.97	98.8	92.4	86.0
9	35	10.29	0.84	133.8	123.5	113.2
9	21	6.18	0.90	81.6	75.9	70.1
8	25½	7.50	0.80	96.4	88.5	80.6
8	18	5.33	0.84	69.3	64.0	58.6
7	20	5.88	0.74	74.1	67.4	60.7
7	15	4.42	0.78	56.4	51.7	46.9
6	17¼	5.07	0.68	62.3	56.1	49.8
6	12¼	3.61	0.72	45.1	40.9	36.7
5	14¾	4.34	0.63	52.1	46.3	40.5
5	9¾	2.87	0.65	34.8	31.1	27.4
4	10¼	3.09	0.57	35.8	31.2	26.7
4	7½	2.21	0.59	25.9	22.8	19.6
3	7½	2.21	0.52	24.7	21.1	17.5
3	5½	1.63	0.53	18.3	15.7	13.2

This table continued on next page.

JONES & LAUGHLIN STEEL COMPANY

Safe Loads in Thousands of Pounds For Single Beam Columns, Square Ends

LENGTH IN FEET

6	7	8	9	10	12	14	16
354.8	335.5	316.2	296.9	277.6	239.0	200.4	161.8
286.7	272.3	257.9	243.5	229.1	200.3	171.5	142.7
359.9	341.5	323.1	304.6	286.2	249.3	212.5	175.6
293.6	279.3	264.9	250.6	236.3	207.6	178.9	150.2
225.8	212.6	199.3	186.1	172.8	146.3	119.8
234.2	218.4	202.5	186.6	170.8	139.0
185.1	173.4	161.8	150.2	138.5	115.3	92.0
209.1	196.9	184.6	172.3	160.1	135.5	111.0
141.4	131.7	122.0	112.3	102.6	83.2
180.5	167.4	154.3	141.3	128.2	102.1
134.2	125.0	115.8	106.6	97.4	78.9
102.0	94.3	86.6	78.9	71.1	55.7
122.3	111.3	100.4	89.4	78.4
79.6	73.2	66.9	60.5	54.1	41.3
102.9	92.6	82.3	72.0	61.7
64.3	58.5	52.8	47.0	41.3
72.8	64.9	57.0	49.1	41.3
53.3	48.0	42.6	37.3	32.0
54.0	47.4	40.7	34.0
42.2	37.4	32.6	27.9
43.5	37.3	31.0
32.5	28.3	24.1	19.9
34.7	28.9
23.7	20.0	16.2
22.1	17.6
16.5	13.3
13.9
10.6

Columns

Continued

Safe Loads in Thousands of Pounds for Plate and Angle Columns, Square Ends

Short legs of angles riveted to web plates.
Column weights do not include rivets.

Allowed stresses per square inch.
14,000 pounds for lengths less than 30 radii.

16,000—70 — for lengths between 30 radii and 150 radii.

Size of Angles, Inches	Size of Web Plates, Inches	Size of Cover Plates, Inches	Area of Column, Square Inches	Weight per Foot of Column, Pounds	Least Radius of Gyration, Inches	Length in Feet						
						4	5	6	7	8	9	10
3 x 3 1/2 x 3 1/2	6 x 1 1/2	—	6.74	23.1	1.24	89.6	85.0	80.4	75.9	71.3	66.7	62.2
3 x 3 1/2 x 3 1/2	6 x 1 1/2	—	8.36	28.8	1.27	111.6	106.1	100.6	95.1	89.5	84.0	78.5
3 x 3 1/2 x 3 1/2	6 x 1 1/2	—	9.93	34.1	1.30	133.2	126.8	120.4	114.0	107.6	101.1	94.7
3 x 3 1/2 x 3 1/2	6 x 1 1/2	—	11.47	39.3	1.33	154.5	147.3	140.1	132.8	125.6	118.3	111.1
4 x 4 x 4	8 x 1 1/2	—	10.86	37.3	1.67	—	—	141.0	135.5	130.1	124.6	119.1
4 x 4 x 4	8 x 1 1/2	—	12.92	44.2	1.70	—	—	168.4	162.0	155.6	149.3	142.9
4 x 4 x 4	8 x 1 1/2	—	14.98	51.1	1.73	—	—	196.0	188.8	181.5	174.2	166.9
4 x 4 x 4	8 x 1 1/2	—	17.00	58.0	1.76	—	—	223.3	215.2	207.1	199.0	190.9
4 x 4 x 4	8 x 1 1/2	—	18.98	64.9	1.79	—	—	250.2	241.3	232.4	223.5	214.6
5 x 5 x 5	10 x 1 1/2	—	13.37	45.4	2.08	—	—	181.5	176.1	170.7	165.3	159.9
5 x 5 x 5	10 x 1 1/2	—	15.95	54.4	2.10	—	—	216.9	210.5	204.2	197.8	191.4
5 x 5 x 5	10 x 1 1/2	—	18.50	62.9	2.13	—	—	252.2	244.9	237.6	230.3	223.0
5 x 5 x 5	10 x 1 1/2	—	21.00	71.4	2.16	—	—	287.0	278.8	270.7	262.5	254.3
5 x 5 x 5	10 x 1 1/2	—	23.51	79.9	2.19	—	—	322.1	313.0	304.0	295.0	286.0
5 x 5 x 5	10 x 1 1/2	—	25.93	88.5	2.22	—	—	356.0	346.2	336.4	326.6	316.8
5 x 5 x 5	10 x 1 1/2	—	28.36	96.6	2.25	—	—	390.2	379.6	369.1	358.5	347.9
5 x 5 x 5	10 x 1 1/2	—	30.74	104.7	2.29	—	—	424.2	412.9	401.6	390.4	379.1

This table continued below.



Size of Angles, Inches	Size of Web Plates, Inches	Size of Cover Plates, Inches	Area of Column, Square Inches	Weight per Foot of Column, Pounds	Least Radius of Gyration, Inches	Length in Feet							
						14	16	18	20	22	24	26	28
3 1/2 x 3 1/2	6 x 1/4	1/4	6.74	23.1	1.24	44.0							
3 1/2 x 3 1/2	6 x 1/4	1/4	8.36	28.8	1.27	56.3							
3 1/2 x 3 1/2	6 x 1/4	1/4	9.93	34.1	1.30	69.1	56.2						
3 1/2 x 3 1/2	6 x 1/4	1/4	11.47	39.3	1.33	82.1	67.6						
3 1/2 x 3 1/2	8 x 1/4	1/4	10.86	37.3	1.67	97.3	86.4	75.4	64.5				
3 1/2 x 3 1/2	8 x 1/4	1/4	12.92	44.2	1.70	117.3	104.6	91.8	79.0				
3 1/2 x 3 1/2	8 x 1/4	1/4	14.98	51.1	1.73	137.9	123.3	108.8	94.2				
3 1/2 x 3 1/2	8 x 1/4	1/4	17.00	58.0	1.76	158.4	142.2	126.0	109.7	93.5			
3 1/2 x 3 1/2	8 x 1/4	1/4	18.98	64.9	1.79	179.0	161.2	143.4	125.5	107.7			
3 1/2 x 3 1/2	10 x 1/4	1/4	13.37	45.4	2.08	138.3	127.5	116.7	105.9	95.1	84.3	73.5	
3 1/2 x 3 1/2	10 x 1/4	1/4	15.95	54.4	2.10	165.9	153.1	140.4	127.6	114.8	102.1	89.3	
3 1/2 x 3 1/2	10 x 1/4	1/4	18.50	62.9	2.13	193.9	179.3	164.7	150.1	135.5	120.9	106.3	
3 1/2 x 3 1/2	10 x 1/4	1/4	21.00	71.4	2.16	221.6	205.3	189.0	172.6	156.3	139.9	123.6	
3 1/2 x 3 1/2	10 x 1/4	1/4	23.51	79.9	2.19	250.0	233.0	215.0	197.0	180.0	162.0	144.0	

Columns
Continued

Safe Load in Thousands of Pounds for Plate and Angle Columns, Square Ends

Allowed stresses per square inch.

14,000 pounds for lengths less than 30 radii.

16,000—70 — for lengths between 30 radii and 150 radii.

Short legs of angles riveted to web plates.
Column weights do not include rivets.

Size of Angles, Inches	Size of Web Plates, Inches	Size of Cover Plates, Inches	Area of Square Column, Inches	Weight Per Foot of Column, Pounds	Least Radius of Gyration, Inches	Length in Feet								
						9	10	12	14	16	18	20	22	24
8 x 6 x 1 1/2	14 x 1 1/2	34.00	115.6	3.33	466.8	458.2	441.1	423.9	406.8	389.6	372.5	355.3	338.1
8 x 6 x 1 1/8	14 x 1 1/8	38.12	129.6	3.36	524.2	514.6	495.5	476.5	457.4	438.4	419.3	400.2	381.2
8 x 6 x 1 1/8	14 x 1 1/8	42.19	143.4	3.39	581.0	570.5	549.6	528.7	507.8	486.9	466.0	445.0	424.1
8 x 6 x 1 1/8	14 x 1 1/8	46.23	157.2	3.42	637.5	626.1	603.4	580.7	558.0	535.3	512.6	489.9	467.2
8 x 6 x 1 1/8	14 x 1 1/8	50.26	170.9	3.45	694.0	681.8	657.3	632.8	608.4	583.9	559.4	535.0	510.5
8 x 6 x 1 1/8	14 x 1 1/8	54.26	184.5	3.48	750.3	737.2	711.0	684.8	658.6	632.4	606.2	580.0	553.8
8 x 6 x 1 1/8	14 x 1 1/8	58.17	197.8	3.51	805.4	791.5	763.7	735.8	708.0	680.1	652.3	624.5	596.6
8 x 6 x 1 1/8	14 x 1 1/8	62.13	211.2	3.54	861.4	846.7	817.2	787.7	758.2	728.7	699.2	669.7	640.3
8 x 6 x 1 1/8	14 x 1 1/8	66.00	224.4	3.57	916.2	900.7	869.7	838.6	807.5	776.5	745.4	714.4	683.3
8 x 6 x 1 1/8	16 x 1 1/8	18 x 1 1/8	69.76	237.2	3.94	967.4	937.7	908.0	878.2	848.5	818.7	789.0	759.3
8 x 6 x 1 1/8	16 x 1 1/8	18 x 1 1/8	77.92	264.9	3.93	1080.2	1046.9	1013.6	980.2	946.9	913.6	880.3	847.0
8 x 6 x 1 1/8	16 x 1 1/8	18 x 1 1/8	86.00	292.4	3.93	1192.2	1155.4	1118.7	1081.9	1045.1	1008.4	971.6	934.8
8 x 6 x 1 1/8	16 x 1 1/8	18 x 1 1/8	90.50	307.7	4.00	1258.0	1219.9	1181.9	1143.9	1105.9	1067.9	1029.9	991.9
8 x 6 x 1 1/8	16 x 1 1/8	18 x 1 1/8	95.00	323.0	4.06	1284.1	1244.8	1205.5	1166.2	1126.9	1087.6	1048.3
8 x 6 x 1 1/8	16 x 1 1/8	18 x 1 1/8	99.50	338.3	4.12	1348.6	1308.0	1267.4	1226.9	1186.3	1145.7	1105.1
8 x 6 x 1 1/8	16 x 1 1/8	18 x 1 1/8	104.00	353.6	4.17	1412.6	1370.7	1328.8	1286.9	1245.0	1203.1	1161.2
8 x 6 x 1 1/8	16 x 1 1/8	18 x 1 1/8	108.50	368.9	4.22	1476.8	1433.3	1390.5	1347.3	1304.1	1260.9	1217.7
8 x 6 x 1 1/8	16 x 1 1/8	18 x 1 1/8	113.00	384.2	4.26	1540.6	1496.1	1451.9	1406.9	1362.4	1317.8	1273.2
8 x 6 x 1 1/8	16 x 1 1/8	18 x 1 1/8	117.50	399.5	4.30	1604.6	1558.7	1512.8	1466.9	1420.9	1375.0	1329.1

This table continued below.



Size of Angles, Inches	Size of Web Plates, Inches	Size of Cover Plates, Inches	Area of Column, Square Inches	Weight Per Foot of Column, Pounds	Least Radius of Gyration, Inches	Length in Feet							
						26	28	30	32	34	36	38	40
8 x 6 x 1 1/2	14 x 1 1/2	34.00	115.6	3.33	321.0	303.8	286.7	260.5	252.4	235.2	218.1	200.9
8 x 6 x 1 1/4	14 x 1 1/4	38.12	129.6	3.36	362.1	343.0	324.0	304.9	285.9	266.8	247.7	228.7
8 x 6 x 1 3/8	14 x 1 3/8	42.19	143.4	3.39	403.2	382.3	361.4	340.5	319.6	298.7	277.8	256.9
8 x 6 x 1 1/2	14 x 1 1/2	46.23	157.2	3.42	444.5	421.7	399.0	376.3	353.6	330.9	308.2	285.5
8 x 6 x 1 1/4	14 x 1 1/4	50.26	170.9	3.45	486.0	461.5	437.1	412.6	388.1	363.7	339.2	314.7
8 x 6 x 1 3/8	14 x 1 3/8	54.26	184.5	3.48	527.7	501.5	475.3	449.1	422.9	396.7	370.5	344.3
8 x 6 x 1 1/2	14 x 1 1/2	58.17	197.8	3.51	568.8	540.9	513.1	485.2	457.4	429.6	401.7	373.9
8 x 6 x 1 1/4	14 x 1 1/4	62.13	211.2	3.54	610.8	581.3	551.8	522.3	492.8	463.3	433.9	404.4
8 x 6 x 1 3/8	14 x 1 3/8	66.00	224.4	3.57	652.3	621.2	590.2	559.1	528.0	497.0	465.9	434.9
8 x 6 x 1 1/2	16 x 1 1/2	18 x 1 1/2	69.76	237.2	3.94	729.5	699.5	670.1	640.3	610.6	580.8	551.1	521.4
8 x 6 x 1 1/4	16 x 1 1/4	18 x 1 1/4	77.92	264.9	3.93	813.7	780.4	747.1	713.8	680.5	647.1	613.8	580.5
8 x 6 x 1 3/8	16 x 1 3/8	18 x 1 3/8	86.00	292.4	3.93	898.1	861.3	824.5	787.8	751.0	714.3	677.5	640.7
8 x 6 x 1 1/2	16 x 1 1/2	18 x 1 1/2	90.50	307.7	4.00	953.9	915.9	877.9	839.8	801.8	763.8	725.8	687.8
8 x 6 x 1 1/4	16 x 1 1/4	18 x 1 1/4	95.00	323.0	4.06	1008.9	969.6	930.3	891.0	851.7	812.4	773.1	733.7
8 x 6 x 1 3/8	16 x 1 3/8	18 x 1 3/8	99.50	338.3	4.12	1064.6	1024.0	983.4	942.9	902.3	861.7	821.1	780.6
8 x 6 x 1 1/2	16 x 1 1/2	18 x 1 1/2	104.00	353.6	4.17	1119.3	1077.4	1035.5	993.6	951.8	909.9	868.0	826.1
8 x 6 x 1 1/4	16 x 1 1/4	18 x 1 1/4	108.50	368.9	4.22	1174.5	1131.3	1088.1	1044.9	1001.7	958.5	915.3	872.1
8 x 6 x 1 3/8	16 x 1 3/8	18 x 1 3/8	113.00	384.2	4.26	1228.7	1184.1	1139.5	1095.0	1050.4	1005.9	961.3	916.7
8 x 6 x 1 1/2	16 x 1 1/2	18 x 1 1/2	117.50	399.5	4.30	1283.2	1237.3	1191.4	1145.5	1099.6	1053.7	1007.8	961.9

This table continued on next page.

Columns
Continued

Safe Load in Thousands of Pounds for Plate and Angle Columns, Square Ends

Short legs of angles riveted to web plates.
Column weights do not include rivets.

Allowed stresses per square inch.

14,000 pounds for lengths less than 30 radii.

$\frac{1}{r}$ 16,000—70 — for lengths between 30 radii and 150 radii.

Size of Angles, Inches	Size of Web Plates, Inches	Size of Cover Plates, Inches	Area of Column, Square Inches	Weight Per Foot of Column, Pounds	Least Radius of Gyration, Inches	Length in Feet								
						9	10	12	14	16	18	20	22	24
8 x 6 x $\frac{1}{2}$	14 x $\frac{1}{2}$	34.00	115.6	3.33	466.8	458.2	441.1	423.9	406.8	389.6	372.5	355.3	338.1
8 x 6 x $\frac{3}{8}$	14 x $\frac{3}{8}$	38.12	129.0	3.36	524.2	514.6	495.5	476.5	457.4	438.4	419.3	400.2	381.2
8 x 6 x $\frac{1}{2}$	14 x $\frac{1}{2}$	42.19	143.4	3.39	581.0	570.5	549.6	528.7	507.8	486.9	466.0	445.0	424.1
8 x 6 x $\frac{3}{8}$	14 x $\frac{3}{8}$	46.23	157.2	3.42	637.5	626.1	603.4	580.7	558.0	535.3	512.6	489.9	467.2
8 x 6 x $\frac{1}{2}$	14 x $\frac{1}{2}$	50.26	170.9	3.45	694.0	681.8	657.3	632.8	608.4	583.9	559.4	535.0	510.5
8 x 6 x $\frac{3}{8}$	14 x $\frac{3}{8}$	54.26	184.5	3.48	750.3	737.2	711.0	684.8	658.6	632.4	606.2	580.0	553.8
8 x 6 x $\frac{1}{2}$	14 x $\frac{1}{2}$	58.17	197.8	3.51	805.4	791.5	763.7	735.8	708.0	680.1	652.3	624.5	596.6
8 x 6 x $\frac{3}{8}$	14 x $\frac{3}{8}$	62.13	211.2	3.54	861.4	846.7	817.2	787.7	758.2	728.7	699.2	669.7	640.3
8 x 6 x $\frac{1}{2}$	14 x $\frac{1}{2}$	66.00	224.4	3.57	916.2	900.7	869.7	838.6	807.5	776.5	745.4	714.4	683.3
8 x 6 x $\frac{3}{8}$	16 x $\frac{3}{8}$	18 x $\frac{1}{2}$	69.76	237.2	3.94	967.4	937.7	908.0	878.2	848.5	818.7	789.0	759.3
8 x 6 x $\frac{1}{2}$	16 x $\frac{1}{2}$	18 x $\frac{3}{8}$	77.92	264.9	3.93	1080.2	1046.9	1013.6	980.2	946.9	913.6	880.3	847.0
8 x 6 x $\frac{3}{8}$	16 x $\frac{3}{8}$	18 x $\frac{1}{2}$	86.00	292.4	3.93	1192.2	1155.4	1118.7	1081.9	1045.1	1008.4	971.6	934.8
8 x 6 x $\frac{1}{2}$	16 x $\frac{1}{2}$	18 x $\frac{3}{8}$	90.50	307.7	4.00	1258.0	1219.9	1181.9	1143.9	1105.9	1067.9	1029.9	991.9
8 x 6 x $\frac{3}{8}$	16 x $\frac{3}{8}$	18 x $\frac{1}{2}$	95.00	323.0	4.06	1284.1	1244.8	1205.5	1166.2	1126.9	1087.6	1048.3
8 x 6 x $\frac{1}{2}$	16 x $\frac{1}{2}$	18 x $\frac{3}{8}$	99.50	338.3	4.12	1348.6	1308.0	1267.4	1226.9	1186.3	1145.7	1105.1
8 x 6 x $\frac{3}{8}$	16 x $\frac{3}{8}$	18 x $\frac{1}{2}$	104.00	353.6	4.17	1412.6	1370.7	1328.8	1286.9	1245.0	1203.1	1161.2
8 x 6 x $\frac{1}{2}$	16 x $\frac{1}{2}$	18 x $\frac{3}{8}$	108.50	368.9	4.22	1476.8	1433.6	1390.5	1347.3	1304.1	1260.9	1217.7
8 x 6 x $\frac{3}{8}$	16 x $\frac{3}{8}$	18 x $\frac{1}{2}$	113.00	384.2	4.26	1540.6	1496.1	1451.5	1406.9	1362.4	1317.8	1273.2
8 x 6 x $\frac{1}{2}$	16 x $\frac{1}{2}$	18 x $\frac{3}{8}$	117.50	399.5	4.30	1604.6	1558.7	1512.8	1466.9	1420.9	1375.0	1329.1

This table continued below.



Size of Angles, Inches	Size of Web Plates, Inches	Size of Cover Plates, Inches	Area of Column, Square Inches	Weight Per Foot of Column, Pounds	Least Radius of Gyration, Inches	LENGTH IN FEET							
						26	28	30	32	34	36	38	40
8 x 6 x 1/2	14 x 1/2	18 x 1/2	34.00	115.6	3.33	321.0	303.8	286.7	269.5	252.4	235.2	218.1	200.9
8 x 6 x 3/4	14 x 3/4	18 x 3/4	38.12	129.6	3.36	362.1	343.0	324.0	304.9	285.9	266.8	247.7	228.7
8 x 6 x 1	14 x 1	18 x 1	42.19	143.4	3.39	403.2	383.2	361.4	340.5	319.6	298.7	277.8	256.9
8 x 6 x 1 1/8	14 x 1 1/8	18 x 1 1/8	46.23	157.2	3.42	444.5	421.7	399.0	376.3	353.6	330.9	308.2	285.5
8 x 6 x 1 1/4	14 x 1 1/4	18 x 1 1/4	50.26	170.9	3.45	486.0	461.5	437.1	412.6	388.1	363.7	339.2	314.7
8 x 6 x 1 1/2	14 x 1 1/2	18 x 1 1/2	54.26	184.5	3.48	527.7	501.5	475.3	449.1	422.9	396.7	370.5	344.3
8 x 6 x 1 3/8	14 x 1 3/8	18 x 1 3/8	58.17	197.8	3.51	568.8	540.9	513.1	485.2	457.4	429.6	401.7	373.9
8 x 6 x 1 1/2	14 x 1 1/2	18 x 1 1/2	62.13	211.2	3.54	610.8	581.3	551.8	522.3	492.8	463.3	433.9	404.4
8 x 6 x 1 3/4	14 x 1 3/4	18 x 1 3/4	66.00	224.4	3.57	652.3	621.2	590.2	559.1	528.0	497.0	465.9	434.9
8 x 6 x 2	16 x 1	18 x 1 1/2	69.76	237.2	3.94	729.5	699.8	670.1	640.3	610.6	580.8	551.1	521.4
8 x 6 x 2 1/8	16 x 1 1/8	18 x 1 1/2	77.92	264.9	3.93	813.7	780.4	747.1	713.8	680.5	647.1	613.8	580.5
8 x 6 x 2 1/4	16 x 1 1/4	18 x 1 3/4	86.00	292.4	3.93	898.1	861.3	824.5	787.8	751.0	714.3	677.5	640.7
8 x 6 x 2 1/2	16 x 1 1/2	18 x 2	90.50	307.7	4.00	953.9	915.9	877.9	839.8	801.8	763.8	725.8	687.8
8 x 6 x 2 3/4	16 x 1 3/4	18 x 2 1/4	95.00	323.0	4.06	1008.9	969.6	930.3	891.0	851.7	812.4	773.1	733.7
8 x 6 x 3	16 x 2	18 x 2 1/2	99.50	338.3	4.12	1064.6	1024.0	983.4	942.9	902.3	861.7	821.1	780.6
8 x 6 x 3 1/8	16 x 1 1/8	18 x 2 3/4	104.00	353.6	4.17	1119.3	1077.4	1035.5	993.6	951.8	909.9	868.0	826.1
8 x 6 x 3 1/4	16 x 1 1/4	18 x 3	108.50	368.9	4.22	1174.5	1131.3	1088.1	1044.9	1001.7	958.5	915.3	872.1
8 x 6 x 3 1/2	16 x 1 1/2	18 x 3 1/4	113.00	384.2	4.26	1228.7	1184.1	1139.5	1095.0	1050.4	1005.9	961.3	916.7
8 x 6 x 3 3/4	16 x 1 3/4	18 x 3 1/2	117.50	399.5	4.30	1283.2	1237.3	1191.4	1145.5	1099.6	1053.7	1007.8	961.9

This table continued on next page.

Columns
Continued

Safe Loads in Thousands of Pounds for Plate and Angle Columns, Square Ends

Allowed stresses per square inch.
 14,000 pounds for lengths less than 30 radii.
 16,000—70 $\frac{1}{r}$ for lengths between 30 radii and 150 radii.

Short legs of angles riveted to web plates.
 Column weights do not include rivets.

Size of Angles, Inches	Size of Web Plates, Inches	Size of Cover Plates, Inches	Area of Column, Square Inches	Weight Per Foot of Column, Pounds	Least Radius of Gyration, Inches	LENGTH IN FEET								
						9	10	12	14	16	18	20	22	24
8 x 6 x 1	16 x 1½	18 x 1½	130.00	442.0	4.28	1773.8	1722.8	1671.8	1620.7	1569.7	1518.7	1467.6
8 x 6 x 1	16 x 1½	18 x 1½	134.50	457.3	4.32	1838.2	1785.9	1733.6	1681.3	1629.0	1576.7	1524.4
8 x 6 x 1	16 x 1½	18 x 1½	139.00	472.6	4.35	1901.9	1848.2	1794.5	1740.9	1687.2	1633.5	1579.8
8 x 6 x 1	16 x 1½	18 x 1½	143.50	487.9	4.38	1965.8	1910.7	1855.7	1800.6	1745.6	1690.5	1635.5
8 x 6 x 1	16 x 1½	18 x 2	148.00	503.2	4.41	2029.7	1973.3	1917.0	1860.6	1804.2	1747.8	1691.4
8 x 6 x 1	16 x 1½	18 x 2½	152.50	518.5	4.43	2093.6	2035.2	1977.3	1919.5	1861.7	1803.8	1746.0
8 x 6 x 1	16 x 1½	18 x 2½	157.00	533.8	4.45	2156.4	2097.1	2037.8	1978.6	1919.3	1860.0	1800.8
8 x 6 x 1	16 x 1½	18 x 2½	161.50	549.1	4.48	2220.2	2160.1	2099.5	2038.9	1978.3	1917.8	1857.2
8 x 6 x 1	16 x 1½	18 x 2½	166.00	564.4	4.50	2284.2	2222.2	2160.2	2098.3	2036.3	1974.3	1912.3
8 x 6 x 1	16 x 1½	18 x 2½	170.50	579.7	4.52	2347.8	2284.4	2221.0	2157.7	2094.3	2030.9	1967.5
8 x 6 x 1	16 x 1½	18 x 2½	175.00	595.0	4.54	2411.5	2346.7	2281.9	2217.7	2152.4	2087.7	2022.9
8 x 6 x 1	16 x 1½	18 x 2½	179.50	610.3	4.55	2474.3	2408.1	2341.8	2276.5	2209.7	2142.9	2076.7
8 x 6 x 1	16 x 1½	18 x 3	184.00	625.6	4.57	2538.2	2470.5	2402.9	2335.2	2267.6	2199.9	2132.3

This table continued below.



Size of Angles, Inches	Size of Web Plates, Inches	Size of Cover Plates, Inches	Area of Column, Square Inches	Weight Per Foot of Column, Pounds	Least Radius of Gyration, Inches	LENGTH IN FEET							
						26	28	30	32	34	36	38	40
8 x 6 x 1	16 x 1 1/2	18 x 1 1/2	130.00	442.0	4.28	1416.6	1365.6	1314.6	1263.5	1212.5	1161.4	1110.4	1059.4
8 x 6 x 1	16 x 1 1/2	18 x 1 1/2	134.50	457.3	4.32	1472.1	1419.8	1367.5	1315.2	1262.9	1210.6	1158.3	1106.0
8 x 6 x 1	16 x 1 1/2	18 x 1 1/2	139.00	472.6	4.35	1526.1	1472.5	1418.8	1365.1	1311.4	1257.7	1204.1	1150.4
8 x 6 x 1	16 x 1 1/2	18 x 1 1/2	143.50	487.9	4.38	1580.4	1525.4	1470.3	1415.3	1360.3	1305.2	1250.2	1195.1
8 x 6 x 1	16 x 1 1/2	18 x 2	148.00	503.2	4.41	1635.1	1578.7	1522.3	1465.9	1409.6	1353.2	1296.8	1240.4
8 x 6 x 1	16 x 1 1/2	18 x 2 1/4	152.50	518.5	4.43	1688.1	1630.3	1572.5	1514.6	1456.8	1399.0	1341.1	1283.3
8 x 6 x 1	16 x 1 1/2	18 x 2 1/2	157.00	533.8	4.45	1741.5	1682.2	1623.0	1563.7	1504.4	1445.1	1385.9	1326.6
8 x 6 x 1	16 x 1 1/2	18 x 2 3/4	161.50	549.1	4.48	1796.6	1736.1	1675.5	1614.9	1554.5	1493.8	1433.2	1372.8
8 x 6 x 1	16 x 1 1/2	18 x 3	166.00	564.4	4.50	1850.4	1788.4	1726.4	1664.4	1602.5	1540.5	1478.5	1416.5
8 x 6 x 1	16 x 1 1/2	18 x 3 1/2	170.50	579.7	4.52	1904.2	1840.8	1777.4	1714.0	1650.7	1587.3	1523.9	1460.5
8 x 6 x 1	16 x 1 1/2	18 x 3 3/4	175.00	595.0	4.54	1958.2	1893.4	1828.7	1763.9	1699.2	1634.4	1569.7	1504.9
8 x 6 x 1	16 x 1 1/2	18 x 4	179.50	610.3	4.55	2010.4	1944.1	1877.8	1811.5	1745.3	1679.0	1612.7	1546.4
8 x 6 x 1	16 x 1 1/2	18 x 4 1/2	184.00	625.6	4.57	2064.6	1997.0	1929.4	1861.7	1794.1	1726.4	1658.8	1591.1

Columns

Continued

Allowed stresses per square inch.

14,000 pounds for lengths less than 30 radii.

16,000—70 $\frac{1}{r}$ for lengths between 30 radii and 150 radii.

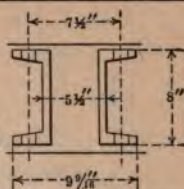
Size of Channels	Size of Plates	Area, Square Inches	Weight per Linear Foot, Pounds	Least Radius of Gyration, Inches	LENGTH IN FEET				
					8	9	10	12	14
2-8"—11 $\frac{1}{4}$ lbs.	Lattice	6.70	29.5	3.11	92.7	90.9	89.1	85.5	81.9
	2-10x $\frac{1}{4}$	11.70	39.5	3.05	161.4	158.2	154.9	148.5	142.1
	2-10x $\frac{3}{8}$	12.95	43.8	3.04	178.6	175.0	171.4	164.3	157.1
	2-10x $\frac{1}{2}$	14.20	48.0	3.02	195.6	191.7	187.7	179.8	171.9
	2-10x $\frac{3}{4}$	15.45	52.3	3.01	212.7	208.4	204.1	195.5	186.8
	2-10x $\frac{1}{2}$	16.70	56.5	3.00	229.8	225.2	220.5	211.1	201.8
	2-10x $\frac{3}{8}$	17.95	60.8	2.99	246.9	241.8	236.8	226.7	216.6
	2-10x $\frac{1}{4}$	19.20	65.0	2.99	264.1	258.7	253.3	242.5	231.7
2-8"—13 $\frac{3}{4}$ lbs.	Lattice	8.08	34.5	2.98	111.1	108.8	106.5	102.0	97.4
	2-10x $\frac{1}{4}$	13.08	44.5	3.00	180.0	176.3	172.7	165.3	158.0
	2-10x $\frac{3}{8}$	14.33	48.8	2.99	197.1	193.0	189.0	181.0	172.9
	2-10x $\frac{1}{2}$	15.58	53.0	2.98	214.2	209.8	205.4	196.6	187.8
	2-10x $\frac{3}{4}$	16.83	57.3	2.97	231.2	226.4	221.7	212.2	202.6
	2-10x $\frac{1}{2}$	18.08	61.5	2.97	248.4	243.3	238.1	227.9	217.7
	2-10x $\frac{3}{8}$	19.33	65.8	2.96	265.4	259.9	254.4	243.5	232.5
	2-10x $\frac{1}{4}$	20.58	70.0	2.96	282.6	276.7	270.9	259.2	247.5
2-8"—16 $\frac{1}{4}$ lbs.	Lattice	9.56	39.5	2.89	130.7	128.0	125.2	119.6	114.1
	2-10x $\frac{3}{8}$	17.06	58.0	2.93	233.8	228.9	224.1	214.3	204.5
	2-10x $\frac{1}{2}$	18.31	62.3	2.93	251.0	245.7	240.5	230.0	219.5
	2-10x $\frac{3}{4}$	19.56	66.5	2.93	268.1	262.5	256.9	245.7	234.5
	2-10x $\frac{1}{2}$	20.81	70.8	2.93	285.2	279.3	273.3	261.4	249.4
	2-10x $\frac{3}{8}$	22.06	75.0	2.92	302.2	295.9	289.5	276.8	264.7
	2-10x $\frac{1}{4}$	23.31	79.3	2.92	319.3	312.6	305.9	292.5	279.7
	2-10x $\frac{3}{4}$	24.56	83.5	2.92	336.4	329.4	322.3	308.2	294.1
2-8"—18 $\frac{3}{4}$ lbs.	Lattice	11.02	44.5	2.82	150.1	146.8	143.5	136.9	130.4
	2-10x $\frac{3}{8}$	18.52	63.0	2.89	253.3	247.9	242.5	231.7	221.0
	2-10x $\frac{1}{2}$	21.02	71.5	2.89	287.4	281.3	275.2	263.0	250.8
	2-10x $\frac{3}{4}$	23.52	80.0	2.89	321.6	314.8	308.0	294.3	280.6
	2-10x $\frac{1}{4}$	26.02	88.5	2.89	355.8	348.3	340.7	325.6	310.4
2-8"—21 $\frac{1}{4}$ lbs.	Lattice	12.50	49.5	2.77	169.7	165.9	162.1	154.5	146.9
	2-10x $\frac{3}{8}$	20.00	68.0	2.84	272.7	266.8	260.8	249.0	237.2
	2-10x $\frac{1}{2}$	22.50	76.5	2.84	306.8	300.1	293.5	280.1	266.8
	2-10x $\frac{3}{4}$	25.00	85.0	2.85	341.1	333.7	326.3	311.6	296.9
	2-10x $\frac{1}{4}$	27.50	93.5	2.85	375.2	367.1	359.0	342.8	326.6
	2-10x $\frac{3}{8}$	30.00	102.0	2.86	409.5	400.7	391.9	374.3	356.7

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JONES & LAUGHLIN STEEL COMPANY

Safe Loads in Thousands of Pounds For 2-8" Channel Columns, Square Ends

Section 2-8" Channels laced with $1\frac{3}{4} \times \frac{5}{16}$ " Bars or 2-8" Channels and 2-10" Plates. Holes $\frac{1}{2}$ "; Rivets $\frac{3}{4}$ " diameter.
Column weights do not include Rivets.



LENGTH IN FEET

16	18	20	22	24	26	28	30	32	34	36	38	40
78.2	74.6	71.0	67.4	63.8	60.2	56.5	52.9	49.3	45.7	42.1	38.4
135.6	129.2	122.7	116.3	109.8	103.4	96.9	90.5	84.0	77.6	71.1	64.7
150.0	142.8	135.6	128.5	121.3	114.2	107.0	99.9	92.7	85.5	78.4	71.2
164.0	156.1	148.2	140.3	132.4	124.5	116.6	108.7	100.8	92.9	85.0
178.2	169.6	161.0	152.3	143.7	135.1	126.5	117.9	109.2	100.6	92.0
192.4	183.1	173.7	164.4	155.0	145.6	136.3	127.0	117.6	108.3	98.9
206.5	196.4	186.3	176.3	166.2	156.1	146.0	135.9	125.8	115.7	105.7
220.9	210.1	199.3	188.5	177.7	167.0	156.2	145.4	134.6	123.8	113.0
.....
92.8	88.3	83.7	79.2	74.6	70.1	65.5	61.0	56.4	51.8	47.3
150.7	143.4	136.0	128.7	121.4	114.1	106.7	99.4	92.1	84.8	77.4
164.9	156.8	148.8	140.7	132.7	124.6	116.6	108.5	100.5	92.4	84.4
179.0	170.2	161.5	152.7	143.9	135.1	126.3	117.5	108.8	100.0	91.2
193.1	183.6	174.1	164.6	155.0	145.5	136.0	126.5	117.0	107.4	97.9
207.5	197.2	187.0	176.8	166.6	156.3	146.1	135.9	125.7	115.4	105.2
221.5	210.5	199.6	188.6	177.6	166.7	155.7	144.7	133.8	122.8	111.8
235.8	224.2	212.5	200.8	189.1	177.4	165.8	154.1	142.4	130.7	119.0
.....
108.5	102.9	97.4	91.8	86.3	80.7	75.2	69.6	64.0	58.5	52.9
194.7	184.9	175.1	165.4	155.6	145.8	136.0	126.2	116.5	106.7	96.9
209.0	198.5	188.0	177.5	167.0	156.5	146.0	135.5	125.0	114.5	104.0
223.2	212.0	200.8	189.6	178.4	167.2	155.9	144.7	133.5	122.3	111.1
237.5	225.6	213.6	201.7	189.8	177.8	165.9	154.0	142.0	130.1	118.2
251.4	238.7	226.0	213.4	200.7	188.0	175.3	162.6	150.0	137.2	124.5
265.7	252.3	238.9	225.4	212.0	198.6	185.2	171.8	158.4	145.0	131.6
279.9	265.8	251.7	237.5	223.4	209.3	195.1	181.0	166.9	152.8	138.6
.....
123.8	117.2	110.7	104.1	97.5	91.0	84.4	77.8	71.3	64.7
210.2	199.4	188.7	177.9	167.1	156.4	145.6	134.8	124.1	113.3	102.5
238.6	226.3	214.1	201.9	189.7	177.5	165.3	153.0	140.8	128.6	116.4
266.9	253.3	239.6	225.9	212.2	198.6	184.9	171.2	157.6	143.9	130.2
295.3	280.2	265.1	249.9	234.8	219.7	204.6	189.4	174.3	159.2	144.1
.....
139.4	131.8	124.2	116.6	109.0	101.5	93.9	86.3	78.7	71.1
225.4	213.5	201.7	189.9	178.0	166.2	154.4	142.5	130.7	118.9
253.5	240.2	226.9	213.6	200.3	187.0	173.7	160.4	147.0	133.7
282.1	267.4	252.7	237.9	223.2	208.4	193.7	179.0	164.2	149.5
310.3	294.1	277.9	261.7	245.5	229.3	213.1	196.9	180.6	164.4
339.0	321.4	303.8	286.2	268.5	250.9	233.3	215.7	198.1	180.4

Columns

Continued

Allowed stresses per square inch.

14,000 pounds for lengths less than 30 radii.

16,000—70 $\frac{1}{r}$ for lengths between 30 radii and 150 radii.

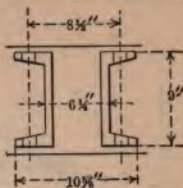
Size of Channels	Size of Plates	Area, Square Inches	Weight per Linear Foot, Pounds	Least Radius of Gyration, Inches	LENGTH IN FEET				
					8	9	10	12	14
2-9"—13½ lbs.	Lattice	7.78	34.3	3.49	107.6	105.8	102.0	98.3
	2-11x¼	13.28	45.2	3.41	183.0	179.7	173.2	166.7
	2-11x⅝	14.66	49.9	3.39	201.9	198.2	191.0	183.7
	2-11x¾	16.03	54.6	3.37	220.5	216.5	208.5	200.5
	2-11x⅞	17.41	59.2	3.35	239.3	234.9	226.2	217.4
	2-11x1	18.78	63.9	3.34	258.0	253.3	243.8	234.4
	2-11x1⅛	20.16	68.6	3.33	276.8	271.7	261.5	251.4
	2-11x1¼	21.53	73.3	3.32	295.5	290.0	279.1	268.2
2-9"—15 lbs.	Lattice	8.82	37.8	3.40	121.5	119.3	115.0	110.6
	2-11x¼	14.32	48.7	3.37	197.0	193.4	186.3	179.2
	2-11x⅝	15.70	53.4	3.36	215.9	212.0	204.1	196.3
	2-11x¾	17.07	58.1	3.34	234.5	230.2	221.6	213.0
	2-11x⅞	18.45	62.7	3.33	253.3	248.7	239.4	230.0
	2-11x1	19.82	67.4	3.32	272.0	267.0	256.9	246.9
	2-11x1⅛	21.20	72.1	3.31	290.8	285.4	274.7	263.9
	2-11x1¼	22.57	76.8	3.30	309.4	303.7	292.2	280.7
2-9"—20 lbs.	Lattice	11.76	47.8	3.21	160.5	157.4	151.2	145.1
	2-11x⅝	18.64	63.4	3.27	255.2	250.4	240.8	231.2
	2-11x¾	20.01	68.1	3.26	273.8	268.6	258.3	248.0
	2-11x⅞	21.39	72.7	3.26	292.6	287.1	276.1	265.1
	2-11x1	22.76	77.4	3.25	311.2	305.3	293.6	281.8
	2-11x1⅛	24.14	82.1	3.25	330.1	323.8	311.4	298.9
	2-11x1¼	25.51	86.8	3.24	348.6	342.0	328.8	315.6
	2-11x1½	26.89	91.4	3.24	367.5	360.5	346.6	332.6
2-9"—25 lbs.	Lattice	14.70	57.8	3.10	203.3	199.4	195.4	179.4
	2-11x¾	22.95	78.1	3.18	318.7	312.6	306.6	282.3
	2-11x1	24.33	82.7	3.18	337.9	331.4	325.0	312.2
	2-11x1⅛	25.70	87.4	3.18	356.9	350.1	343.3	329.7
	2-11x1¼	27.08	92.1	3.18	376.1	368.9	361.7	347.4
	2-11x1½	28.45	96.8	3.18	395.1	387.6	380.1	365.0
	2-11x1¾	29.83	101.4	3.18	414.2	406.4	398.5	382.7
	2-11x2	31.20	106.1	3.18	433.3	425.0	416.8	400.3
2-9"—25 lbs.	2-11x1⅞	32.58	110.8	3.18	452.4	443.8	435.2	418.0
	2-11x2	33.95	115.5	3.18	471.5	462.5	453.5	435.6
	2-11x2¼	35.33	120.1	3.18	490.6	481.3	472.0	453.3
	2-11x2½	36.70	124.8	3.18	509.7	499.9	490.0	467.0

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JONES & LAUGHLIN STEEL COMPANY

Safe Loads in Thousands of Pounds For 9" Channel Columns, Square Ends

Section 2-9" Channels laced with 2"x $\frac{1}{4}$ " Bars or 2-9"
Channels and 2-11" Plates. Holes $\frac{1}{8}$ "; Rivets $\frac{3}{4}$ " diameter.
Column weights do not include Rivets.



LENGTH IN FEET

16	18	20	22	24	26	28	30	32	34	36	38	40
94.5	90.8	87.0	83.3	79.5	75.8	72.1	68.3	64.6	60.8	57.1	53.3	49.6
160.1	153.6	147.0	140.5	134.0	127.4	120.9	114.3	107.8	101.3	94.7	88.2	81.6
176.4	169.2	161.9	154.6	147.4	140.1	132.8	125.6	118.3	111.1	103.8	96.5	89.3
192.6	184.6	176.6	168.6	160.6	152.6	144.6	136.6	128.6	120.6	112.6	104.7	96.7
208.7	200.0	191.3	182.5	173.8	165.1	156.3	147.6	138.9	130.1	121.4	112.7	103.9
224.9	215.5	206.0	196.6	187.1	177.7	168.2	158.8	149.3	139.9	130.5	121.0	111.6
241.2	231.0	220.9	210.7	200.5	190.3	180.2	170.0	159.8	149.7	139.5	129.3	119.1
257.3	246.4	235.5	224.6	213.7	202.9	192.0	181.1	170.2	159.3	148.4	137.5	126.6
106.3	101.9	97.5	93.2	88.8	84.5	80.1	75.8	71.4	67.0	62.7	58.3	54.0
172.0	164.9	157.7	150.6	143.5	136.3	129.2	122.0	114.9	107.8	100.6	93.5	86.3
188.4	180.6	172.7	164.9	157.0	149.2	141.3	133.5	125.6	117.8	109.9	102.1	94.2
204.4	195.9	187.3	178.7	170.1	161.5	152.9	144.3	135.7	127.2	118.6	110.0	101.4
220.8	211.4	202.1	192.8	183.5	174.2	164.9	155.6	146.3	137.0	127.7	118.4	109.0
236.9	226.9	216.8	206.8	196.8	186.7	176.7	166.7	156.7	146.6	136.6	126.6	116.5
253.1	242.4	231.6	220.8	210.1	199.3	188.6	177.8	167.0	156.3	145.5	134.8	124.0
269.2	257.7	246.2	234.7	223.2	211.8	200.3	188.8	177.3	165.8	154.3	142.8	131.3
138.9	132.8	126.6	120.5	114.3	108.2	102.0	95.8	89.7	83.5	77.4	71.2	65.1
221.6	212.1	202.5	192.9	183.3	173.8	164.2	154.6	145.0	135.5	125.9	116.3	106.7
237.7	227.4	217.1	206.7	196.4	186.1	175.8	165.5	155.2	144.9	134.6	124.2	113.9
254.1	243.0	232.0	221.0	210.0	199.0	187.9	176.9	165.9	154.9	143.8	132.8	121.8
270.0	258.3	246.5	234.7	223.0	211.2	199.5	187.7	175.9	164.2	152.4	140.6	128.9
286.4	273.9	261.5	249.0	236.5	224.0	211.5	199.1	186.6	174.1	161.6	149.2	136.7
302.3	289.1	275.9	262.7	249.4	236.2	223.0	209.8	196.5	183.3	170.1	156.9	143.6
318.7	304.8	290.8	276.9	262.9	249.0	235.0	221.1	207.2	193.2	179.3	165.3	151.4
334.9	320.3	305.6	291.0	276.3	261.7	247.0	232.4	217.7	203.1	188.4	173.8	159.1
171.5	163.5	155.5	147.6	139.6	131.6	123.7	115.7	107.7	99.8	91.8	83.8
270.2	258.1	246.0	233.8	221.7	209.6	197.5	185.3	173.2	161.1	149.0	136.8
286.4	273.6	260.7	247.9	235.0	222.2	209.3	196.5	183.6	170.7	157.9	145.1
302.6	289.0	275.4	261.8	248.3	234.7	221.1	207.5	194.0	180.4	166.8	153.2
318.8	304.5	290.2	275.9	261.6	247.3	233.0	218.7	204.4	190.1	175.8	161.4
335.0	319.9	304.9	289.9	274.8	259.8	244.8	229.7	214.7	199.7	184.6	169.6
351.2	335.4	319.7	303.9	288.2	272.4	256.6	240.9	225.1	209.4	193.6	177.8
367.3	350.8	334.4	317.9	301.4	284.9	268.4	251.9	235.5	219.0	202.5	186.0
383.6	366.4	349.2	331.9	314.7	297.5	280.3	263.1	245.9	228.7	211.5	194.2
399.7	381.8	363.8	345.9	328.0	310.0	292.1	274.2	256.2	238.3	220.3	202.4
416.0	397.3	378.6	360.0	341.3	322.6	304.0	285.3	266.6	248.0	229.3	210.6

JONES & LAUGHLIN STEEL COMPANY

Columns Continued

Allowed stresses per square inch.
14,000 pounds for lengths less than 30 radii.
 $16,000 - 70 \frac{1}{r}$ for lengths between 30 radii and 150 radii.

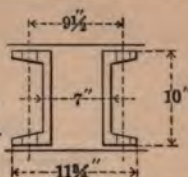
Size of Channels	Size of Plates	Area, Square Inches	Weight per Linear Foot, Pounds	Least Radius of Gyration, Inches	LENGTH IN FEET				
					9	10	12	14	16
2-10"—15 lbs.	Lattice	8.92	37.8	3.87	123.4	119.5	115.6	111.7
	2-12x $\frac{1}{4}$	14.92	50.4	3.77	205.5	198.8	192.2	185.5
	2-12x $\frac{3}{8}$	16.42	55.5	3.74	225.8	218.5	211.1	203.7
	2-12x $\frac{1}{2}$	17.92	60.6	3.72	246.3	238.2	230.1	222.0
	2-12x $\frac{3}{4}$	19.42	65.7	3.70	266.6	257.8	249.0	240.2
	2-12x $\frac{1}{2}$	20.92	70.8	3.68	287.0	277.4	267.9	258.3
	2-12x $\frac{3}{8}$	22.42	75.9	3.67	307.4	297.2	286.9	276.6
	2-12x $\frac{1}{4}$	23.92	81.0	3.66	327.8	316.9	305.9	294.9
2-10"—20 lbs.	Lattice	11.76	47.8	3.66	161.2	155.8	150.4	145.0
	2-12x $\frac{3}{8}$	20.76	60.6	3.65	284.4	274.8	265.3	255.7
	2-12x $\frac{1}{2}$	22.26	75.7	3.64	304.8	294.5	284.2	274.0
	2-12x $\frac{3}{4}$	23.76	80.8	3.63	325.2	314.2	303.2	292.2
	2-12x $\frac{1}{2}$	25.26	85.9	3.62	345.6	333.8	322.1	310.4
	2-12x $\frac{3}{8}$	26.76	91.0	3.61	365.9	353.4	341.0	328.5
	2-12x $\frac{1}{4}$	28.26	96.1	3.60	386.2	373.0	359.9	346.7
	2-12x $\frac{3}{4}$	29.76	101.2	3.60	406.7	392.8	379.0	365.1
2-10"—25 lbs.	Lattice	14.70	57.8	3.52	203.6	200.1	193.1	186.1	179.1
	2-12x $\frac{1}{2}$	26.70	90.8	3.57	370.7	364.4	351.8	339.2	326.7
	2-12x $\frac{3}{8}$	28.20	95.9	3.57	391.5	384.8	371.6	358.3	345.0
	2-12x $\frac{1}{4}$	29.70	101.0	3.56	412.1	405.1	391.1	377.1	363.1
	2-12x $\frac{3}{4}$	31.20	106.1	3.56	433.0	425.6	410.9	396.2	381.4
	2-12x $\frac{1}{2}$	32.70	111.2	3.55	453.6	445.8	430.4	414.9	399.4
	2-12x $\frac{3}{8}$	34.20	116.3	3.55	474.4	466.3	450.1	434.0	417.7
	2-12x $\frac{1}{4}$	35.70	121.4	3.54	494.9	486.5	469.5	452.6	435.7
2-10"—30 lbs.	Lattice	17.64	67.8	3.42	243.2	238.9	230.2	221.6	212.9
	2-12x $\frac{3}{8}$	32.64	111.0	3.50	451.7	443.9	428.2	412.6	396.9
	2-12x $\frac{1}{2}$	35.64	121.2	3.50	493.3	484.7	467.6	450.5	433.4
	2-12x $\frac{3}{4}$	38.64	131.4	3.50	534.8	525.5	507.0	488.4	469.9
	2-12x $\frac{1}{4}$	41.64	141.6	3.49	576.0	566.0	546.0	525.9	505.9
	2-12x $\frac{3}{8}$	44.64	151.8	3.48	617.1	606.1	585.1	564.0	543.0
2-10"—35 lbs.	Lattice	20.58	77.8	3.35	282.8	277.7	267.4	257.0	246.7
	2-12x $\frac{3}{8}$	35.58	121.0	3.45	491.3	482.6	465.3	448.0	430.7
	2-12x $\frac{1}{2}$	38.58	131.2	3.45	532.7	523.3	504.6	485.8	467.0
	2-12x $\frac{3}{4}$	41.58	141.4	3.45	574.2	564.0	543.8	523.6	503.3
	2-12x $\frac{1}{4}$	44.58	151.6	3.45	615.6	604.7	583.0	561.3	539.6
	2-12x $\frac{3}{8}$	47.58	161.8	3.45	657.0	645.4	622.3	599.1	575.9

This table continued on next page.

JONES & LAUGHLIN STEEL COMPANY

Safe Loads in Thousands of Pounds For 10" Channel Columns, Square Ends

Section 2-10" Channels laced with 2"x $\frac{5}{16}$ " Bars or 2-10" Channels and 2-12" Plates. Holes $\frac{1}{4}$ "; Rivets $\frac{3}{4}$ " diameter.
Column weights do not include Rivets.



LENGTH IN FEET

18	20	22	24	26	28	30	32	34	36	38	40	
107.9	104.0	100.1	96.3	92.4	88.5	84.6	80.8	76.9	73.0	69.1	65.3
178.9	172.2	165.6	158.9	152.3	145.6	139.0	132.3	125.7	119.0	112.4	105.7
196.3	189.0	181.6	174.2	166.8	159.5	152.1	144.7	137.3	130.0	122.6	115.2
213.9	205.8	197.7	189.6	181.5	173.4	165.3	157.2	149.1	141.1	133.0	124.9
231.4	222.5	213.7	204.9	196.1	187.3	178.5	169.6	160.8	152.0	143.2	134.4
248.8	239.2	229.7	220.1	210.6	201.0	191.5	181.9	172.4	162.8	153.3	143.7
266.4	256.1	245.8	235.6	225.3	215.0	204.8	194.5	184.3	174.0	163.7	153.5
283.9	272.9	262.0	251.0	240.0	229.0	218.0	207.1	196.1	185.1	174.1	163.1
139.6	134.2	128.8	123.4	118.0	112.6	107.2	101.8	96.4	91.0	85.6	80.2
246.2	236.6	227.1	217.5	207.9	198.4	188.8	179.3	169.7	160.2	150.6	141.1
263.7	253.4	243.1	232.9	222.6	212.3	202.1	191.8	181.5	171.2	161.0	150.7
281.2	270.2	259.2	248.2	237.2	226.2	215.2	204.2	193.2	182.2	171.2	160.2
298.7	286.9	275.2	263.5	251.8	240.0	228.3	216.6	204.9	193.2	181.4	169.7
316.1	303.6	291.2	278.7	266.3	253.8	241.4	228.9	216.5	204.0	191.6	179.1
333.5	320.3	307.1	293.9	280.7	267.5	254.3	241.2	228.0	214.8	201.6	188.4
351.2	337.3	323.4	309.5	295.6	281.7	267.8	254.0	240.1	226.2	212.3	198.4
172.1	165.0	158.0	151.0	144.0	137.0	130.0	122.9	115.9	108.9	101.9	94.9
314.1	301.6	289.0	276.4	263.9	251.3	238.7	226.2	213.6	201.0	188.5	175.9
331.8	318.5	305.2	292.0	278.7	265.4	252.1	238.9	225.6	212.3	199.1	185.8
349.1	335.1	321.1	307.0	293.0	279.0	265.0	251.0	237.0	223.0	209.0	194.9
366.7	352.0	337.3	322.6	307.8	293.1	278.4	263.7	249.0	234.2	219.5	204.8
383.9	368.5	353.0	337.5	322.0	306.6	291.1	275.6	260.1	244.7	229.2	213.7
401.5	385.4	369.2	353.0	336.8	320.6	304.4	288.3	272.1	255.9	239.7	223.5
418.7	401.8	384.8	367.9	350.9	334.0	317.1	300.1	283.2	266.2	249.3	232.3
204.2	195.6	186.9	178.2	169.6	160.9	152.2	143.5	134.9	126.2	117.5	108.9
381.2	365.6	349.9	334.2	318.6	302.9	287.2	271.6	255.9	240.2	224.6	208.9
416.3	399.2	382.1	365.0	347.8	330.7	313.6	296.5	279.4	262.3	245.2	228.1
451.3	432.8	414.2	395.7	377.1	358.6	340.0	321.5	302.9	284.4	265.8	247.3
485.8	465.8	445.7	425.7	405.7	385.6	365.6	345.5	325.5	305.4	285.4	265.4
236.4	226.1	215.8	205.4	195.1	184.8	174.5	164.1	153.8	143.5	133.2	122.9
413.3	396.0	378.7	361.4	344.0	326.7	309.4	292.1	274.7	257.4	240.1	222.8
448.2	429.4	410.6	391.8	373.1	354.3	335.5	316.7	297.9	279.1	260.3	241.5
483.1	462.8	442.6	422.3	402.1	381.8	361.6	341.3	321.1	300.8	280.6	260.3
517.9	496.2	474.5	452.8	431.0	409.4	387.7	365.9	344.2	322.5	300.8	279.1
552.8	529.6	506.4	483.2	460.1	436.9	413.8	390.6	367.4	344.2	321.1	297.9

JONES & LAUGHLIN STEEL COMPANY

Columns Continued

Allowed stresses per square inch.
14,000 pounds for lengths less than 30 radii.
16,000—70 $\frac{1}{r}$ for lengths between 30 radii and 150 radii.

Size of Channels	Size of Plates	Area, Square Inches	Weight per Linear Foot, Pounds	Least Radius of Gyration, Inches	LENGTH IN FEET			
					12	14	16	18
2-12"—20½ lbs.	Lattice	12.06	48.8	4.61	166.6	162.2	157.8	153.4
	2-14x½	20.81	70.8	4.39	285.2	277.2	269.3	261.3
	2-14x¾	22.56	76.7	4.36	308.8	300.1	291.4	282.7
	2-14x1	24.31	82.7	4.34	332.5	323.1	313.7	304.3
	2-14x1½	26.06	88.6	4.32	356.2	346.0	335.9	325.8
	2-14x1¾	27.81	94.6	4.30	379.8	368.9	358.0	347.2
	2-14x2	29.56	100.5	4.29	403.5	391.9	380.4	368.8
	2-14x2½	31.31	106.5	4.28	427.2	414.9	402.6	390.3
2-12"—25 lbs.	Lattice	14.70	57.8	4.43	201.8	196.2	190.6	185.0
	2-14x¾	25.20	85.7	4.30	344.1	334.3	324.4	314.6
	2-14x1	26.95	91.7	4.29	367.9	357.3	346.8	336.2
	2-14x1½	28.70	97.6	4.27	391.5	380.2	368.9	357.6
	2-14x1¾	30.45	103.6	4.26	415.2	403.1	391.1	379.1
	2-14x2	32.20	109.5	4.25	438.8	426.1	413.4	400.6
	2-14x2½	33.95	115.5	4.24	462.5	449.0	435.6	422.1
	2-14x3	35.70	121.4	4.23	486.1	471.9	457.8	443.6
2-12"—30 lbs.	Lattice	17.64	67.8	4.28	240.7	233.8	226.8	219.9
	2-14x1½	31.64	107.6	4.22	430.7	418.1	405.5	392.9
	2-14x2	35.14	119.5	4.20	477.9	463.8	449.8	435.7
	2-14x2½	38.64	131.4	4.19	525.3	509.8	494.3	478.8
	2-14x3	42.14	143.3	4.18	572.6	555.7	538.7	521.8
	2-14x3½	45.64	155.2	4.17	619.9	601.5	583.2	564.8
	Lattice	20.58	77.8	4.17	279.5	271.2	263.0	254.7
	2-14x2½	38.08	129.5	4.16	517.0	501.6	486.3	470.9
2-12"—35 lbs.	Lattice	41.58	141.4	4.15	564.3	547.5	530.6	513.8
	2-14x3	45.08	153.3	4.14	611.5	593.2	574.9	556.6
	2-14x3½	48.58	165.2	4.13	658.7	639.0	619.2	599.4
	Lattice	23.52	87.8	4.09	318.4	308.7	299.0	289.4
	2-14x3½	44.52	151.4	4.10	602.9	584.6	566.4	548.1
	2-14x4	48.02	163.3	4.10	650.3	630.6	610.9	591.2
	2-14x1	51.52	175.2	4.10	697.7	676.5	655.4	634.3
	2-14x1½	55.02	187.1	4.09	744.7	722.1	699.5	676.9
2-12"—40 lbs.	Lattice	58.52	199.0	4.09	792.1	768.1	744.0	720.0

This table continued on next page.

JONES & LAUGHLIN STEEL COMPANY

Columns Continued

Allowed stresses per square inch.
14,000 pounds for lengths less than 30 radii.

16,000—70 $\frac{1}{r}$ for lengths between 30 radii and 150 radii.

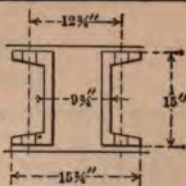
Size of Channels	Size of Plates	Area, Square Inches	Weight per Linear Foot, Pounds	Least Radius of Gyration, Inches	LENGTH IN FEET			
					12	14	16	18
2-15"—33 lbs.	Lattice	19.80	76.0	5.35	273.3	267.1	260.9	
	2-16x $\frac{3}{8}$	31.80	106.8	5.08	435.2	424.7	414.1	
	2-16x $\frac{7}{8}$	33.80	113.6	5.06	462.3	451.0	439.8	
	2-16x $\frac{1}{2}$	35.80	120.4	5.03	489.1	477.1	465.2	
	2-16x $\frac{3}{4}$	37.80	127.2	5.01	516.1	503.4	492.7	
	2-16x $\frac{5}{8}$	39.80	134.0	4.99	543.1	529.6	516.2	
	2-16x $\frac{1}{4}$	41.80	140.8	4.98	570.0	556.0	541.9	
	2-16x $\frac{3}{4}$	43.80	147.6	4.96	597.0	582.1	567.3	
	2-16x $\frac{1}{2}$	45.80	154.4	4.95	624.0	608.5	592.9	
	2-16x $\frac{3}{8}$	47.80	161.2	4.93	650.8	634.5	618.2	
	2-16x1	51.80	174.8	4.91	704.7	687.0	669.3	
2-15"—35 lbs.	Lattice	20.58	80.0	5.32	283.8	277.3	270.8	
	2-16x $\frac{3}{8}$	32.58	110.8	5.07	445.8	434.9	424.1	
	2-16x $\frac{1}{2}$	36.58	124.4	5.02	499.6	487.3	475.1	
	2-16x $\frac{3}{4}$	40.58	138.0	4.98	553.4	539.8	526.1	
	2-16x $\frac{5}{8}$	44.58	151.6	4.95	607.4	592.3	577.1	
	2-16x $\frac{1}{4}$	48.58	165.2	4.93	661.4	644.8	628.2	
	2-16x1	52.58	178.8	4.90	715.1	697.2	679.0	
2-15"—40 lbs.	Lattice	23.52	90.0	5.21	323.3	315.6	308.1	
	2-16x $\frac{1}{2}$	39.52	134.4	4.98	538.9	525.7	512.4	
	2-16x $\frac{3}{4}$	47.52	161.6	4.92	646.7	630.5	614.3	
	2-16x1	55.52	188.8	4.88	754.5	735.4	716.3	
	2-16x1 $\frac{1}{4}$	63.52	216.0	4.85	862.3	840.3	818.3	
	2-16x1 $\frac{1}{2}$	71.52	243.2	4.82	969.8	944.9	920.0	
2-15"—45 lbs.	Lattice	26.48	100.0	5.12	362.9	354.2	345.5	
	2-16x $\frac{1}{2}$	42.48	144.4	4.94	578.5	564.1	549.7	
	2-16x $\frac{3}{4}$	50.48	171.6	4.89	686.3	668.9	651.6	
	2-16x1	58.48	198.8	4.85	793.8	773.6	753.3	
	2-16x1 $\frac{1}{4}$	66.48	226.0	4.82	901.5	878.3	855.1	
	2-16x1 $\frac{1}{2}$	74.48	253.2	4.80	1035.2	1009.2	983.1	957.1
2-15"—50 lbs.	Lattice	29.42	110.0	5.03	401.9	392.1	382.3	
	2-16x $\frac{3}{4}$	53.42	181.6	4.85	725.2	706.7	688.2	
	2-16x1	61.42	208.8	4.82	832.9	811.5	790.1	
	2-16x1 $\frac{1}{4}$	69.42	236.0	4.80	965.0	940.7	916.3	892.0
	2-16x1 $\frac{1}{2}$	77.42	263.2	4.78	1075.5	1048.3	1021.1	993.8
2-15"—55 lbs.	Lattice	32.36	120.0	4.96	441.0	430.1	419.1	
	2-16x $\frac{3}{4}$	56.36	191.6	4.82	764.2	744.6	724.9	
	2-16x1	64.36	218.8	4.80	894.6	872.0	849.5	827.0
	2-16x1 $\frac{1}{4}$	72.36	246.0	4.78	1005.2	979.7	954.3	928.9
	2-16x1 $\frac{1}{2}$	80.36	273.2	4.76	1115.6	1087.3	1050.9	1030.5

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JONES & LAUGHLIN STEEL COMPANY

Safe Loads in Thousands of Pounds For 15" Channel Columns, Square Ends

Section 2-15" Channels laced with $2\frac{1}{4}" \times \frac{3}{8}"$ Bars or 2-15"
Channels and 2-16" Plates. Holes $\frac{1}{4}"$; Rivets $\frac{3}{4}"$ diameter.
Column weights do not include rivets.



LENGTH IN FEET

20	22	24	26	28	30	32	34	36	38	40
254.6	248.4	242.2	236.0	229.8	223.5	217.4	211.1	204.9	198.6	192.5
403.6	393.1	382.6	372.0	361.6	351.0	340.5	330.0	319.5	309.0	298.5
428.6	417.4	406.1	394.9	383.7	372.5	361.2	350.0	338.8	327.6	316.4
453.2	441.3	429.3	417.4	405.4	393.4	381.5	369.5	357.6	345.6	333.7
478.0	465.4	452.7	440.0	427.3	414.7	402.0	389.3	376.6	364.0	351.3
502.8	489.4	476.0	462.6	449.2	435.8	422.4	409.0	395.6	382.2	368.7
527.8	513.7	499.6	485.5	471.4	457.3	443.0	428.9	415.0	400.9	386.7
552.4	537.6	522.8	507.9	493.1	478.3	463.4	448.6	433.8	418.9	404.1
577.4	561.8	546.3	530.7	515.2	499.7	484.1	468.6	453.0	437.5	421.9
601.9	585.6	569.4	553.1	536.8	520.5	504.2	487.9	471.6	455.3	439.0
651.6	633.8	616.1	598.4	580.7	562.9	545.2	527.5	509.8	492.1	474.3
264.3	257.8	251.3	244.8	238.3	231.8	225.3	218.8	212.3	205.8	199.3
413.3	402.5	391.7	380.9	370.1	359.3	348.6	337.8	327.0	316.2	305.3
462.9	450.6	438.4	426.1	413.9	401.7	389.4	377.1	364.9	352.7	340.4
512.4	498.7	485.0	471.3	457.6	443.9	430.3	416.6	402.9	389.2	375.4
562.0	546.9	531.7	516.6	501.5	486.4	471.2	456.1	441.0	425.8	410.7
611.7	595.1	578.6	562.0	545.5	528.9	512.4	495.8	479.3	462.7	446.2
661.1	643.1	625.0	607.0	588.9	570.9	552.9	534.9	516.8	498.8	480.6
300.5	292.9	285.3	277.7	270.1	262.6	254.9	247.4	239.8	232.2	224.7
499.0	485.7	472.3	459.0	445.7	432.3	419.0	405.7	392.3	379.0	365.6
598.1	581.9	565.6	549.4	533.2	517.0	500.8	484.5	468.3	452.1	435.8
697.2	678.1	659.0	639.8	620.7	601.6	582.5	563.4	544.3	525.2	506.0
796.3	774.3	752.3	730.3	708.3	686.3	664.3	642.3	620.3	598.3	576.3
895.0	870.1	845.2	820.2	795.3	770.4	745.5	720.5	695.6	670.7	645.8
336.8	328.1	319.4	310.7	302.0	293.4	284.7	276.0	267.3	258.6	250.0
535.2	520.8	506.3	491.9	477.4	463.0	448.5	434.1	419.6	405.2	390.7
634.2	616.9	599.6	582.2	564.9	547.5	530.2	512.8	495.5	478.2	460.9
733.1	712.8	692.6	672.3	652.1	631.8	611.6	591.3	571.0	550.8	530.5
831.9	808.8	785.6	762.4	739.3	716.1	693.0	669.8	646.6	623.4	600.3
931.0	904.9	878.9	852.8	826.7	800.7	774.6	748.5	722.5	696.4	670.3
372.5	362.6	352.8	343.0	333.2	323.3	313.5	303.7	293.8	284.0	274.2
609.7	651.2	632.7	614.1	595.6	577.1	558.6	540.1	521.6	503.1	484.6
768.7	747.3	725.9	704.5	683.1	661.7	640.3	618.9	597.5	576.0	554.6
867.8	843.5	819.2	794.9	770.6	746.3	722.0	697.1	673.4	649.1	624.8
966.6	939.4	912.2	885.0	857.8	830.6	803.3	776.1	748.9	721.7	694.5
408.2	397.2	386.2	375.3	364.3	353.4	342.4	331.4	320.5	309.5	298.6
705.3	685.7	666.0	646.4	626.7	607.1	587.4	567.8	548.2	528.5	508.9
804.5	782.0	759.4	736.9	714.4	691.9	669.3	646.8	624.3	601.8	579.2
903.4	878.0	852.6	827.1	801.7	776.3	750.8	725.4	700.0	674.5	649.1
1002.1	973.8	945.4	917.1	888.7	860.4	832.0	803.6	775.2	746.9	718.6

Columns

Continued

Outside Dia- meter, Inches	Thickness of Metal, Inches	LENGTH OF COLUMN IN FEET								Sectional Area, Square Inches	Weight per Foot of Length of Column, Lbs.	
		8	10	12	14	16	18	20	22			24
6	$\frac{1}{2}$	52.4	46.0	40.2	35.0	30.4	26.4	23.0	8.6	26.95	
6	$\frac{3}{4}$	75.0	66.0	57.6	50.0	43.4	37.8	33.0	12.4	38.59	
6	$\frac{7}{8}$	85.4	75.2	65.6	59.0	49.4	43.0	37.6	14.1	43.96	
6	1	95.2	83.8	73.0	63.6	55.2	48.0	42.0	15.7	49.01	
6	$1\frac{1}{8}$	104.4	92.0	80.2	69.6	60.4	52.6	46.0	17.2	53.76	
7	$\frac{3}{4}$	95.4	86.2	77.0	68.6	60.8	53.8	47.8	42.4	37.8	14.7	45.96
7	1	122.2	110.4	98.6	87.6	77.8	68.8	61.2	54.2	48.4	18.9	58.90
7	$1\frac{1}{8}$	134.4	121.6	108.6	96.6	85.6	75.8	67.4	59.8	53.4	20.8	64.77
8	$\frac{3}{4}$	115.8	106.6	97.2	88.2	79.4	71.6	64.4	57.8	52.2	17.1	53.29
8	1	149.2	137.4	125.0	113.4	102.2	92.0	82.8	74.6	67.2	22.0	68.64
8	$1\frac{1}{4}$	179.8	165.6	151.0	136.8	123.4	111.0	99.8	89.8	81.0	26.5	82.71
9	$\frac{3}{4}$	136.2	127.2	117.8	108.4	99.2	90.4	82.4	75.0	68.2	19.4	60.65
9	1	176.0	164.6	152.4	140.0	128.2	116.8	106.4	96.8	88.2	25.1	78.40
9	$1\frac{1}{4}$	213.2	199.2	184.4	169.6	155.2	141.6	128.8	117.4	106.8	30.4	94.94
9	$1\frac{1}{2}$	247.6	231.4	214.2	197.0	180.2	164.4	149.6	136.2	124.0	35.3	110.26
9	$1\frac{3}{4}$	279.2	261.0	241.6	222.2	203.2	185.4	168.8	153.6	139.8	39.9	124.36
10	1	202.8	191.8	179.6	167.2	154.8	143.0	131.6	121.0	111.0	28.3	88.23
10	$1\frac{1}{4}$	246.6	233.0	218.2	203.2	188.2	173.6	159.8	146.8	135.0	34.4	107.23
10	$1\frac{1}{2}$	287.4	271.6	254.6	237.0	219.4	202.4	186.4	170.0	157.4	40.1	124.99
10	$1\frac{3}{4}$	325.4	307.6	288.2	268.2	248.4	229.2	211.0	194.0	178.2	45.4	141.65
11	1	229.6	218.8	207.0	194.6	182.0	169.6	160.4	146.0	135.4	31.4	98.03
11	$1\frac{1}{4}$	279.8	266.6	252.2	237.2	221.8	206.6	195.6	178.8	165.0	38.3	119.46
11	$1\frac{1}{2}$	327.0	311.8	295.0	277.2	257.4	241.6	228.6	208.2	192.8	44.8	139.68
11	$1\frac{3}{4}$	371.4	354.2	335.0	315.0	294.6	274.4	259.6	236.6	219.0	50.9	158.68
11	2	413.2	393.8	372.6	350.2	327.6	305.2	288.8	263.0	243.6	56.6	176.44

The above table is based on the Gordon Formula $P = \frac{8000}{1 + \frac{l^2}{800d^2}}$

in which P = Allowable pressure per square inch of cross section.

l = Length of Column in inches.

d = Outside diameter in inches.

This table continued on next page.

Safe Loads in Thousands of Pounds Hollow Cylindrical Cast Iron Columns

Outside Diameter, Inches	Thickness of Metal, Inches	LENGTH OF COLUMN IN FEET								Sectional Area, Square Inches	Weight per Foot of Length of Column, Lbs.
		8	10	12	14	16	18	20	22	24	
12	1	256.0	245.8	234.4	222.0	209.4	196.8	184.4	172.2	160.8	34.6
12	1 1/4	312.8	300.2	286.2	271.4	255.8	240.4	225.2	210.4	196.4	42.2
12	1 1/2	366.6	351.8	335.4	318.0	299.8	281.8	264.0	246.6	230.2	49.5
12	1 3/4	417.4	400.8	382.0	362.2	341.4	320.8	300.6	281.0	262.2	56.4
12	2	465.4	446.8	426.0	403.8	380.8	357.8	335.2	313.2	292.2	62.8
13	1	282.4	272.6	261.4	249.4	237.0	224.2	211.6	199.0	187.0	37.7
13	1 1/4	345.6	333.6	320.0	305.4	290.0	274.4	258.8	243.6	228.8	46.1
13	1 1/2	406.0	391.8	375.8	358.6	340.6	322.2	304.0	286.2	268.6	54.2
13	1 3/4	463.2	447.2	429.0	409.4	388.8	367.8	347.0	326.6	306.6	61.9
13	2	517.8	499.8	479.4	457.4	434.6	411.0	387.8	365.0	342.6	69.1
14	1	308.6	299.2	288.6	277.0	264.6	251.8	239.0	226.2	213.6	40.8
14	1 1/4	378.4	366.8	353.8	339.4	324.4	308.8	293.0	277.2	262.0	50.1
14	1 1/2	445.2	431.6	416.2	399.4	381.6	363.4	344.6	326.2	308.2	58.9
14	1 3/4	508.8	493.4	475.8	456.6	436.2	415.2	394.0	373.0	352.4	67.4
14	2	569.6	552.4	532.8	511.2	488.4	464.8	441.2	417.6	394.4	75.4
15	1	334.8	325.8	315.6	304.2	292.0	279.4	266.6	253.6	240.8	44.0
15	1 1/4	411.0	400.0	387.4	373.4	358.6	343.0	327.2	311.4	295.8	54.0
15	1 1/2	484.2	471.4	456.4	440.0	422.4	404.2	385.6	367.0	348.4	63.6
15	1 3/4	554.4	539.6	522.6	503.8	483.8	462.8	441.4	420.2	399.0	72.9
15	2	621.6	605.0	586.0	565.0	542.4	519.0	495.0	471.0	447.2	81.7

The above table is based on the Gordon Formula $P = \frac{8000}{1 + \frac{l^2}{800d^2}}$

in which P = Allowable pressure per square inch of cross section.

l = Length of Column in inches.

d = Outside diameter in inches.

Struts

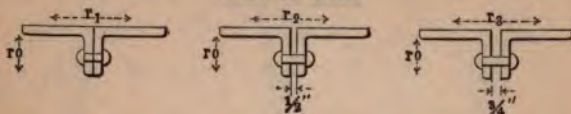
Safe Strength of Steel Struts

For different proportions of length in inches = l To least radius of gyration in inches = r Safe strength in pounds per square inch = $16000 - 70 \frac{l}{r}$

$\frac{l}{r}$	Safe Strength per Square Inch, Pounds	$\frac{l}{r}$	Safe Strength per Square Inch, Pounds	$\frac{l}{r}$	Safe Strength per Square Inch, Pounds	$\frac{l}{r}$	Safe Strength per Square Inch, Pounds
30	13900	60	11800	90	9700	120	7600
31	13830	61	11730	91	9630	121	7530
32	13760	62	11660	92	9560	122	7460
33	13690	63	11590	93	9490	123	7390
34	13620	64	11520	94	9420	124	7320
35	13550	65	11450	95	9350	125	7250
36	13480	66	11380	96	9280	126	7180
37	13410	67	11310	97	9210	127	7110
38	13340	68	11240	98	9140	128	7040
39	13270	69	11170	99	9070	129	6970
40	13200	70	11100	100	9000	130	6900
41	13130	71	11030	101	8930	131	6830
42	13060	72	10960	102	8860	132	6760
43	12990	73	10890	103	8790	133	6690
44	12920	74	10820	104	8720	134	6620
45	12850	75	10750	105	8650	135	6550
46	12780	76	10680	106	8580	136	6480
47	12710	77	10610	107	8510	137	6410
48	12640	78	10540	108	8440	138	6340
49	12570	79	10470	109	8370	139	6270
50	12500	80	10400	110	8300	140	6200
51	12430	81	10330	111	8230	141	6130
52	12360	82	10260	112	8160	142	6060
53	12290	83	10190	113	8090	143	5990
54	12220	84	10120	114	8020	144	5920
55	12150	85	10050	115	7950	145	5850
56	12080	86	9980	116	7880	146	5780
57	12010	87	9910	117	7810	147	5710
58	11940	88	9840	118	7740	148	5640
59	11870	89	9770	119	7670	149	5570
						150	5500

Radii of Gyration

For Two Unequal Legged Angles, Placed with Shorter Legs Back to Back

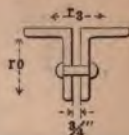
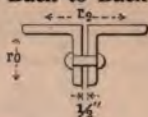
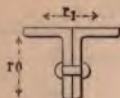


Size of Angles, Inches	Weight per Foot of Single Angle, Pounds	Area of Two Angles, Square Inches	Radii of Gyration			
			r ₀	r ₁	r ₂	r ₃
8 x 6 x 1 ¹ / ₈	49.3	29.00	1.71	3.66	3.85	3.95
8 x 6 x 1 ¹ / ₂	23.0	13.50	1.79	3.56	3.74	3.83
7 x 3 ¹ / ₂ x 7 ⁷ / ₈	28.7	16.84	0.90	3.45	3.65	3.75
7 x 3 ¹ / ₂ x 7 ¹ / ₁₆	15.0	8.80	0.95	3.37	3.56	3.66
6 x 4 x 1 ¹ / ₁₆	25.4	14.94	1.11	2.81	3.00	3.10
6 x 4 x 3 ³ / ₈	12.3	7.22	1.17	2.74	2.92	3.01
6 x 3 ¹ / ₂ x 3 ³ / ₄	22.4	13.12	0.94	2.88	3.08	3.18
6 x 3 ¹ / ₂ x 3 ³ / ₈	11.7	6.84	0.99	2.81	3.00	3.10
5 x 4 x 1 ¹ / ₁₆	22.7	13.30	1.15	2.27	2.46	2.56
5 x 4 x 3 ³ / ₈	11.0	6.46	1.20	2.20	2.38	2.48
5 x 3 ¹ / ₂ x 3 ³ / ₄	19.8	11.62	0.98	2.34	2.53	2.63
5 x 3 ¹ / ₂ x 1 ¹ / ₁₆	8.7	5.12	1.03	2.26	2.44	2.54
5 x 3 x 1 ¹ / ₁₆	17.1	10.06	0.81	2.40	2.59	2.69
5 x 3 x 5 ¹ / ₁₆	8.2	4.80	0.85	2.33	2.51	2.61
4 ¹ / ₂ x 3 x 1 ¹ / ₁₆	16.0	9.36	0.83	2.12	2.32	2.42
4 ¹ / ₂ x 3 x 1 ¹ / ₁₆	7.7	4.50	0.88	2.06	2.25	2.34
4 x 3 ¹ / ₂ x 1 ¹ / ₁₆	18.5	10.86	1.01	1.81	2.01	2.11
4 x 3 ¹ / ₂ x 5 ¹ / ₁₆	7.7	4.50	1.07	1.73	1.91	2.00
4 x 3 x 1 ¹ / ₁₆	14.8	8.68	0.84	1.85	2.05	2.15
4 x 3 x 1 ¹ / ₁₆	7.2	4.18	0.89	1.79	1.97	2.07
3 ¹ / ₂ x 3 x 1 ¹ / ₁₆	13.6	8.00	0.86	1.59	1.78	1.88
3 ¹ / ₂ x 3 x 1 ¹ / ₄	5.4	3.12	0.91	1.52	1.70	1.79
3 ¹ / ₂ x 2 ¹ / ₂ x 1 ¹ / ₁₆	10.4	6.12	0.70	1.63	1.83	1.93
3 ¹ / ₂ x 2 ¹ / ₂ x 1 ¹ / ₄	4.9	2.88	0.74	1.58	1.76	1.86
3 x 2 ¹ / ₂ x 9 ¹ / ₁₆	9.5	5.56	0.72	1.36	1.56	1.66
3 x 2 ¹ / ₂ x 1 ¹ / ₄	4.5	2.62	0.75	1.31	1.50	1.59
3 x 2 x 1 ¹ / ₂	7.7	4.50	0.55	1.42	1.62	1.72
3 x 2 x 5 ¹ / ₁₆	3.07	1.82	0.58	1.37	1.55	1.65
2 ¹ / ₂ x 2 x 1 ¹ / ₂	6.8	4.00	0.56	1.15	1.35	1.46
2 ¹ / ₂ x 2 x 1 ¹ / ₁₆	2.75	1.62	0.60	1.10	1.28	1.38

Radii of Gyration

Continued

For Two Unequal Legged Angles, Placed with Longer Legs Back to Back



Size of Angles, Inches	Weight per Foot of Single Angle, Pounds	Area of Two Angles, Square Inches	Radii of Gyration			
			r ₀	r ₁	r ₂	r ₃
8 x 6 x 1 1/8	49.3	29.00	2.47	2.41	2.59	2.69
8 x 6 x 1/2	23.0	13.50	2.56	2.32	2.48	2.57
7 x 3 1/2 x 7/8	28.7	16.84	2.20	1.28	1.47	1.57
7 x 3 1/2 x 7/16	15.0	8.80	2.26	1.21	1.38	1.47
6 x 4 x 1 1/8	25.4	14.94	1.87	1.56	1.75	1.85
6 x 4 x 3/8	12.3	7.22	1.93	1.50	1.67	1.76
6 x 3 1/2 x 3/4	22.4	13.12	1.89	1.32	1.51	1.61
6 x 3 1/2 x 3/8	11.7	6.84	1.94	1.26	1.43	1.53
5 x 4 x 1 1/8	22.7	13.30	1.53	1.64	1.83	1.93
5 x 4 x 3/8	11.0	6.46	1.59	1.58	1.75	1.85
5 x 3 1/2 x 3/4	19.8	11.62	1.55	1.40	1.59	1.69
5 x 3 1/2 x 1/16	8.7	5.12	1.61	1.33	1.50	1.59
5 x 3 x 1 1/8	17.1	10.06	1.56	1.15	1.34	1.44
5 x 3 x 5/16	8.2	4.80	1.61	1.09	1.26	1.35
4 1/2 x 3 x 1 1/8	16.0	9.36	1.39	1.19	1.38	1.48
4 1/2 x 3 x 5/16	7.7	4.50	1.44	1.13	1.30	1.40
4 x 3 1/2 x 1 1/8	18.5	10.86	1.19	1.50	1.69	1.79
4 x 3 1/2 x 5/16	7.7	4.50	1.26	1.42	1.60	1.69
4 x 3 x 1 1/8	14.8	8.68	1.22	1.23	1.42	1.52
4 x 3 x 5/16	7.2	4.18	1.27	1.17	1.35	1.44
3 1/2 x 3 x 1 1/8	13.6	8.00	1.05	1.28	1.48	1.57
3 1/2 x 3 x 1/4	5.4	3.12	1.11	1.20	1.38	1.48
3 1/2 x 2 1/2 x 5/16	10.4	6.12	1.08	1.01	1.20	1.31
3 1/2 x 2 1/2 x 1/4	4.9	2.88	1.12	0.96	1.13	1.23
3 x 2 1/2 x 5/16	9.5	5.56	0.91	1.05	1.25	1.35
3 x 2 1/2 x 1/4	4.5	2.62	0.95	1.00	1.18	1.28
3 x 2 x 1/2	7.7	4.50	0.92	0.80	1.00	1.10
3 x 2 x 5/16	3.07	1.82	0.97	0.75	0.93	1.03
2 1/2 x 2 x 1/2	6.8	4.00	0.75	0.84	1.04	1.15
2 1/2 x 2 x 5/16	2.75	1.62	0.79	0.79	0.97	1.07

Radii of Gyration Continued

For Two Equal Legged Angles, Placed Back to Back



Size of Angles, Inches	Weight per Foot of Single Angle, Pounds	Area of Two Angles, Square Inches	RADIUS OF GYRATION			
			r_0	r_1	r_2	r_3
8 x 8 x $1\frac{1}{8}$	56.9	33.46	2.42	3.42	3.60	3.69
8 x 8 x $1\frac{1}{2}$	26.4	15.50	2.51	3.33	3.50	3.59
6 x 6 x 1	37.4	22.00	1.80	2.59	2.77	2.87
6 x 6 x $\frac{3}{8}$	14.9	8.72	1.88	2.49	2.67	2.76
5 x 5 x $\frac{1}{2}$	28.9	17.00	1.48	2.17	2.36	2.46
5 x 5 x $\frac{3}{8}$	12.3	7.22	1.56	2.09	2.26	2.35
4 x 4 x $\frac{1}{2}$	19.9	11.68	1.18	1.75	1.94	2.04
4 x 4 x $\frac{1}{4}$	6.6	3.88	1.25	1.66	1.84	1.93
$3\frac{1}{2}$ x $3\frac{1}{2}$ x $\frac{3}{4}$	16.0	9.38	1.03	1.54	1.74	1.84
$3\frac{1}{2}$ x $3\frac{1}{2}$ x $\frac{1}{4}$	5.8	3.38	1.09	1.46	1.64	1.73
3 x 3 x $\frac{5}{8}$	11.5	6.72	0.88	1.32	1.51	1.62
3 x 3 x $\frac{1}{4}$	4.9	2.88	0.93	1.25	1.43	1.53
$2\frac{1}{2}$ x $2\frac{1}{2}$ x $\frac{1}{2}$	7.7	4.50	0.74	1.10	1.29	1.40
$2\frac{1}{2}$ x $2\frac{1}{2}$ x $\frac{3}{16}$	3.07	1.80	0.78	1.04	1.22	1.32
2 x 2 x $\frac{1}{2}$	6.0	3.50	0.58	0.89	1.09	1.20
2 x 2 x $\frac{3}{16}$	2.44	1.42	0.62	0.84	1.03	1.13

Struts

Continued

Allowed stresses per square inch.

14,000 pounds for lengths less than 30 radii.

16,000—70 $\frac{1}{r}$ for lengths between 30 radii and 150 radii.

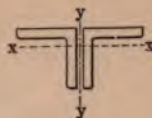
Size of Angles, Inches	Area 2 Angles, Square Inches	Least Radius of Gyratlon, Inches	Axis of Least Radius of Gyratlon	LENGTH IN FEET					
				2	3	4	5	6	7
8 x 6 x $1\frac{1}{8}$	29.00	2.47	X-X	395.0
8 x 6 x 1	26.00	2.49	X-X	354.6
8 x 6 x $\frac{7}{8}$	22.96	2.51	{ X-X Y-Y }	313.6
8 x 6 x $\frac{3}{4}$	19.88	2.48	Y-Y	270.9
8 x 6 x $\frac{5}{8}$	16.72	2.46	Y-Y	227.6
8 x 6 x $\frac{1}{2}$	13.50	2.44	Y-Y	183.5
7 x $3\frac{1}{2}$ x $\frac{7}{8}$	16.84	1.42	Y-Y	229.6	219.6	209.7	199.7
7 x $3\frac{1}{2}$ x $\frac{3}{4}$	14.62	1.40	Y-Y	198.8	190.1	181.3	172.5
7 x $3\frac{1}{2}$ x $\frac{5}{8}$	12.34	1.37	Y-Y	167.2	159.6	152.0	144.5
7 x $3\frac{1}{2}$ x $\frac{1}{2}$	10.00	1.35	Y-Y	135.1	128.9	122.7	116.4
7 x $3\frac{1}{2}$ x $\frac{3}{8}$	8.80	1.33	Y-Y	118.6	113.0	107.5	101.9
6 x 4 x $\frac{11}{8}$	14.94	1.70	Y-Y	202.1	194.7	187.4
6 x 4 x $\frac{3}{4}$	13.88	1.69	Y-Y	187.6	180.7	173.8
6 x 4 x $\frac{5}{8}$	11.72	1.67	Y-Y	158.1	152.1	146.3
6 x 4 x $\frac{1}{2}$	9.50	1.64	Y-Y	127.7	122.8	117.9
6 x 4 x $\frac{3}{8}$	7.22	1.62	Y-Y	96.8	93.1	89.3
6 x $3\frac{1}{2}$ x $\frac{3}{4}$	13.12	1.46	Y-Y	179.7	172.2	164.6	157.1
6 x $3\frac{1}{2}$ x $\frac{5}{8}$	11.10	1.43	Y-Y	151.5	145.0	138.5	132.0
6 x $3\frac{1}{2}$ x $\frac{1}{2}$	9.00	1.41	Y-Y	122.6	117.2	111.8	106.5
6 x $3\frac{1}{2}$ x $\frac{3}{8}$	6.84	1.39	Y-Y	92.9	88.8	84.6	80.5
5 x 4 x $\frac{11}{8}$	13.30	1.53	X-X	183.6	176.3	169.0	161.7
5 x 4 x $\frac{3}{4}$	12.38	1.54	X-X	171.1	164.3	157.6	150.8
5 x 4 x $\frac{5}{8}$	10.46	1.55	X-X	144.7	139.0	133.3	127.7
5 x 4 x $\frac{1}{2}$	8.50	1.57	X-X	117.8	113.3	108.7	104.1
5 x 4 x $\frac{3}{8}$	6.46	1.59	X-X	89.7	86.3	82.9	79.5
5 x $3\frac{1}{2}$ x $\frac{3}{4}$	11.62	1.54	Y-Y	160.6	154.2	147.9	141.6
5 x $3\frac{1}{2}$ x $\frac{5}{8}$	9.84	1.51	Y-Y	135.5	130.1	124.6	119.1
5 x $3\frac{1}{2}$ x $\frac{1}{2}$	8.00	1.49	Y-Y	110.0	105.4	100.9	96.4
5 x $3\frac{1}{2}$ x $\frac{3}{8}$	6.10	1.46	Y-Y	83.6	80.1	76.5	73.0
5 x $3\frac{1}{2}$ x $\frac{1}{8}$	5.12	1.45	Y-Y	70.1	67.1	64.1	61.2
5 x 3 x $\frac{11}{8}$	10.06	1.29	Y-Y	134.8	128.2	121.7	115.1
5 x 3 x $\frac{3}{4}$	9.22	1.28	Y-Y	123.3	117.3	111.2	105.2
5 x 3 x $\frac{5}{8}$	7.50	1.25	Y-Y	99.8	94.8	89.8	84.7
5 x 3 x $\frac{1}{2}$	5.72	1.23	Y-Y	75.9	72.0	68.1	64.2
5 x 3 x $\frac{3}{8}$	4.80	1.22	Y-Y	63.6	60.3	57.0	53.7

This table continued on next page.

JONES & LAUGHLIN STEEL COMPANY

Safe Loads in Thousands of Pounds For Struts Composed of Two Angles with Unequal Legs

Long legs parallel and $\frac{3}{8}$ inches apart.



LENGTH IN FEET

8	9	10	12	14	16	18	20	22	24	26	28	30
385.1	375.2	365.4	345.7	325.9	306.2	286.5	266.8	247.0	227.3	207.6	187.9	168.1
345.8	337.1	328.3	310.7	293.2	275.7	258.1	240.6	223.0	205.5	188.0	170.4	152.9
305.9	298.2	290.5	275.2	259.8	244.4	229.1	213.7	198.3	183.0	167.6	152.2	136.9
264.2	257.5	250.7	237.3	223.8	210.3	196.9	183.4	169.9	156.5	143.0	129.5	116.1
221.8	216.1	210.4	199.0	187.7	176.2	164.8	153.3	141.9	130.5	119.1	107.7	96.2
178.8	174.2	169.5	160.2	150.9	141.6	132.3	123.1	113.8	104.5	95.2	85.9	76.6
189.7	179.8	169.8	149.9	130.0	110.1	93.6	76.4	60.4	45.9	32.4	18.9	5.4
163.7	155.0	146.2	128.7	111.1	93.6	76.4	60.4	45.9	32.4	18.9	5.4	
136.9	129.3	121.8	106.6	91.5	76.4	60.4	45.9	32.4	18.9	5.4		
110.2	104.0	97.8	85.3	72.9	60.4	45.9	32.4	18.9	5.4			
96.3	90.8	85.2	74.1	63.0	51.9	40.8	29.7	18.6	7.5			
180.0	172.6	165.2	155.5	135.7	120.9	106.2	91.4	76.6	61.8	47.0	32.2	17.4
166.9	160.0	153.1	139.3	125.5	111.7	97.9	84.1	70.3	56.5	42.7	28.9	15.1
140.4	134.5	128.6	116.8	105.0	93.2	81.4	69.6	57.8	46.0	34.2	22.4	10.6
113.1	108.2	103.3	93.6	83.8	74.1	64.3	54.6	44.8	35.0	25.2	15.4	5.6
85.6	81.8	78.1	70.6	63.1	55.6	48.1	40.7	33.2	25.7	18.2	10.7	3.2
149.5	142.0	134.4	119.3	104.2	89.2	74.1	59.0	43.9	28.8	13.7		
125.4	118.9	112.4	99.4	86.3	73.3	60.2	47.1	34.0	20.9	7.8		
101.1	95.7	90.4	79.7	68.9	58.2	47.5	36.8	26.1	15.4	4.7		
76.4	72.2	68.1	59.8	51.6	43.3	35.0	26.7	18.4	9.1			
154.4	147.1	139.8	125.2	110.6	96.0	81.4	66.8	52.2	37.6	23.0	8.4	
144.1	137.3	130.6	117.0	103.5	90.0	76.5	63.0	49.5	36.0	22.5	9.0	
122.0	116.3	110.7	99.3	88.0	76.6	65.3	54.0	42.7	31.4	20.1	8.8	
99.6	95.0	90.5	81.4	72.3	63.1	54.0	44.9	35.8	26.7	17.6	6.3	
76.0	72.6	69.2	62.4	55.5	48.7	41.9	35.0	28.1	21.2	14.3	7.4	
135.2	128.9	122.5	109.9	91.2	84.5	71.8	59.0	46.2	33.4	20.6	8.0	
113.7	108.2	102.7	91.8	80.8	69.9	59.0	48.1	37.0	25.6	14.6	5.2	
91.9	87.4	82.9	73.9	64.9	55.8	46.8	37.7	28.6	19.5	10.4	3.3	
69.5	66.0	62.5	55.5	48.5	41.5	34.4	27.4	20.3	13.2	6.1		
58.2	55.2	52.3	46.3	40.4	34.5	28.5	22.6	16.7	10.8	4.9		
108.6	102.0	95.5	82.4	69.3	56.2	43.1	30.0	16.9	4.0			
99.1	93.1	87.0	74.9	62.8	50.7	38.6	26.5	14.4	2.9			
79.7	74.6	69.6	50.5	49.4	36.8	24.7	12.9	1.4				
60.3	56.4	52.5	44.6	36.8	24.7	12.9	1.4					
50.4	47.0	43.7	37.1	30.5	24.7	12.9	1.4					

JONES & LAUGHLIN STEEL COMPANY

Struts Continued

Allowed stresses per square inch.
14,000 pounds for lengths less than 30 radii.
16,000—70 $\frac{1}{r}$ for lengths between 30 radii and 150 radii.

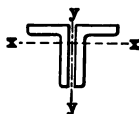
Size of Angles, Inches	Area 2 Angles, Square Inches	Least Radius of Gyration, Inches	Axis of Least Radius of Gyration	LENGTH IN FEET					
				2	3	4	5	6	7
4½ x 3 x ¼	9.36	1.33	Y-Y	126.1	120.2	114.3	108.4
4½ x 3 x ⅜	8.60	1.31	Y-Y	115.5	110.0	104.5	99.0
4½ x 3 x ½	7.00	1.29	Y-Y	93.8	89.2	84.7	80.1
4½ x 3 x ¾	5.34	1.27	Y-Y	71.3	67.8	64.2	60.7
4½ x 3 x ⅞	4.50	1.26	Y-Y	60.0	57.0	54.0	51.0
4 x 3½ x ¼	10.86	1.19	X-X	150.8	143.1	135.4	127.8	120.1
4 x 3½ x ⅜	10.12	1.20	X-X	140.7	133.6	126.5	119.4	112.3
4 x 3½ x ½	8.60	1.22	X-X	113.9	108.0	102.1	96.2
4 x 3½ x ¾	7.00	1.23	X-X	92.9	88.1	83.3	78.5
4 x 3½ x ¾	5.34	1.25	X-X	71.1	67.5	63.9	60.3
4 x 3½ x ⅞	4.50	1.26	X-X	60.0	57.0	54.0	51.0
4 x 3 x ¼	8.68	1.22	X-X	115.0	109.0	103.0	97.0
4 x 3 x ⅜	7.96	1.23	X-X	105.6	100.1	94.7	89.3
4 x 3 x ½	6.50	1.25	X-X	86.5	82.2	77.8	73.4
4 x 3 x ¾	4.96	1.26	X-X	66.1	62.8	59.5	56.2
4 x 3 x ⅞	4.18	1.27	X-X	55.8	53.1	50.3	47.5
3½ x 3 x ¼	8.00	1.05	X-X	108.8	102.4	96.0	89.6	83.2
3½ x 3 x ⅜	7.34	1.06	X-X	100.0	94.2	88.4	82.5	76.7
3½ x 3 x ½	6.00	1.07	X-X	81.9	77.2	72.4	67.7	63.0
3½ x 3 x ¾	4.60	1.09	X-X	63.0	59.4	55.9	52.3	48.8
3½ x 3 x ¾	3.12	1.11	X-X	42.8	40.5	38.1	35.8	33.4
3½ x 2½ x ¼	6.12	1.08	X-X	83.6	78.9	74.1	69.4	64.6
3½ x 2½ x ⅜	5.50	1.09	X-X	75.3	71.0	66.8	62.6	58.3
3½ x 2½ x ½	4.22	1.10	X-X	57.9	54.6	51.4	48.2	45.0
3½ x 2½ x ¾	2.88	1.09	Y-Y	39.4	37.2	35.0	32.8	30.5
3 x 2½ x ¼	5.56	.91	X-X	73.6	68.4	63.3	58.2	53.0
3 x 2½ x ⅜	5.00	.91	X-X	66.2	61.5	56.9	52.3	47.7
3 x 2½ x ½	3.84	.93	X-X	51.0	47.6	44.1	40.6	37.2
3 x 2½ x ¾	2.62	.95	X-X	35.0	32.7	30.3	28.0	25.7
3 x 2 x ¼	4.50	.92	X-X	59.7	55.6	51.5	47.3	43.2
3 x 2 x ⅜	3.46	.92	Y-Y	45.9	42.7	39.6	36.4	33.2
3 x 2 x ½	2.88	.89	Y-Y	31.3	29.1	26.9	24.6	22.4
3 x 2 x ¾	1.82	.88	Y-Y	23.9	22.2	20.4	18.7	17.0
2½ x 2 x ¼	4.00	.75	X-X	55.0	50.6	46.1	41.6	37.1	32.6
2½ x 2 x ⅜	3.10	.77	X-X	42.8	39.5	36.1	32.7	29.3	25.9
2½ x 2 x ½	2.10	.78	X-X	29.4	27.1	24.8	22.5	20.2	17.9
2½ x 2 x ¾	1.62	.79	X-X	22.5	20.0	19.0	17.3	15.6	13.9

This table continued on next page.

JONES & LAUGHLIN STEEL COMPANY

Safe Loads in Thousands of Pounds For Struts Composed of Two Angles with Unequal Legs

Long legs parallel and $\frac{3}{8}$ inches apart.



LENGTH IN FEET

8	9	10	12	14	16	18	20	22	24	26	28	30
102.5	96.6	90.6	78.8	67.0	55.2							
93.6	88.0	82.5	71.4	60.4	49.4							
75.5	71.0	66.4	57.3	48.2	39.1							
57.2	53.6	50.1	43.0	36.0								
48.0	45.0	42.0	36.0	30.0								
112.4	104.8	97.1	81.8	66.4								
105.2	98.2	91.1	76.9	62.7								
90.2	84.3	78.4	66.5	54.7								
73.8	69.0	64.2	54.6	45.1								
56.7	53.1	49.6	42.4	35.2								
48.0	45.0	42.0	36.0	30.0								
91.1	85.1	79.1	67.2	55.2								
83.9	78.4	73.0	62.1	51.3								
69.1	64.7	60.3	51.6	42.8								
52.9	49.6	46.3	39.7	33.1								
44.8	42.0	39.2	33.7	28.2								
76.8	70.4	64.0	51.2									
70.9	65.1	59.3	47.6									
58.3	53.6	48.9	39.5									
45.2	41.7	38.2	31.1									
31.0	28.7	26.3	21.6									
59.8	55.1	50.3	40.8									
54.1	49.9	45.6	37.1									
41.7	38.5	35.3	28.9									
28.3	26.1	23.9	19.4									
47.9	42.8	37.6										
43.1	38.5	33.8										
33.7	30.2	26.8										
23.4	21.1	18.8										
39.1	35.0	30.9										
30.1	26.9	23.8										
20.1	17.9	15.6										
15.2	13.5	11.7										
28.2	23.7											
22.5	19.2											
15.7	13.4											
12.1	10.4											

Struts

Continued

Allowed stresses per square inch.

14,000 pounds for lengths less than 30 radii.

16,000—70 $\frac{1}{r}$ for lengths between 30 radii and 150 radii.

Size of Angles, Inches	Area 2 Angles, Square Inches	Least Radius of Gyration, Inches	Axis of Least Radius of Gyration	LENGTH IN FEET					
				2	3	4	5	6	7
8 x 8 x $1\frac{1}{8}$	33.46	2.42	X-X	454.1
8 x 8 x 1	30.00	2.44	X-X	407.7
8 x 8 x $\frac{7}{8}$	26.46	2.45	X-X	359.9
8 x 8 x $\frac{3}{4}$	22.88	2.47	X-X	311.5
8 x 8 x $\frac{5}{8}$	19.22	2.49	X-X	262.1
8 x 8 x $\frac{1}{2}$	15.50	2.50	X-X	211.6
6 x 6 x 1	22.00	1.80	X-X	300.7	290.4	280.1
6 x 6 x $\frac{7}{8}$	19.46	1.81	X-X	266.2	257.2	248.2
6 x 6 x $\frac{3}{4}$	16.88	1.83	X-X	231.3	223.6	215.8
6 x 6 x $\frac{5}{8}$	14.22	1.84	X-X	195.1	188.6	182.1
6 x 6 x $\frac{1}{2}$	11.50	1.86	X-X	158.0	152.8	147.6
6 x 6 x $\frac{3}{8}$	8.72	1.88	X-X	120.0	116.1	112.2
5 x 5 x $1\frac{1}{8}$	17.00	1.48	X-X	233.4	223.8	214.1	204.5
5 x 5 x $\frac{7}{8}$	15.96	1.49	X-X	219.4	210.4	201.4	192.4
5 x 5 x $\frac{3}{4}$	13.88	1.51	X-X	191.2	183.5	175.8	168.0
5 x 5 x $\frac{5}{8}$	11.72	1.52	X-X	161.6	155.1	148.7	142.2
5 x 5 x $\frac{1}{2}$	9.50	1.54	X-X	131.3	126.1	120.9	115.7
5 x 5 x $\frac{3}{8}$	7.22	1.56	X-X	100.0	96.1	92.2	88.3
4 x 4 x $1\frac{1}{8}$	11.68	1.18	X-X	161.9	153.6	145.3	137.0	128.7
4 x 4 x $\frac{7}{8}$	10.88	1.19	X-X	151.0	143.4	135.7	128.0	120.3
4 x 4 x $\frac{3}{4}$	9.22	1.20	X-X	128.2	121.7	115.3	108.8	102.3
4 x 4 x $\frac{5}{8}$	7.50	1.22	X-X	99.3	97.2	89.0	83.8
4 x 4 x $\frac{1}{2}$	5.72	1.23	X-X	75.9	72.0	68.1	64.2
4 x 4 x $\frac{3}{8}$	3.88	1.25	X-X	51.6	49.0	46.4	43.8
3 $\frac{1}{2}$ x 3 $\frac{1}{2}$ x $\frac{3}{4}$	9.38	1.03	X-X	127.1	119.5	111.8	104.2	96.5
3 $\frac{1}{2}$ x 3 $\frac{1}{2}$ x $\frac{5}{8}$	7.96	1.04	X-X	108.1	101.6	95.2	88.8	82.4
3 $\frac{1}{2}$ x 3 $\frac{1}{2}$ x $\frac{1}{2}$	6.50	1.06	X-X	88.5	83.4	78.2	73.1	67.9
3 $\frac{1}{2}$ x 3 $\frac{1}{2}$ x $\frac{3}{8}$	4.96	1.07	X-X	67.7	63.8	59.9	56.0	52.1
3 $\frac{1}{2}$ x 3 $\frac{1}{2}$ x $\frac{1}{4}$	3.38	1.09	X-X	46.3	43.7	41.1	38.4	35.8
3 x 3 x $\frac{5}{8}$	6.72	0.88	X-X	88.3	81.9	75.4	69.0	62.6
3 x 3 x $\frac{1}{2}$	5.50	0.90	X-X	72.6	67.5	62.3	57.2	52.1
3 x 3 x $\frac{3}{8}$	4.22	0.91	X-X	55.8	51.9	48.0	44.1	40.3
3 x 3 x $\frac{1}{4}$	2.88	0.93	X-X	38.3	35.7	33.1	30.5	27.9
2 $\frac{1}{2}$ x 2 $\frac{1}{2}$ x $\frac{1}{2}$	4.50	0.74	X-X	61.8	56.7	51.6	46.5	41.4	36.2
2 $\frac{1}{2}$ x 2 $\frac{1}{2}$ x $\frac{3}{8}$	3.46	0.75	X-X	47.6	43.7	39.9	36.0	32.1	28.2
2 $\frac{1}{2}$ x 2 $\frac{1}{2}$ x $\frac{1}{4}$	2.94	0.76	X-X	40.5	37.3	34.0	30.8	27.5	24.3
2 $\frac{1}{2}$ x 2 $\frac{1}{2}$ x $\frac{3}{16}$	2.38	0.77	X-X	32.9	30.3	27.7	25.1	22.5	19.9
2 $\frac{1}{2}$ x 2 $\frac{1}{2}$ x $\frac{1}{16}$	1.80	0.78	X-X	24.9	23.0	21.0	19.1	17.2	15.2
2 x 2 x $\frac{1}{2}$	3.50	0.58	X-X	45.9	40.8	35.7	30.7	25.6	20.5
2 x 2 x $\frac{3}{8}$	2.72	0.59	X-X	35.8	31.9	28.0	24.2	20.3	16.4
2 x 2 x $\frac{1}{4}$	2.30	0.60	X-X	30.4	27.1	23.9	20.7	17.5	14.3
2 x 2 x $\frac{3}{16}$	1.88	0.61	X-X	24.9	22.3	19.7	17.1	14.5	12.0
2 x 2 x $\frac{1}{16}$	1.42	0.62	X-X	18.9	16.9	15.0	13.1	11.2	9.3

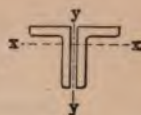
This table continued on next page.

JONES & LAUGHLIN STEEL COMPANY

Safe Loads in Thousands of Pounds

For Struts Composed of Two Angles with
Equal Legs

Parallel legs $\frac{3}{8}$ inches apart.



LENGTH IN FEET

8	9	10	12	14	16	18	20	22	24	26	28	30
442.4	430.8	419.2	396.0	372.8	349.5	326.3	303.1	279.9	256.6	233.4	210.2	186.9
397.4	387.0	376.7	356.1	335.4	314.7	294.1	273.4	252.8	232.1	211.4	190.8	170.1
350.8	341.7	332.6	314.5	296.4	278.2	260.1	241.9	223.8	205.7	187.5	169.4	151.2
303.7	296.0	288.3	272.7	257.1	241.6	226.0	210.5	194.9	179.3	163.8	148.2	132.6
255.6	249.2	242.7	229.7	216.7	203.8	190.8	177.8	164.9	151.9	138.9	125.9	113.0
206.3	201.1	195.9	185.5	175.1	164.7	154.3	143.8	133.4	123.0	112.6	102.2	91.8
269.9	259.6	249.3	228.8	208.3	187.8	167.2	146.7	126.2
239.1	230.1	221.1	203.0	184.9	166.9	148.8	130.8	112.7
208.1	200.3	192.6	177.1	161.6	146.1	130.6	115.1	99.6
175.6	169.1	162.6	149.6	136.6	123.6	110.6	97.7	84.7
142.4	137.3	132.1	121.7	111.3	100.9	90.5	80.1	69.7
108.4	104.5	100.6	92.8	85.0	77.2	69.4	61.6	53.8
194.8	185.2	175.5	156.2	136.9	117.6	98.3
183.4	174.4	165.4	147.4	129.4	111.4	93.4
160.3	152.6	144.9	129.4	114.0	98.6	83.1
135.7	129.2	122.8	109.8	96.9	83.9	70.9
110.5	105.4	100.2	89.8	79.5	69.1	58.7
84.4	80.5	76.6	68.9	61.1	53.3	45.6
120.4	112.1	103.7	87.1	70.5
112.6	105.0	97.3	81.9	66.6
95.9	89.4	83.0	70.1	57.2
78.7	73.5	68.4	58.0	47.7
60.3	56.4	52.5	44.6	36.8
41.2	38.6	36.0	30.8	25.6
88.9	81.2	73.6	58.3
75.9	69.5	63.1	50.2
62.8	57.6	52.5	42.2
48.2	44.3	40.4	32.5
33.2	30.6	28.0	22.8
56.2	49.8	43.4
46.0	41.8	36.7
36.4	32.5	28.6
25.3	22.7	20.1
31.1	26.0
24.4	20.5
21.0	17.8
17.3	14.7
13.3	11.4

Struts

Continued

Allowed stresses per square inch.
14,000 pounds for lengths less than 30 radii.
16,000—70 $\frac{1}{r}$ for lengths between 30 radii and 150 radii.

Size of Angle, Inches	Area of Angle, Square Inches	Least Radius of Gyration, Inches	LENGTH IN FEET			
			2	3	4	5
8 x 8 x $\frac{1}{8}$	16.73	1.55	231.4	222.3
8 x 8 x $\frac{1}{4}$	15.00	1.56	207.7	199.6
8 x 8 x $\frac{3}{8}$	13.23	1.56	183.2	176.1
8 x 8 x $\frac{1}{2}$	11.44	1.57	158.6	152.4
8 x 8 x $\frac{3}{4}$	9.61	1.58	133.3	128.2
8 x 8 x $\frac{7}{8}$	7.75	1.59	107.6	103.5
6 x 6 x $\frac{1}{8}$	11.00	1.16	152.1	144.1	136.2
6 x 6 x $\frac{1}{4}$	9.73	1.16	134.5	127.5	120.5
6 x 6 x $\frac{3}{8}$	8.44	1.17	116.9	110.8	104.7
6 x 6 x $\frac{1}{2}$	7.11	1.17	98.4	93.3	88.2
6 x 6 x $\frac{3}{4}$	5.75	1.18	79.7	75.6	71.6
6 x 6 x $\frac{7}{8}$	4.36	1.19	60.5	57.5	54.4
5 x 5 x $\frac{1}{8}$	8.50	.96	113.7	106.2	98.8
5 x 5 x $\frac{1}{4}$	7.98	.96	106.7	99.8	92.8
5 x 5 x $\frac{3}{8}$	6.94	.97	93.0	87.0	81.0
5 x 5 x $\frac{1}{2}$	5.86	.97	78.5	73.5	68.4
5 x 5 x $\frac{3}{4}$	4.75	.98	63.8	59.7	55.6
5 x 5 x $\frac{7}{8}$	3.61	.99	48.6	45.5	42.4
4 x 4 x $\frac{1}{8}$	5.84	.77	80.7	74.3	68.0	61.6
4 x 4 x $\frac{1}{4}$	5.44	.77	75.2	69.2	63.3	57.4
4 x 4 x $\frac{3}{8}$	4.61	.77	63.7	58.7	53.6	48.6
4 x 4 x $\frac{1}{2}$	3.75	.78	51.9	47.9	43.8	39.8
4 x 4 x $\frac{3}{4}$	2.86	.79	39.7	36.6	33.6	30.5
4 x 4 x $\frac{7}{8}$	1.94	.79	26.9	24.8	22.8	20.7
3 $\frac{1}{2}$ x 3 $\frac{1}{2}$ x $\frac{3}{8}$	4.69	.67	63.3	57.4	51.5	45.7
3 $\frac{1}{2}$ x 3 $\frac{1}{2}$ x $\frac{1}{2}$	3.98	.68	53.8	48.9	44.0	39.1
3 $\frac{1}{2}$ x 3 $\frac{1}{2}$ x $\frac{5}{8}$	3.25	.68	44.0	40.0	35.9	31.9
3 $\frac{1}{2}$ x 3 $\frac{1}{2}$ x $\frac{3}{4}$	2.48	.68	33.6	30.5	27.4	24.4
3 $\frac{1}{2}$ x 3 $\frac{1}{2}$ x $\frac{7}{8}$	1.69	.69	22.9	20.9	18.8	16.8
3 x 3 x $\frac{5}{8}$	3.36	.58	44.0	39.2	34.3	29.4
3 x 3 x $\frac{1}{2}$	2.75	.58	36.0	32.1	28.1	24.1
3 x 3 x $\frac{3}{4}$	2.11	.58	27.6	24.6	21.5	18.5
3 x 3 x $\frac{7}{8}$	1.44	.59	18.9	16.9	14.8	12.8
3 x 3 x $\frac{1}{4}$	1.09	.60	14.4	12.9	11.3	9.8
2 $\frac{1}{2}$ x 2 $\frac{1}{2}$ x $\frac{1}{4}$	2.25	.48	28.1	24.2	20.3	16.3
2 $\frac{1}{2}$ x 2 $\frac{1}{2}$ x $\frac{3}{8}$	1.73	.48	21.6	18.6	15.6	12.5
2 $\frac{1}{2}$ x 2 $\frac{1}{2}$ x $\frac{1}{2}$	1.47	.49	18.5	16.0	13.4	10.9
2 $\frac{1}{2}$ x 2 $\frac{1}{2}$ x $\frac{3}{4}$	1.19	.49	15.0	12.9	10.9	8.8
2 $\frac{1}{2}$ x 2 $\frac{1}{2}$ x $\frac{7}{8}$.90	.49	11.3	9.8	8.2	6.7
2 x 2 x $\frac{1}{4}$	1.75	.38	20.3	16.4	12.5
2 x 2 x $\frac{3}{8}$	1.36	.39	15.9	13.0	10.0
2 x 2 x $\frac{1}{2}$	1.15	.39	13.4	11.0	8.5
2 x 2 x $\frac{3}{4}$.94	.39	11.0	9.0	6.9
2 x 2 x $\frac{7}{8}$.71	.39	8.3	6.8	5.2

This table continued on next page.

JONES & LAUGHLIN STEEL COMPANY

Safe Loads in Thousands of Pounds For Equal Leg Single Angle Struts

LENGTH IN FEET

6	7	8	9	10	12	14	16	18
213.3	204.2	195.1	186.1	177.0	158.9	140.8	122.6	104.5
191.5	183.5	175.4	167.3	159.2	143.1	126.9	110.8	94.6
168.9	161.8	154.7	147.6	140.4	126.2	111.9	97.7	83.5
146.3	140.2	134.1	128.0	121.8	109.6	97.4	85.1	72.9
123.1	118.0	112.9	107.8	102.7	92.5	82.2	72.0	61.8
99.4	95.3	91.3	87.2	83.1	74.9	66.7	58.5	50.3
128.2	120.2	112.3	104.3	96.3	80.4	64.5
113.4	106.4	99.3	92.3	85.2	71.1	57.0
98.7	92.6	86.6	80.5	74.4	62.3	50.2
83.1	78.0	72.9	67.8	62.7	52.5	42.3
67.5	63.4	59.3	55.2	51.1	42.9	34.7
51.3	48.2	45.1	42.1	39.0	32.8	26.7
91.4	83.9	76.5	69.1	61.6	46.8
85.8	78.8	71.8	64.8	57.9	43.9
75.0	69.0	63.0	57.0	50.9	38.9
63.3	58.2	53.2	48.1	43.0	32.9
51.6	47.5	43.4	39.4	35.3	27.1
39.4	36.3	33.3	30.2	27.1	21.0
55.2	48.8	42.5	36.1
51.4	45.5	39.6	33.6
43.6	38.6	33.5	28.5
35.8	31.7	27.7	23.7
27.5	24.5	21.4	18.4
18.7	16.6	14.5	12.5
39.8	33.9	28.0
34.2	29.3	24.4
27.9	23.9	19.9
21.3	18.2	15.2
14.7	12.6	10.6
24.6	19.7
20.1	16.1
15.4	12.4
10.7	8.7
8.3	6.8
12.4
9.5
8.4
6.8
5.1
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.....
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Foundation Grillages

As a means of avoiding large masses of masonry and deep excavations, it has become the practice to use in foundation work, grillages composed of beams imbedded in concrete. These grillages are constructed of one, two or three layers of beams, depending on the load to be carried and the capacity of the earth to resist pressure. Such beams should be spaced at least $2\frac{1}{2}$ " or 3" apart in the clear between flanges, so as to enable the concrete to be readily placed and tamped.

The top tier of beams in all cases should be held in position and alignment by bolting the beams together by tie rods with separators made of gas pipe. Where more than one tier of beams is used, it is not the custom to use separators and tie rods on the lower tiers. Pipe separators are preferable to the usual cast iron separators as they interfere less with the continuity of the concrete.

In the design of grillages, it is customary to assume that the load supported by each beam in a tier is equal to the total load on the foundation, divided by the number of beams in that tier; also, that such loading is uniformly distributed over that portion of the top flange to which it is applied, and that the beam is supported with a uniform pressure from below over its entire length.

Under these conditions, the maximum bending moment occurs at the center of the length of the beam, and is given by the formula $\frac{W(L-N)}{8}$ in which W equals the load supported by each beam in pounds, L equals the length of beam in feet, and N the length in feet in which load is applied. This formula, it will be noted, is the same as that for a beam supported at each end and uniformly loaded, the length of which corresponds with the dimension of $L-N$ in the above formula. By the use of this length of $L-N$ as a span, it is possible to pick the size of grillage beams direct from the tables of safe loads for beams, as published in this book. It should be noted, however, that if the dimension of $L-N$ is less than the span given in these tables that there is great danger of the shear in the beam being in excess of the capacity of the beam webs to resist such shear.

Where beams are thoroughly imbedded in concrete and the webs prevented from buckling, the grillage beam would ordinarily be considered safe in shear, if such shear did not exceed in intensity

Foundation Grillages

Continued

12,000 pounds per square inch of web area, this web area being the depth of the beam, multiplied by its web thickness.

To transmit the load from the columns to the top tier of grillage beams, it is usually economical to use a rolled steel slab in place of either riveted bases on the columns or of separate cast iron bases.

The size of the slab is usually determined by the outside dimensions of the column and the width of the top tier of grillage beams. In figuring the thickness of the slabs, the assumption of uniform distribution of load made in the case of the grillage beams cannot hold except as to the reaction on the underside of the slab.

The maximum moment in the slab will be along a line practically coincident with the outside lines of the column section.

Slabs

As a direct means of determining the thickness of the distribution slabs, the following formulae may be used.

$t = \sqrt{\frac{3w(B-b)^2}{64,000 AB}}$ for an extreme fiber stress of 16,000 pounds per square inch, in the slab, or

$t = \sqrt{\frac{3w(B-b)^2}{80,000 AB}}$ for an extreme fiber stress of 20,000 pounds per square inch.

In these formulae—

W = Total length of column in pounds.

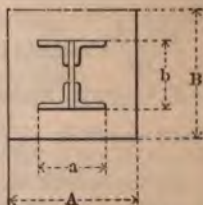
A = Width of slab in inches.

B = Length of slab in inches.

t = Thickness of slab in inches.

a = Outside dimension of column in inches.

b = Inside dimension of column in inches.



As a typical example of the above type of foundation, a column load of 1,080,000 pounds may be assumed with an allowable ground pressure of 7,500 pounds per square foot.

$1,080,000 \div 7,500 = 144$ square feet, so that a foundation 12 ft. \times 12 ft. would give the required area.

Assuming the slab to be 36 inches square and the size of the column at the bottom to be 20" \times 14", and inserting the

Foundation Grillages

Continued

values in the above formulae for thickness of slab, the result is

$$\sqrt{\frac{3 \times 1,080,000 \times 22^2}{80,000 \times 36 \times 36}} = 3 \frac{7}{10} \text{", or say } 3 \frac{3}{4} \text{"} \text{ for thickness of slab.}$$

Grillage Beams

For the top tier of beams, the length of the beams would be 11 ft. The width would correspond to the size of the slab as figured above, or 3 ft. The section modulus required, using formula, $\frac{3W(L-n)}{32,000}$

$$\text{would be } \frac{3 \times 1,080,000 \times 8}{32,000} = 810.$$

By referring to the tables of beam properties, it will be seen that four 24", 105 lb. beams, the section modulus of each being 234.3, would more than equal this requirement, the total section modulus for the four beams being 937.2.

To check these sizes of beams for shear in the web, it is necessary to get the shear in their webs at the edges of the slab. This would be $\frac{1,080,000}{11} \times \frac{11-3}{2} = 392,720 \pi$.

To resist this shear, there are four beam webs, 24" \times .625", or 60 square inches.

$$\frac{392,720}{60} = 6,045 \text{ pounds per square inch.}$$

For security against buckling of the webs under their direct load, there would be $\frac{1,080,000}{4 \times 36 \times .625} = 12,000$ pounds per square inch.

From the table on page 140, it will be noted that the safe buckling load for a 24", 105 lb. beam is 12,350 lbs. per square inch, so the use of these beams may be considered safe.

For the bottom tier of beams, the required section modulus would be, $\frac{3 \times 1,080,000 \times (11-3)}{32,000} = 810$. This requirement would be met by the use of thirteen 15", 50 lb. beams having a section modulus each of 64.5 or 838.5 for the entire number.

Foundation Grillages

Continued

Where columns are to be supported close to party lines it is frequently desirable to use cantilever foundations, by which two or more foundations are combined. In the following example, the lower grillage and slabs are designed in the same manner as for the isolated footing previously mentioned. The cantilever girder would be designed as follows:

Maximum moments are over center of reaction from lower grillage and are equal to column load \times distance center of column to center of grillage. In this case the wall column would cause a moment of $600,000 \times 24 = 14,400,000$ inch pounds. The interior column would cause a moment of $900,000 \times 16 = 14,400,000$ pounds, or the same as for the wall column.

Section modulus required for this cantilever girder would be $14,400,000$

$\frac{16,000}{937.2} = 900$, for which four 24" 105 lb. beams, having a total modulus of 937.2, can be used.

Typical Double Foundations

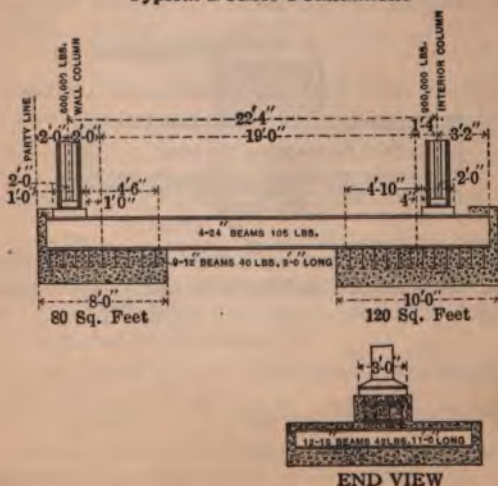


Plate Girders

Plate girders are used to carry heavy loads, or for long spans where beams or rolled sections are inadequate. A plate girder consists of one or more vertical plates called web plates to which are riveted the top and bottom flanges. The function of the flanges is to take the compressive and tensile stresses developed in the outer fibers, while the web is considered to take the shearing stress. A plate girder is sometimes figured by the moment of inertia of its component parts but more frequently by considering the flange stresses as concentrated at the center of gravity of the flanges.

Proportioning Webs

In order to avoid excessive deflection, the width of the web plate is preferably made not less than $1/15$ the clear span. The thickness of web plate depends upon the shear which is greatest at the supports. This thickness must be such that the resistance to shear, computed by multiplying the area of cross-section of web by the safe unit shearing stress, shall be equal to the maximum shear on the girder.

Stiffeners

The distribution of the shear over the web causes compression forces which are assumed to act at angles of 45 degrees with the axis of the girder in the manner indicated by figure on page 224. The web under these compression stresses is subject to failure laterally and the allowable shearing stress must, therefore, be reduced by a column formula. Either the web must be made thick enough not to exceed this allowable stress on a length of $1.414 \times ab$, which is the length on a 45 degree line between the adjacent edges of flange angles, or this unsupported length must be reduced by using stiffeners so spaced as to cut this 45 degree length down to limits which will conform to the allowable shearing stress given by the formula and to the thickness of web which it is desired to use.

A convenient diagram for determining spacing of stiffeners is shown on following page.

EXAMPLE: A plate girder composed of four $6 \times 6 \times \frac{1}{2}$ " angles and one $42 \times \frac{3}{8}$ " web plate has a shear of 90,000 pounds near the end support. Required the spacing of stiffener angles necessary to avoid crippling of the web plate.

The area of web plate = 15.75 square inches.

Shearing stress per square inch = $\frac{90,000}{15.75} = 5,714$ pounds.

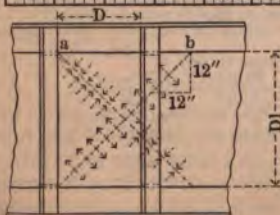
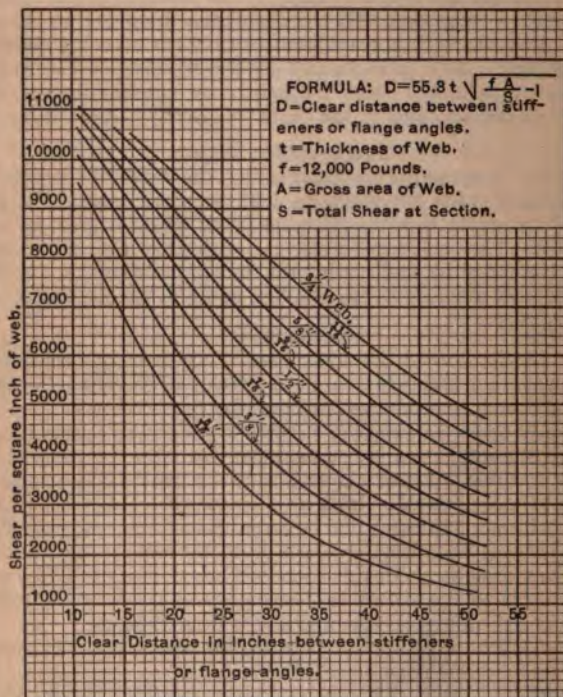
The distance between adjacent edges of flange angles = 30.5 inches.

Referring to the diagram, we locate the horizontal line representing the unit shear of 5,700 pounds, and trace same to its intersection with curve line marked $\frac{3}{8}$ " and follow down along a vertical line from this point of intersection to the bottom line, where the required spacing distance of $21\frac{1}{2}$ " is read.

Plate Girders

Continued

Diagram for Spacing Stiffeners



When $D = D_1$, no stiffeners are required.

Terra Cotta Arches

For Floor Loads of 150 Pounds per Square Foot

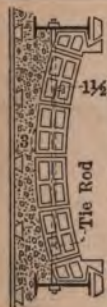
FLAT ARCH



Typical Construction
Bottom of arch below bottom of beam

Depth of Beam, Inches	Depth of Arch, Inches	Depth of Floor, Inches	Limiting Span, Feet	APPROXIMATE WEIGHT, Pounds per Square Foot					
				Steel	Terra Cotta	Concrete	Flooring	Ceiling	Total
6	6	11	5½	6	22	30	4	5	67
7	6	12	5½	7	22	38	4	5	76
8	6	13	5½	8	22	45	4	5	84
7	7	12	6	8	24	30	4	5	71
8	7	13	6	8	24	38	4	5	79
9	7	14	6	8	24	45	4	5	86
8	8	13	6½	8	27	30	4	5	74
9	8	14	6½	8	27	38	4	5	82
10	8	15	6½	8	27	45	4	5	89
9	9	14	7½	8	29	30	4	5	76
10	9	15	7½	9	29	38	4	5	85
12	9	17	7½	9	29	53	4	5	110
10	10	15	8	9	31	30	4	5	79
12	10	17	8	9	31	45	4	5	94
12	12	17	9½	10	35	30	4	5	84
15	12	20	9½	10	35	53	4	5	107
15	15	20	11	12	42	30	4	5	83

SEGMENTAL FLOOR ARCHES



Typical Construction
Top of arch level with top of Beam

Depth of Beam, Inches	Depth of Arch, Inches	Depth of Floor, Inches	Limiting Span, Feet	APPROXIMATE WEIGHT, Pounds per Square Foot					
				Steel	Terra Cotta	Concrete	Flooring	Ceiling	Total
6	4	Rise of Arch about ¾" per ft. of Span	4½	7	20	27	4	5	63
7	4		5	7	20	28	4	5	64
8	4		5½	7	20	29	4	5	65
9	4		6	8	20	30	4	5	67
8	6		5	8	26	27	4	5	70
9	6		5½	8	26	28	4	5	71
10	6		6	9	26	29	4	5	73
12	6		6½	9	26	30	4	5	74
10	8		5½	9	31	27	4	5	76
12	8		6	9	31	28	4	5	77
12	8		6½	10	31	29	4	5	79
15	8		7	10	31	30	4	5	80
12	10		5¾	10	34	27	4	5	80
12	10		6½	11	34	28	4	5	82
15	10		7	11	34	29	4	5	83
15	10		7½	12	34	30	4	5	85

For flat arches on raised skews, where the top of the arch is level with top of floor beams, deduct about 7 pounds per inch of difference between the height of the floor beam and the arch.

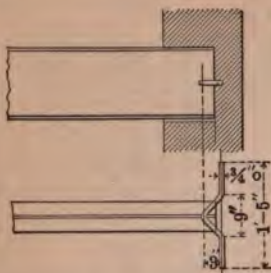
Terra Cotta Partition, Ceiling, Roofing and Furring Blocks

Thickness, Inches	APPROXIMATE WEIGHT, POUNDS PER SQUARE FOOT			
	Partition	Ceiling	Roofing	Furring
1½				9
2	12-14	12		10
3	15-17	20	20	
4	13-19		22	
5	20-23			
6	24-26			
8	28-33			

For tile partitions plastered on both sides, add about 10 pounds per square foot.

Anchors and Tie Rods

Government Anchors



Angle Anchors



1 Bolt Anchor

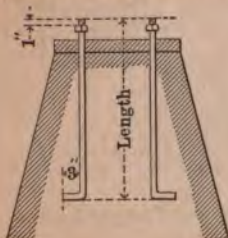
Two 6" \times 4" \times 3/8" Angles 0' 3" Wt. 7 lbs.

2 Bolt Anchor

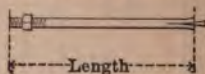
Two 6" \times 4" \times 3/8" Angles 0' 5" Wt. 12 lbs.

Weights include bolts

Anchor Bolts in Foundations



Wedge Bolts



3/4" Bolt 0' 6" lg. Appr. Wt. 1.2 lbs.

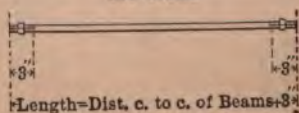
3/4" Bolt 0' 9" lg. Appr. Wt. 1.6 lbs.

7/8" Bolt 0' 9" lg. Appr. Wt. 2.4 lbs.

7/8" Bolt 1' 0" lg. Appr. Wt. 2.9 lbs.

Weights include nuts and wedges.

Tie Rods



Roof Design

The character of the roof to be used on a building is a necessary corollary of the type of structure which is to be covered. On rare occasions, it will pay to put a temporary roof on a permanent structure but it would never pay to put a permanent roof on a temporary structure. A building in which the fire hazard has been reduced by a fire-resisting type of construction should have a roof equally fire-resistant from the inside and from the outside.

For a permanent building a roof should be used, the maintenance cost of which will be low, and which will compare in durability with the building itself. The durability of a roof is measured by its resistance to the effects of wind and weather. A roof for a mill or factory should also be able to resist the gases and moisture frequently produced from operations carried on beneath it. Ample provision should also be made for drainage and it is generally preferable to drain a roof to the outside rather than to drain it to interior points.

The loads to be assumed in designing roofs very properly vary with the location. In regions of heavy snows, and with roofs whose slopes are so flat that snow would be retained, a minimum load per horizontal square foot would probably be about 25 pounds. This should hold for all slopes up to approximately 20 degrees.

For steeper slopes than this, the load maybe reduced in the ratio of about one pound for each degree that the slope is increased up to 45 degrees. For roofs of steeper pitch than this, it is hardly necessary to consider snow load as little snow will rest on a roof of this pitch.

Wind loads, on the other hand, should be assumed as increasing with the pitch of the roof, in place of decreasing, as would be the case with snow loads, and a provision for horizontal wind force of 40 pounds per square foot of vertical surface in exposed locations would in most cases be ample.

For inclined surfaces, it is only necessary to take the component of this wind pressure that is normal to the surface being considered, for which the formula $P_n = P (\sin a) 1.84 \cos a - l$; in which P equals direct horizontal pressure, P_n equals the pressure normal to

Roof Design

Continued

the sloping surface and a the angle of the sloping surface with the horizontal. On an assumption of 30 pounds per square foot, this formula works out to give a normal pressure as per the following table.

Slope a°	Pressure, Pn, per Square Foot, Pounds	Slope a°	Pressure, Pn, per Square Foot, Pounds	Slope a°	Pressure, Pn, per Square Foot, Pounds	Slope a°	Pressure, Pn, per Square Foot, Pounds
5	3.9	20	13.8	35	22.6	50	28.6
10	7.2	25	17.0	40	25.0	55	29.6
15	10.7	30	19.9	45	27.0	60	30.0

It will be noted that for slopes making an angle of over 60 degrees with the horizontal, the pressure normal to the slope is that of a vertical surface.

For climates corresponding to that of our northern states, and where the local building laws do not fix the roof loads to be used, good practice indicates that for roofs where the clear span is not over 100 feet, provision for a total load about as follows is right.

ROOF COVERING		Roof Load per Square Foot, Pounds
Gravel or Composition	{ on boards, flat slope, 1 to 6 or less	50
	{ on boards, steep slope, more than 1 to 6	45
Roofing	{ on 3 inch flat tile or cinder concrete	60
Corrugated sheeting	on boards or purlins	40
Slate	{ on boards or purlins	50
	{ on 3 inch flat tile or cinder concrete	65
Tile on steel purlins		55
Glass		45

In more southern latitudes where snow is not likely to occur, these loads can be safely reduced about 10 pounds per square foot.

For protection against weather the use of tin, gravel, asphalt or similar composition roofing is good for flat roofs, as is slate, tin and tile for steeper pitched roofs. Mill and factory buildings have for years been satisfactorily covered with corrugated sheets.

Roof Design

Continued

The first mentioned above require sheathing to properly support them on rafters or purlins. Corrugated sheets are sometimes placed on sheathing but more frequently are directly attached to the roof purlins.

The weights of these various weather-proofing materials run approximately as follows:

ROOFING MATERIAL	Weight per Square Foot, Pounds
Copper, No. 22 B. W. G.	1½
Corrugated galvanized iron, No. 20 B. W. G.	2¼
Corrugated galvanized iron, No. 26 B. W. G.	1¼
Felt, 2 layers.	½
Felt and asphalt or coal-tar.	2
Glass, ½ inch thick.	1¾
Lath and plaster ceiling.	6-8
Lead, ½ inch thick.	7½
Mackite, 1 inch thick, with plaster.	10
Sheathing, hemlock, 1 inch thick.	2
Sheathing, white pine, spruce, 1 inch thick.	2¼-2½
Sheathing, yellow pine, 1 inch thick.	3½
Shingles, 6x18 inches, 6 inches to weather.	2
Skylight, glass ⅜ to ½ inch, including frame.	4-10
Slag roof, 4-ply, with cement and sand.	4
Slate, ½ inch thick, 3 inch double lap.	4½
Slate, ⅜ inch thick, 3 inch double lap.	6¾
Terneplate, IC.	1½
Terneplate, IX.	¾
Tiles (plain), 10½x6¼x5½ inches, 5¼ inches to weather.	18
Tiles (Spanish), 14½x10½ inches, 7¼ inches to weather.	8½
Zinc, No. 20 B. W. G.	1½

Where flat roofs are used on spans up to 45 feet, it is frequently economical to carry the roof on beams. This is not possible where the spans exceed this limit and it then becomes necessary to use trusses, the total load on the roof being usually considered as uniformly distributed, although, with steep pitched roofs, it will be necessary to make a special analysis of the stresses due to the unequal loading of the trusses from wind pressure.

In placing purlins on roof trusses, it is always advisable to place them on the panel points of the truss, as this obviates local stresses in the chords due to bending, which will always occur when purlins are placed other than at panel points.

Roof Design

Continued

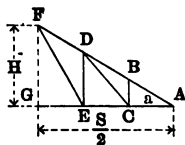
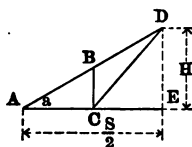
The maximum spacing of purlins will depend on the strength of the sheathing or corrugated sheets used for the direct support of the roof. With corrugated sheets the usual spacing is about 5 feet, while with 2" sheathing it is frequently possible to get 8 to 10 feet spacing of purlins.

The approximate weight of roof trusses which it is frequently convenient to know for purposes of preliminary design, can be determined by the formula $\frac{L}{20} + \frac{12}{l}$ = weight of truss in pounds per horizontal square foot. In this formula, L equals the span, and l equals the distance center to center of trusses.

This is based on 40 pounds per square foot total load and where loads exceed this amount, the weight of the truss can be increased in direct proportion as the load exceeds this amount.

Trusses

Formulae for Stresses and Coefficients



$$n = \frac{s}{H} = 2 \cot a$$

PRATT TRUSS—4 Panels

Member	Stress	Length
AB, BD	$+ \frac{1}{4} \sqrt{n^2 + 4} \times W$	$\frac{1}{4} S \sec a$
AC	$- \frac{1}{4} n \times W$	$\frac{1}{4} S$
CE	$- \frac{1}{4} n \times W$	$\frac{1}{4} S$
BC	$+ 1 \times W$	$\frac{1}{4} H$
CD	$- \frac{1}{4} \sqrt{n^2 + 16} \times W$	$\frac{1}{4} \sqrt{S^2 + 16 H^2}$

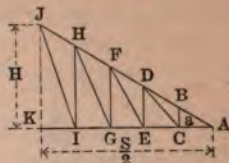
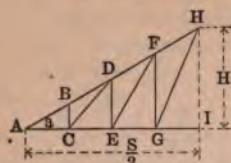
PRATT TRUSS—6 Panels

Member	Stress	Length
AB, BD	$+ \frac{5}{4} \sqrt{n^2 + 4} \times W$	$\frac{1}{6} S \sec a$
DF	$+ \sqrt{n^2 + 4} \times W$	$\frac{1}{6} S \sec a$
AC	$- \frac{5}{4} n \times W$	$\frac{1}{6} S$
CE	$- n \times W$	$\frac{1}{6} S$
EG	$- \frac{3}{4} n \times W$	$\frac{1}{6} S$
BC	$+ 1 \times W$	$\frac{1}{6} H$
DE	$+ \frac{3}{2} \times W$	$\frac{1}{6} H$
CD	$- \frac{1}{4} \sqrt{n^2 + 16} \times W$	$\frac{1}{6} \sqrt{S^2 + 16 H^2}$
EF	$- \frac{1}{4} \sqrt{n^2 + 32} \times W$	$\frac{1}{6} \sqrt{S^2 + 36 H^2}$

Trusses

Continued

Formulae for Stresses and Coefficients



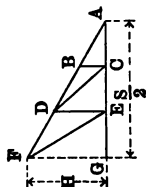
$$n = \frac{S}{H} = 2 \cot \alpha$$

PRATT TRUSS—8 Panels

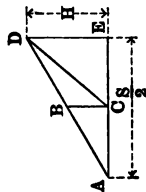
Member	Stress	Length
AB, BD	$+7/4 \sqrt{n^2 + 4} \times W$	$3/8 S \sec \alpha$
DF	$+3/2 \sqrt{n^2 + 4} \times W$	$3/8 S \sec \alpha$
FH	$+5/4 \sqrt{n^2 + 4} \times W$	$3/8 S \sec \alpha$
AC	$-7/4 n \times W$	$3/8 S$
CE	$-3/2 n \times W$	$3/8 S$
EG	$-5/4 n \times W$	$3/8 S$
GI	$-n \times W$	$3/8 S$
BC	$+1 \times W$	$3/8 H$
DE	$+3/2 \times W$	$3/8 H$
FG	$+2 \times W$	$3/8 H$
CD	$-1/4 \sqrt{n^2 + 16} \times W$	$3/8 \sqrt{S^2 + 16 H^2}$
EF	$-1/4 \sqrt{n^2 + 36} \times W$	$3/8 \sqrt{S^2 + 36 H^2}$
GH	$-1/4 \sqrt{n^2 + 64} \times W$	$3/8 \sqrt{S^2 + 64 H^2}$

PRATT TRUSS—10 Panels

Member	Stress	Length
AB, BD	$+9/4 \sqrt{n^2 + 4} \times W$	$1/10 S \sec \alpha$
DF	$+2 \sqrt{n^2 + 4} \times W$	$1/10 S \sec \alpha$
FH	$+7/4 \sqrt{n^2 + 4} \times W$	$1/10 S \sec \alpha$
HJ	$+3/2 \sqrt{n^2 + 4} \times W$	$1/10 S \sec \alpha$
AC	$-9/4 n \times W$	$1/10 S$
CE	$-2 n \times W$	$1/10 S$
EG	$-7/4 n \times W$	$1/10 S$
GI	$-3/2 n \times W$	$1/10 S$
IK	$-5/4 n \times W$	$1/5 S$
BC	$+1 \times W$	$1/5 H$
DE	$+3/2 \times W$	$2/5 H$
FG	$+2 \times W$	$3/5 H$
HI	$+5/2 \times W$	$4/5 H$
CD	$-1/4 \sqrt{n^2 + 16} \times W$	$1/10 \sqrt{S^2 + 16 H^2}$
EF	$-1/4 \sqrt{n^2 + 32} \times W$	$1/10 \sqrt{S^2 + 36 H^2}$
GH	$-1/4 \sqrt{n^2 + 64} \times W$	$1/10 \sqrt{S^2 + 64 H^2}$
IJ	$-1/4 \sqrt{n^2 + 100} \times W$	$1/10 \sqrt{S^2 + 100 H^2}$



Trusses
Continued
Coefficients of Stresses

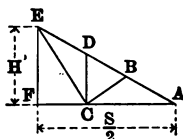
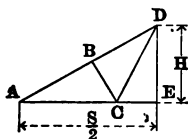


Member	n = Span + Height = 2 cot a						n = Span + Height = 2 cot a					
	3	$\frac{24}{7}$	2 cot 30°	4	$\frac{24}{5}$	6	3	$\frac{24}{7}$	2 cot 30°	4	$\frac{24}{5}$	6
AB, BD	2.70	2.98	3.00	3.35	3.90	4.74	4.51	4.96	5.00	5.59	6.50	7.91
AC	2.25	2.57	2.60	3.00	3.60	4.50	3.61	3.97	4.00	4.47	5.20	6.32
CE	1.50	1.71	1.73	2.00	2.40	3.00	3.75	4.29	4.33	5.00	6.00	7.50
BC	1.00	1.00	1.00	1.00	1.00	1.00	3.00	3.43	3.46	4.00	4.80	6.00
CD	1.25	1.32	1.32	1.41	1.56	1.80	2.25	2.57	2.60	3.00	3.60	4.50
							1.00	1.00	1.00	1.00	1.00	1.00
							1.50	1.50	1.50	1.50	1.50	1.50
							1.25	1.32	1.32	1.41	1.56	1.80
							1.68	1.73	1.73	1.80	1.92	2.12

Trusses

Continued

Formulae for Stresses and Lengths



$$n = \frac{S}{H} = 2 \cot a$$

SIMPLE FINK TRUSS

Member	Stress	Length
AB	$+\frac{3}{4} \frac{\sqrt{n^2+4}}{1} \times W$	$\frac{1}{4} L \sec a$
BD	$+\frac{1}{\sqrt{n^2+4}} (\frac{3}{4} n^2 + 1) \times W$	$\frac{1}{4} L \sec a$
AC	$-\frac{3}{4} n \times W$	$\frac{1}{4} L \sec^2 a$
CE	$-\frac{1}{4} n \times W$	$L (1 - \frac{1}{4} \sec^2 a)$
BC	$+\frac{n}{\sqrt{n^2+4}} \times W$	$\frac{1}{4} L \sec a \tan a$
CD	$-\frac{1}{4} n \times W$	$\frac{1}{4} L \sec^2 a$

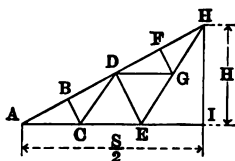
SIMPLE FAN TRUSS

Member	Stress	Length
AB	$+\frac{1}{\sqrt{n^2+4}} (5/4 n^2 + 5) \times W$	$\frac{1}{6} L \sec a$
BD	$+\frac{1}{2 \sqrt{n^2+4}} 13/6 (n^2 + 6) \times W$	$\frac{1}{6} L \sec a$
DE	$+\frac{1}{\sqrt{n^2+4}} (5/4 n^2 + 1) \times W$	$\frac{1}{6} L \sec a$
AC	$-\frac{5}{4} n \times W$	$\frac{1}{4} L \sec^2 a$
CF	$-\frac{1}{4} n \times W$	$L (1 - \frac{1}{4} \sec^2 a)$
BC, CD	$+n \sqrt{n^4 + 40 n^2 + 144} \times W$	$+\frac{1}{4} L \sqrt{\frac{\sec^2 a + \sec^2 a \tan^2 a}{9}}$
CE	$-\frac{1}{4} n \times W$	$\frac{1}{4} L \sec^2 a$

Trusses

Continued

Formulae for Stresses and Lengths



$$n = \frac{S}{H} = 2 \cot a$$

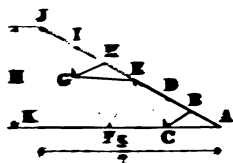
COMPOUND FINK TRUSS

Member	Stress	Length
AB	$+ \frac{7/4 \sqrt{n^2 + 4}}{1} \times W$	$\frac{1}{4} L \sec a$
BD	$+ \frac{1}{\sqrt{n^2 + 4}} (7/4 n^2 + 5) \times W$	$\frac{1}{4} L \sec a$
DF	$+ \frac{1}{\sqrt{n^2 + 4}} (7/4 n^2 + 3) \times W$	$\frac{1}{4} L \sec a$
FH	$+ \frac{1}{\sqrt{n^2 + 4}} (7/4 n^2 + 1) \times W$	$\frac{1}{4} L \sec a$
AC	$- \frac{7/4 n}{\sqrt{n^2 + 4}} \times W$	$\frac{1}{4} L \sec^3 a$
CE	$- \frac{3/2 n}{\sqrt{n^2 + 4}} \times W$	$\frac{1}{4} L \sec^3 a$
EI	$- \frac{n}{\sqrt{n^2 + 4}} \times W$	$L (1 - \frac{1}{4} \sec^3 a)$
BC, FG	$+ \frac{n}{\sqrt{n^2 + 4}} \times W$	$\frac{1}{4} L \sec a \tan a$
DE	$+ \frac{1}{\sqrt{n^2 + 4}} \times W$	$\frac{1}{4} L \sec a \tan a$
CD, DG	$- \frac{1/4 n}{\sqrt{n^2 + 4}} \times W$	$\frac{1}{4} L \sec^3 a$
EG	$- \frac{1/2 n}{\sqrt{n^2 + 4}} \times W$	$\frac{1}{4} L \sec^3 a$
GH	$- \frac{1/4 n}{\sqrt{n^2 + 4}} \times W$	$\frac{1}{4} L \sec^3 a$

Index

Continued

Remember for Stresses and Lengths



$$R = \frac{E}{H} = 2 \cos \alpha$$

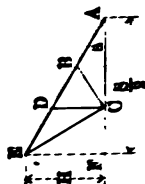
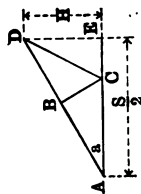
COMPOUND FAN TRUSS

Member	Stress	Length
AB	$+ \frac{1}{\sqrt{n^2 + 4}} (11/4 n^2 + 11) \times W$	$1/12 L \sec \alpha$
BD	$+ \frac{1}{\sqrt{n^2 + 4}} (31/12 n^2 + 9) \times W$	$1/12 L \sec \alpha$
DE	$+ \frac{1}{\sqrt{n^2 + 4}} (11/4 n^2 + 7) \times W$	$1/12 L \sec \alpha$
EH	$+ \frac{1}{\sqrt{n^2 + 4}} (11/4 n^2 + 5) \times W$	$1/12 L \sec \alpha$
HI	$+ \frac{1}{\sqrt{n^2 + 4}} (31/12 n^2 + 3) \times W$	$1/12 L \sec \alpha$
IJ	$+ \frac{1}{\sqrt{n^2 + 4}} (11/4 n^2 + 1) \times W$	$1/12 L \sec \alpha$
AC	$- \frac{11}{4} n \times W$	$\frac{1}{4} L \sec^2 \alpha$
CF	$- \frac{9}{4} n \times W$	$\frac{1}{4} L \sec^2 \alpha$
FK	$- \frac{3}{2} n \times W$	$L (1 - \frac{1}{4} \sec^2 \alpha)$
BC, CD GH, GI	$\left. \begin{aligned} &+ \frac{n \sqrt{n^4 + 40 n^2 + 144}}{6 (n^2 + 4)} \times W \\ &\quad \frac{3 n}{3 n} \times W \end{aligned} \right\}$	$\frac{1}{4} L \sqrt{\frac{\sec^2 \alpha}{9} + \sec^2 \alpha \tan^2 \alpha}$
EF	$+ \frac{\sqrt{n^2 + 4}}{3 n} \times W$	$\frac{1}{4} L \sec \alpha \tan \alpha$
CE, EG	$- \frac{1}{4} n \times W$	$\frac{1}{4} L \sec^2 \alpha$
FG	$- \frac{1}{4} n \times W$	$\frac{1}{4} L \sec^2 \alpha$
GJ	$- \frac{5}{4} n \times W$	$\frac{1}{4} L \sec^2 \alpha$

Trusses
Continued
Coefficients for Calculating Strength of Truss Members

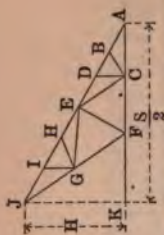
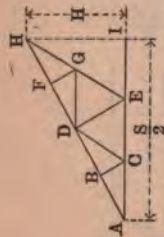
Continued from pages 236 and 237

	3	24/7	2 cot 30°	4	24/5	5	6
Values of n							
Values of a	33° 41' 24"	30° 15' 23"	30°	26° 33' 54"	22° 37' 12"	21° 48' 5"	18° 26' 6"
Sec a	1.2018	1.1577	1.1547	1.1180	1.0833	1.0770	1.0541
Sec ² a	1.4444	1.3403	1.3333	1.2500	1.1736	1.1600	1.1111
Sec a tan a	0.8012	0.6753	0.6667	0.5590	0.4514	0.4308	0.3514
$\sqrt{\frac{\sec^2 a}{9} + \sec^2 a \tan^2 a}$	0.8958	0.7778	0.7698	0.6718	0.5781	0.5608	0.4969



Trusses
Continued
Coefficients of Stresses

Members	n = Span + Height = 2 cot α							Members	n = Span + Height = 2 cot α						
	3	$\frac{2A}{7}$	2 cot 30°	4	$\frac{2A}{5}$	5	6		3	$\frac{2A}{7}$	2 cot 30°	4	$\frac{2A}{5}$	5	6
AB	2.70	2.98	3.00	3.35	3.90	4.04	4.74	AB	4.51	4.98	5.00	5.50	6.50	6.73	7.01
BD	2.15	2.47	2.50	2.91	3.52	3.67	4.43	BD	3.54	3.96	4.00	4.55	5.38	5.60	6.04
AC	2.25	2.57	2.60	3.00	3.60	3.75	4.50	DC	3.40	3.95	4.00	4.70	5.73	5.90	7.27
CE	1.50	1.71	1.73	2.00	2.40	2.50	3.00	AC	3.75	4.30	4.33	5.00	6.00	6.25	7.50
BC	0.83	0.86	0.87	0.89	0.92	0.93	0.95	CF	2.25	2.57	2.60	3.00	3.60	3.75	4.50
CD	0.75	0.86	0.87	1.00	1.20	1.25	1.50	CB, CD	0.93	0.99	1.00	1.08	1.18	1.21	1.34
								CE	1.50	1.71	1.73	2.00	2.40	2.50	3.00



Trusses

Continued

Coefficients of Stresses

Member	n = Span ÷ Height = 2 cot α						n = Span ÷ Height = 2 cot α					
	3	$\frac{24}{7}$	2 cot 30°	4	$\frac{24}{5}$	6	3	$\frac{24}{7}$	2 cot 30°	4	$\frac{24}{5}$	6
AB	6.31	6.95	7.00	7.83	9.10	9.42	9.92	10.91	11.00	12.30	14.30	17.39
BD	5.76	6.44	6.50	7.38	8.72	9.05	8.95	9.91	10.00	11.25	13.18	16.13
DF	5.20	5.94	6.00	6.93	8.33	8.68	8.81	9.91	10.00	11.40	13.53	16.76
FH	4.65	5.43	5.50	6.48	7.95	8.31	8.25	9.40	9.50	10.96	13.15	16.44
AC	5.25	6.00	6.07	7.00	8.40	8.75	7.28	8.41	8.50	9.91	12.02	15.18
CE	4.50	5.14	5.20	6.00	7.20	7.50	7.14	8.40	8.50	10.06	12.38	15.93
CI	3.00	3.43	3.46	4.00	4.80	5.00	8.25	9.43	9.53	11.00	13.20	16.50
BC, FG	0.83	0.86	0.87	0.89	0.92	0.93	6.75	7.71	7.79	9.00	10.80	13.50
DE	1.66	1.73	1.73	1.79	1.85	1.86	4.50	5.14	5.20	6.00	7.20	9.00
CD, DG	0.75	0.86	0.87	1.00	1.20	1.25	0.93	0.99	1.00	1.08	1.18	1.34
EG	1.50	1.71	1.73	2.00	2.40	2.50	2.50	2.59	2.60	2.68	2.77	2.85
GH	2.25	2.57	2.60	3.00	3.60	3.75	1.50	1.71	1.73	2.00	2.40	3.00
							2.25	2.57	2.60	3.00	3.60	4.50
							3.75	4.29	4.33	5.00	6.00	7.50

JONES & LAUGHLIN STEEL COMPANY

Compression Formulae

Comparison of Allowable Unit Stresses in Pounds per Square

	A.R.E. Assn. Chicago Used by J. & L. S. Co.	Gordon	New York	Philadelphia	Boston	Pitt
$\frac{l}{r}$	$\frac{l}{r}$ $16000-70\frac{l}{r}$ 14000 Max.	$\frac{l}{r^2}$ $1+\frac{36000}{r^2}$	$\frac{l}{r}$ $15200-58\frac{l}{r}$	$\frac{l}{r^2}$ $1+\frac{11000}{r^2}$	$\frac{l}{r^2}$ $1+\frac{20000}{r^2}$	
0	14000	12500	15200	16250	16000	13
5	14000	12490	14910	16215	15980	13
10	14000	12460	14620	16100	15920	13
15	14000	12420	14330	15925	15820	13
20	14000	12365	14040	15680	15690	13
25	14000	12285	13750	15375	15515	13
30	13900	12195	13460	15020	15310	13
35	13550	12090	13170	14620	15075	13
40	13200	11970	12880	14185	14815	13
45	12850	11835	12590	13725	14530	13
50	12500	11690	12300	13240	14220	13
55	12150	11530	12010	12745	13900	13
60	11800	11365	11720	12240	13560	13
65	11450	11185	11430	11740	13210	12
70	11100	11000	11140	11240	12850	12
75	10750	10810	10850	10750	12490	11
80	10400	10615	10560	10275	12120	11
85	10050	10410	10270	9810	11755	10
90	9700	10205	9980	9360	11390	10
95	9350	9995	9690	8930	11025	9
100	9000	9785	9400	8510	10670	9
105	8650	9570	9110	8115	10315	8
110	8300	9355	8820	7740	9970	8
115	7950	9140	8530	7380	9630	7
120	7600	8930	8240	7035	9300	7
125	7250	8715	6715	6

EXPLANATION OF HEADINGS

J. & L. S. Co.—Jones & Laughlin Steel Company.

A. R. E. Assn.—American Railway Engineering Association.

Cities—Building Laws.

Unit stresses given below heavy line are not found by formula given.

Continued on next page.

Compression Formulae

Continued

Comparison of Allowable Unit Stresses in Pounds Per Square Inch

$\frac{l}{r}$	A.R.E. Assn. Chicago Used by J. & L. S. Co.	Gordon	New York	Philadelphia	Boston	Pittsburgh
	$\frac{l}{r}$ $\frac{16000-70}{r}$ 14000 Max.	$\frac{12500}{l^2}$ $1+\frac{36000}{r^2}$	$\frac{15200-58}{r}$	$\frac{16250}{l^2}$ $1+\frac{11000}{r^2}$	$\frac{16000}{l^2}$ $1+\frac{20000}{r^2}$	$\frac{19000-100}{r}$ 13000 Max.
130	6900	8510	6405	6500
135	6550	8300	6115	6250
140	6200	8095	5840	6000
145	5850	7890	5750
150	5500	7690	5500
155	7495
160	7305
165	7120
170	6935
175	6755
180	6580
185	6410
190	6240
195	6080
200	5920

EXPLANATION OF HEADINGS

J. & L. S. Co.—Jones & Laughlin Steel Company.

A. R. E. Assn.—American Railway Engineering Association.

Cities—Building Laws.

Unit stresses given below heavy line are not found by formula given.

Floors and Roofs

Minimum Live Loads, Pounds per Square Foot

By Building Laws of Various Cities

KIND OF BUILDING	Boston, 1912	New York, 1906	Philadelphia, 1913	Baltimore, 1908	Pittsburgh, 1913	Cleveland, 1911	Chicago, 1911	St. Louis, 1910	San Francisco, 1910
Apartments.....	50	60	70	60	50	50	40	60	60
Public Rooms* and Halls.....	100	80
Assembly Halls.....	125	90	120	...	125	100	...	100	125
Fixed Seat Auditoriums.....	75	125	80	100	...	75
Movable Seat Auditoriums.....	125	...	100	100	...	125
Churches.....	...	90	...	75	125	...	100	...	125
Dance Halls.....	200	150	150	100
Drill Rooms.....	200	150
Riding Schools.....	200	150
Theaters.....	...	90	...	75	125	...	100	...	125
Dwellings.....	50	60	70	60	50	40	40	60	60
Public Rooms*.....	100
Hotels.....	50	60	70	60	70	50	50	60	60
First Floors.....	100	...
Corridors.....	80
Office Floors.....	100	80
Public Rooms*.....	100
Manufacturing.....	125	120	120	125	125	...	100	...	125
Light Factories.....	...	120	150	...	125	150	...
Mercantile.....
Heavy Storehouses.....	...	150	150	250	200	200	250
Retail Stores.....	125	...	120	125	125	125	100	150	125
Warehouses.....	250	150	150	...	200	...	100	150	250
Offices.....	100	75	100	75	70	60	50	70	60
First Floor.....	100	150	...	150	150	150
Corridors.....	100
Schools (Class Rooms).....	60	75	...	75	70	60	40	100	75
Assembly Rooms—Halls.....	125	90	70	80	75	...	125
Sidewalks.....	...	300	...	200	...	200	150
Stables—Carriage Houses.....	...	75	...	100	...	80	100	...	75
Area less than 500 sq. ft.....	40
Stairways and Landings.....	70	80	100
Fire Escapes.....	70	80
Roofs—Flat.....	40	50	...	40	\$50	40	25	40	30
Horizontal Projection Steep Roofs.....	...	30	...	20	\$50	...	25	...	20
Superficial Surface.....	30	...	\$50	40
Wind Pressure.....	...	30	30	30	25	30	20	30	20

*Area greater than 500 square feet.

†First floors 200.

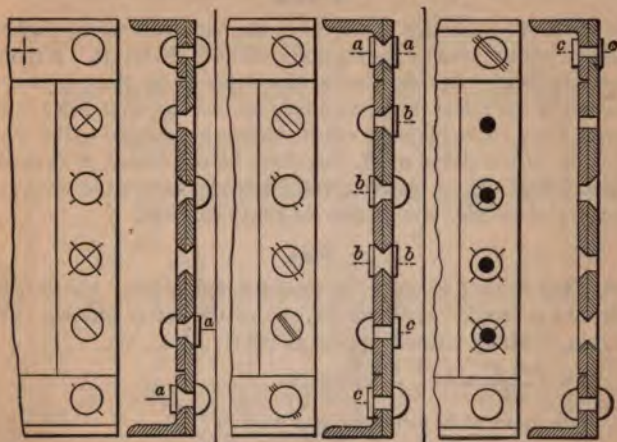
‡Slopes less than 20 degrees.

§Dead and live, except for one story steel frame buildings, corrugated iron roofs, 35 pounds.

||High buildings, built up districts, 35 pounds; 14 stories or over, 25 pounds at tenth story, 2 ½ pounds less each story below.

Figures for manufacturing establishments do not include machinery.

Conventional Signs for Riveting



Maximum height of heads marked $a = \frac{3}{8}"$

" " " " " $b = \frac{1}{4}"$

" " " " " $c = \frac{3}{8}"$

Two full heads

+ or

Shop

Field

Countersunk and chipped other side (or side not visible)

Countersunk and chipped this side (or side visible)

Countersunk and chipped both sides

Other side
(Not Visible)

This side
(Visible)

Both
Sides

Countersunk but not chipped limit $\frac{1}{8}"$ high

Flattened head $\frac{1}{4}"$ high and countersunk



Flattened head $\frac{1}{4}"$ high and not countersunk

Stresses in Rivets and Pins

Rivets

It is common practice to disregard the friction between plates in a riveted joint caused by the clamping effect of the rivets. A riveted joint may fail by the shearing of the rivets or by the crippling or crushing of the metal in the members around the rivet holes. The bearing value of the plates or rolled sections in addition to the shearing value of the rivets must, therefore, be considered in designing riveted joints. If the shearing value exceeds the bearing value, the latter will determine the number of rivets required.

Pins

Pins are subject to shearing, bending and bearing stresses, but their size is mostly governed by one of the latter stresses. The following bending formula applies to pins:

$$M = \frac{f \pi d^3}{32} = \frac{f A d}{8}, \text{ in which}$$

M = moment of forces for any section

f = extreme fiber stress at that section

A = area of section

d = diameter of pin

π = 3.14159

The forces are assumed as acting in a plane through the axis of the pin.

EXAMPLE 1.

A bolster or end shoe of a bridge carries a load of 100,000 pounds; assume the distance between points (i. e.) centers of support of bolster plates and center of post plates $2\frac{1}{2}"$. Bending moment = $50,000 \times 2\frac{1}{2}" = 125,000$ inch pounds; therefore, for $f = 20,000$;

$$d = \sqrt[3]{\frac{125,000 \times 32}{20,000 \times 3.14}} = 3.994" \text{ or } 4 \text{ inch pin.}$$

EXAMPLE 2.

Required the bearing in shoe for a 4" pin, transmitting a load of 100,000 pounds at 20,000 pounds pressure per square inch. The bearing value of a 4 inch pin for 1 inch thickness is $= 4 \times 20,000 = 80,000$ pounds. Therefore, the thickness of metal required = $\frac{100,000}{20,000} = 1\frac{1}{4}$ inches, or each web of the shoe must be $\frac{5}{8}$ inch

including pin plates.

Riveted Plates, Bars and Angles Area To Be Deducted for One Hole

THICKNESS OF PLATE, BAR OR ANGLE

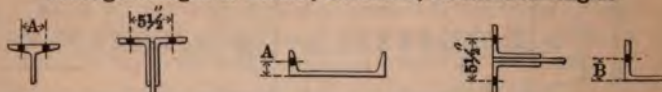
Size of Hole	$\frac{1}{8}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$
$\frac{9}{16}$.07	.11	.14	.18	.21	.25	.28	.32	.35
$\frac{5}{8}$.08	.12	.16	.20	.23	.27	.31	.35	.39
$\frac{1}{2}$.09	.13	.17	.21	.26	.30	.34	.39	.43
$\frac{3}{4}$.10	.14	.19	.23	.28	.33	.38	.42	.47
$\frac{7}{8}$.10	.15	.20	.25	.30	.36	.41	.46	.51
$\frac{1}{8}$.11	.16	.22	.27	.33	.38	.44	.49	.55
$\frac{1}{4}$.12	.18	.23	.29	.35	.41	.47	.53	.59
$\frac{3}{8}$.13	.19	.25	.31	.38	.44	.50	.56	.63
$\frac{1}{2}$.14	.20	.27	.33	.40	.46	.53	.60	.66
$\frac{5}{8}$.15	.21	.28	.35	.42	.49	.56	.63	.70

THICKNESS OF PLATE, BAR OR ANGLE

Size of Hole	$\frac{1}{16}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	1	$1\frac{1}{16}$	$1\frac{1}{8}$
$\frac{9}{16}$.39	.42	.46	.53	.59	.63	.56	.60	.63
$\frac{5}{8}$.43	.47	.51	.59	.64	.69	.63	.66	.70
$\frac{1}{2}$.47	.52	.56	.64	.70	.75	.69	.73	.77
$\frac{3}{4}$.52	.56	.61	.66	.71	.81	.75	.80	.84
$\frac{7}{8}$.56	.61	.66	.71	.77	.88	.81	.86	.91
$\frac{1}{8}$.60	.66	.71	.76	.82	.93	.88	.93	.98
1	.64	.70	.76	.82	.88	.94	.94	1.00	1.05
$1\frac{1}{16}$.69	.75	.81	.88	.94	1.00	1.00	1.06	1.13
$1\frac{1}{8}$.73	.80	.86	.93	.98	1.05	1.06	1.13	1.20
$1\frac{1}{4}$.77	.84	.91	.98	.98	1.05	1.13	1.20	1.27

Standard Spacing and Dimensions of Rivet and Bolt Holes

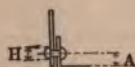
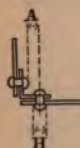
Through Flanges of Beams, Channels, Connection Angles



STEEL BEAMS				STEEL CHANNELS				ANGLES		
Depth in Inches	Weight per Foot, Pounds	Diameter of Bolt or Rivet, In.	Inches, A	Depth in Inches	Weight per Foot, Pounds	Diameter of Bolt or Rivet, In.	Inches, A	Depth of Leg, Inches	Maximum Diameter of Bolt or Rivet, Inches	Inches, B
24	105.	3/4	4 1/2	15	45.	3/4	2 1/4	8	1
24	80.	3/4	4	15	33.	3/4	1 7/8			
20	80.	3/4	4	12	30.	3/4	2	7	1
20	65.	3/4	3 1/2	12	20.5	3/4	1 3/4			
18	55.	3/4	3 1/4	10	25.	3/4	2	6	1	3 1/2
15	60.	3/4	3 1/4	10	15.	3/4	1 1/2			
15	42.	3/4	3	9	20.	3/4	1 3/4	5	1	2 3/4
12	40.	3/4	3	9	13.25	3/4	1 3/8			
12	31.5	3/4	2 3/4	8	16.25	3/4	1 1/2	4 1/2	1	2 1/2
10	25.	3/4	2 5/8	8	11.25	3/4	1 1/4			
9	21.	3/4	2 1/2	7	17.25	3/4	1 1/2	4	1	2 1/4
8	18.	3/4	2 1/4	7	9.75	3/4	1 1/4			
7	15.	5/8	2 1/4	6	13.	5/8	1 3/8	3 1/2	1	2
6	12.25	5/8	2	6	8.	5/8	1 1/8			
5	9.75	1/2	1 3/4	5	9.	1/2	1 1/4	3	7/8	1 3/4
4	7.5	1/2	1 1/2	5	6.5	1/2	1			
3	5.5	3/8	1 1/8	4	5.25	1/2	1	2 1/2	3/4	1 3/8
.....	3	4.	3/8	1 1/8			
				SHIP CHANNELS				2	5/8	1 1/8
				13	31.5	3/4	2 1/4	1 1/2	1/2	1 1/8
				10	21.8	3/4	2	1	3/8	3/8
				9	28.6	3/4	2 1/4			
				8	23.8	3/4	2 1/4			
				8	21.4	3/4	2 1/4			
				7	18.	3/4	2			
				6	13.3	3/4	1 3/4			
				6	15.	3/4	1 3/4			

Minimum Rivet Spacing

		VALUES OF "X" FOR VARYING VALUES OF A AND B																			
		Values of B	VALUES OF A																		
			$\frac{7}{8}$	1	$1\frac{1}{8}$	$1\frac{1}{4}$	$1\frac{3}{8}$	$1\frac{1}{2}$	$1\frac{5}{8}$	$1\frac{3}{4}$	$1\frac{7}{8}$	2	$2\frac{1}{8}$	$2\frac{1}{4}$	$2\frac{3}{8}$	$2\frac{1}{2}$	$2\frac{5}{8}$	$2\frac{3}{4}$	$2\frac{7}{8}$	3	
C	$\frac{1}{16}$	$1\frac{1}{8}$	$1\frac{7}{16}$	$1\frac{1}{2}$	$1\frac{9}{16}$	$1\frac{11}{16}$	$1\frac{3}{4}$	$1\frac{7}{8}$	2	$2\frac{1}{16}$	$2\frac{3}{16}$	$2\frac{5}{16}$	$2\frac{7}{16}$	$2\frac{9}{16}$	$2\frac{11}{16}$	$2\frac{13}{16}$	$2\frac{15}{16}$	$2\frac{17}{16}$	$2\frac{19}{16}$	$2\frac{21}{16}$	
	$\frac{1}{8}$	$1\frac{1}{4}$	$1\frac{9}{16}$	$1\frac{5}{8}$	$1\frac{11}{16}$	$1\frac{3}{4}$	$1\frac{7}{8}$	$1\frac{15}{16}$	$2\frac{1}{16}$	$2\frac{1}{8}$	$2\frac{1}{4}$	$2\frac{3}{8}$	$2\frac{1}{2}$	$2\frac{5}{8}$	$2\frac{3}{4}$	$2\frac{7}{8}$	$2\frac{9}{8}$	$2\frac{11}{8}$	$2\frac{13}{8}$	$2\frac{15}{8}$	
	$\frac{3}{16}$	$1\frac{3}{8}$	$1\frac{11}{16}$	$1\frac{3}{4}$	$1\frac{7}{8}$	$1\frac{15}{16}$	2	$2\frac{1}{8}$	$2\frac{3}{8}$	$2\frac{5}{8}$	$2\frac{7}{8}$	$2\frac{9}{8}$	$2\frac{11}{8}$	$2\frac{13}{8}$	$2\frac{15}{8}$	$2\frac{17}{8}$	$2\frac{19}{8}$	$2\frac{21}{8}$	$2\frac{23}{8}$	$2\frac{25}{8}$	
D	$\frac{1}{4}$	$1\frac{1}{2}$	$1\frac{13}{16}$	$1\frac{7}{8}$	$1\frac{15}{16}$	2	$2\frac{1}{8}$	$2\frac{3}{8}$	$2\frac{5}{8}$	$2\frac{7}{8}$	$2\frac{9}{8}$	$2\frac{11}{8}$	$2\frac{13}{8}$	$2\frac{15}{8}$	$2\frac{17}{8}$	$2\frac{19}{8}$	$2\frac{21}{8}$	$2\frac{23}{8}$	$2\frac{25}{8}$	3	
	$\frac{5}{16}$	$1\frac{5}{8}$	$1\frac{13}{16}$	$1\frac{7}{8}$	2	$2\frac{1}{16}$	$2\frac{1}{8}$	$2\frac{3}{8}$	$2\frac{5}{8}$	$2\frac{7}{8}$	$2\frac{9}{8}$	$2\frac{11}{8}$	$2\frac{13}{8}$	$2\frac{15}{8}$	$2\frac{17}{8}$	$2\frac{19}{8}$	$2\frac{21}{8}$	$2\frac{23}{8}$	$2\frac{25}{8}$	$3\frac{1}{8}$	
	$\frac{3}{8}$	$1\frac{3}{4}$	$1\frac{15}{16}$	2	$2\frac{1}{16}$	$2\frac{1}{8}$	$2\frac{3}{8}$	$2\frac{5}{8}$	$2\frac{7}{8}$	$2\frac{9}{8}$	$2\frac{11}{8}$	$2\frac{13}{8}$	$2\frac{15}{8}$	$2\frac{17}{8}$	$2\frac{19}{8}$	$2\frac{21}{8}$	$2\frac{23}{8}$	$2\frac{25}{8}$	$3\frac{1}{8}$	$3\frac{3}{8}$	
E	$\frac{7}{16}$	$1\frac{7}{8}$	$2\frac{1}{16}$	$2\frac{1}{8}$	$2\frac{3}{8}$	$2\frac{5}{8}$	$2\frac{7}{8}$	$2\frac{9}{8}$	$2\frac{11}{8}$	$2\frac{13}{8}$	$2\frac{15}{8}$	$2\frac{17}{8}$	$2\frac{19}{8}$	$2\frac{21}{8}$	$2\frac{23}{8}$	$2\frac{25}{8}$	$3\frac{1}{8}$	$3\frac{3}{8}$	$3\frac{5}{8}$	$3\frac{7}{8}$	
	$\frac{1}{2}$	$2\frac{1}{8}$	$2\frac{3}{8}$	$2\frac{5}{8}$	$2\frac{7}{8}$	$2\frac{9}{8}$	$2\frac{11}{8}$	$2\frac{13}{8}$	$2\frac{15}{8}$	$2\frac{17}{8}$	$2\frac{19}{8}$	$2\frac{21}{8}$	$2\frac{23}{8}$	$2\frac{25}{8}$	$3\frac{1}{8}$	$3\frac{3}{8}$	$3\frac{5}{8}$	$3\frac{7}{8}$	$3\frac{9}{8}$	$3\frac{11}{8}$	
	$\frac{9}{16}$	$2\frac{3}{8}$	$2\frac{5}{8}$	$2\frac{7}{8}$	$2\frac{9}{8}$	$2\frac{11}{8}$	$2\frac{13}{8}$	$2\frac{15}{8}$	$2\frac{17}{8}$	$2\frac{19}{8}$	$2\frac{21}{8}$	$2\frac{23}{8}$	$2\frac{25}{8}$	$3\frac{1}{8}$	$3\frac{3}{8}$	$3\frac{5}{8}$	$3\frac{7}{8}$	$3\frac{9}{8}$	$3\frac{11}{8}$	$3\frac{13}{8}$	
F	$\frac{5}{8}$	$2\frac{5}{8}$	$2\frac{7}{8}$	$2\frac{9}{8}$	$2\frac{11}{8}$	$2\frac{13}{8}$	$2\frac{15}{8}$	$2\frac{17}{8}$	$2\frac{19}{8}$	$2\frac{21}{8}$	$2\frac{23}{8}$	$2\frac{25}{8}$	$3\frac{1}{8}$	$3\frac{3}{8}$	$3\frac{5}{8}$	$3\frac{7}{8}$	$3\frac{9}{8}$	$3\frac{11}{8}$	$3\frac{13}{8}$	$3\frac{15}{8}$	
	$\frac{11}{16}$	$2\frac{7}{8}$	$2\frac{9}{8}$	$2\frac{11}{8}$	$2\frac{13}{8}$	$2\frac{15}{8}$	$2\frac{17}{8}$	$2\frac{19}{8}$	$2\frac{21}{8}$	$2\frac{23}{8}$	$2\frac{25}{8}$	$3\frac{1}{8}$	$3\frac{3}{8}$	$3\frac{5}{8}$	$3\frac{7}{8}$	$3\frac{9}{8}$	$3\frac{11}{8}$	$3\frac{13}{8}$	$3\frac{15}{8}$	$3\frac{17}{8}$	
	$\frac{3}{4}$	$2\frac{9}{8}$	$2\frac{11}{8}$	$2\frac{13}{8}$	$2\frac{15}{8}$	$2\frac{17}{8}$	$2\frac{19}{8}$	$2\frac{21}{8}$	$2\frac{23}{8}$	$2\frac{25}{8}$	$3\frac{1}{8}$	$3\frac{3}{8}$	$3\frac{5}{8}$	$3\frac{7}{8}$	$3\frac{9}{8}$	$3\frac{11}{8}$	$3\frac{13}{8}$	$3\frac{15}{8}$	$3\frac{17}{8}$	$3\frac{19}{8}$	
Values Below or to Right of Zigzag Line "C" are Large Enough for $\frac{3}{4}$ " Rivets		"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	
		"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	
		"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	



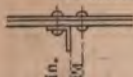
"A" must not be less than $\frac{1}{4}$ " + $\frac{1}{2}$ H



C	$\frac{3}{4}$ " Riv.	$\frac{3}{4}$ " Riv.
Inches	B	B
$1\frac{1}{8}$	$1\frac{1}{2}$	$1\frac{3}{8}$
$1\frac{3}{16}$	$1\frac{7}{16}$	$1\frac{5}{16}$
$1\frac{1}{4}$	$1\frac{3}{8}$	$1\frac{1}{4}$
$1\frac{5}{16}$	$1\frac{5}{16}$	$1\frac{3}{16}$
$1\frac{3}{8}$	$1\frac{1}{4}$	$1\frac{1}{16}$
$1\frac{7}{16}$	$1\frac{3}{16}$	1
$1\frac{1}{2}$	$1\frac{1}{8}$	$\frac{7}{8}$
$1\frac{9}{16}$	$1\frac{1}{16}$	$\frac{11}{16}$
$1\frac{5}{8}$	$\frac{11}{16}$	$\frac{5}{8}$
$1\frac{11}{16}$	$\frac{11}{16}$	$\frac{1}{2}$
$1\frac{3}{4}$	$\frac{11}{16}$	0

Minimum Rivet Spacing, Etc.

Clearance for Web Riveting



For $\frac{3}{8}$ " Rivets

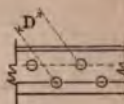
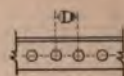
1 1/4" " 3/4" "

1 1/2" " 7/8" "

1 3/4" " 1" "

Rivets in Crimped Angles

Minimum Rivet Spacing

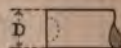


Diam. of Rivets Inches	D. Min. Inches
1/4	1
3/8	1 1/4
1/2	1 3/4
5/8	2
3/4	2 1/4
7/8	2 5/8
1	3



Distance Y should be $1\frac{1}{2}$ " + thickness of chord angles, but not less than 2"

Standard Rivet Dies



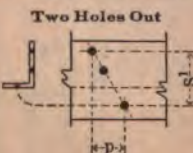
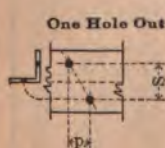
Diameter D = 2" for $\frac{3}{8}$ " Rivets
 " = 2 1/4" " $\frac{1}{2}$ " "
 " = 2 5/8" " $\frac{3}{4}$ " "

Clearance for Cover Plate Riveting
Dimensions in Inches



f	1/2	1	1 1/2	2	2 1/2	3	3 1/2	4	4 1/2	5	5 1/2	6
b	2 1/2	2 3/8	2 1/4	2 1/2	2 3/4	2 7/8	3	3 1/8	3 1/4	3 1/2	3 3/4	3 7/8
g	0	1/2	1	1 1/2	2	2 1/2						
b	2 1/2	2 1/4	2 1/8	2	1 1/2	0						

Staggering of Rivets to Maintain Net Section



Diameter of Hole taken out, $\frac{1}{8}$ " greater than nominal diameter of rivet

S	3/4 Riv.	1/2 Riv.	S	3/4 Riv.	1/2 Riv.
1	1 1/2	1 1/4	5	3 1/4	3 1/8
1 1/2	1 1/2	2	5 1/2	3 1/4	3 1/8
2	2 1/4	2 1/4	6	3 3/4	3 3/8
2 1/2	2 1/4	2 3/4	6 1/2	3 3/4	3 3/8
3	2 3/4	2 3/4	7	3 3/4	3 3/8
3 1/2	2 3/4	2 3/4	7 1/2	3 3/4	4
4	2 3/4	3	8	3 3/4	4 1/4
4 1/2	2 3/4	3 1/8	8 1/2	4	4 1/4

Rivets Length for Variant Grips



GRIP IN INCHES	DIAMETER IN INCHES					GRIP IN INCHES	DIAMETER IN INCHES				
	1/2	5/8	3/4	7/8	1		1/2	5/8	3/4	7/8	1
	Length in Inches						Length in Inches				
1/2	1 5/8	1 3/4	2	2 1/8	2 1/4	1/2	1 1/4	1 3/8	1 3/8	1 1/2	1 1/2
5/8	1 3/4	2	2 1/8	2 1/4	2 3/8	5/8	1 3/8	1 1/2	1 1/2	1 3/8	1 3/8
3/4	1 7/8	2 1/8	2 1/4	2 3/8	2 1/2	3/4	1 1/2	1 3/8	1 3/8	1 3/4	1 3/4
7/8	2	2 1/4	2 3/8	2 1/2	2 5/8	7/8	1 3/8	1 3/4	1 3/4	1 7/8	1 7/8
1	2 1/8	2 1/2	2 3/4	2 5/8	2 3/4	1	1 3/4	1 7/8	1 7/8	2	2
1 1/8	2 1/4	2 1/2	2 5/8	2 3/4	2 7/8	1 1/8	1 7/8	2	2	2 1/8	2 1/8
1 1/4	2 3/8	2 5/8	2 3/4	2 7/8	3	1 1/4	2	2 1/8	2 1/8	2 1/4	2 1/4
1 3/8	2 1/2	2 3/4	2 7/8	3	3 1/8	1 3/8	2 1/8	2 1/4	2 1/4	2 5/8	2 5/8
1 1/2	2 3/4	3	3 1/8	3 1/4	3 3/8	1 1/2	2 1/4	2 3/8	2 1/8	2 1/2	2 1/2
1 5/8	2 7/8	3 1/8	3 1/4	3 3/8	3 1/2	1 5/8	2 3/8	2 1/2	2 5/8	2 5/4	2 5/4
1 3/4	3	3 1/4	3 3/8	3 1/2	3 5/8	1 3/4	2 1/2	2 5/8	2 3/4	2 5/8	2 5/8
1 7/8	3 3/8	3 3/8	3 1/2	3 5/8	3 3/4	1 7/8	2 5/8	2 3/4	2 7/8	3	3
2	3 1/4	3 1/2	3 3/8	3 3/4	3 7/8	2	2 3/4	2 7/8	3	3	3 1/8
2 1/8	3 3/8	3 3/8	3 3/4	3 7/8	4	2 1/8	2 7/8	3	3 1/8	3 1/4	3 1/4
2 1/4	3 1/2	3 3/4	3 7/8	4	4 1/8	2 1/4	3	3 1/8	3 1/4	3 1/4	3 3/8
2 3/8	3 3/8	3 7/8	4	4 1/8	4 1/4	2 3/8	3 1/8	3 1/4	3 3/8	3 1/2	3 1/2
2 1/2	3 3/4	4	4 1/8	4 1/4	4 3/8	2 1/2	3 1/4	3 3/8	3 1/4	3 1/2	3 5/8
2 5/8	3 7/8	4 1/8	4 1/4	4 3/8	4 1/2	2 5/8	3 3/8	3 1/2	3 3/8	3 3/4	3 3/4
2 3/4	4	4 1/4	4 3/8	4 1/2	4 5/8	2 3/4	3 1/2	3 3/8	3 3/4	3 3/4	3 3/8
2 7/8	4 3/8	4 3/8	4 1/2	4 5/8	4 3/4	2 7/8	3 3/8	3 3/4	3 7/8	4	4
3	4 3/8	4 5/8	4 3/4	4 7/8	5	3	3 7/8	3 3/8	4	4 1/8	4 1/4
3 1/8	4 1/2	4 3/4	4 7/8	5	5 1/8	3 1/8	4	4	4 1/8	4 1/4	4 3/8
3 1/4	4 3/8	4 7/8	5	5 1/4	5 1/4	3 1/4	4 1/8	4 1/4	4 1/4	4 3/8	4 1/2
3 3/8	4 3/4	5	5 1/8	5 1/4	5 3/8	3 3/8	4 1/4	4 3/8	4 3/8	4 1/2	4 3/4
3 1/2	4 3/8	5 1/8	5 1/4	5 3/8	5 1/2	3 1/2	4 3/8	4 1/2	4 1/2	4 5/8	4 5/8
3 3/8	5	5 1/4	5 3/8	5 1/2	5 5/8	3 3/8	4 1/2	4 3/8	4 3/8	4 3/4	4 3/8
3 3/4	5 1/8	5 3/8	5 1/2	5 5/8	5 3/4	3 3/4	4 3/8	4 3/4	4 3/4	4 7/8	5
3 7/8	5 1/4	5 1/2	5 5/8	5 3/4	5 7/8	3 7/8	4 3/4	4 7/8	4 7/8	5	5 1/8
4	5 3/8	5 3/4	5 3/4	5 7/8	6	4	4 7/8	5	5 3/8	5 1/8	5 1/4
4 1/8	5 1/2	5 5/8	5 5/8	6	6 1/8	4 1/8	5	5 1/8	5 1/4	5 3/8	5 3/8
4 1/4	5 5/8	5 5/8	6	6 1/8	6 1/4	4 1/4	5 1/8	5 1/4	5 3/8	5 3/8	5 3/8
4 3/8	5 3/4	6	6 1/4	6 1/8	6 3/8	4 3/8	5 1/4	5 3/8	5 1/2	5 5/8	5 5/8
4 1/2	6	6 1/4	6 3/8	6 1/2	6 5/8	4 1/2	5 5/8	5 5/4
4 3/4	6 1/8	6 3/8	6 1/2	6 3/4	6 3/4	4 3/4	5 3/4	5 3/8
4 5/8	6 3/4	6 3/4	6 3/4	6 3/4	6 7/8	4 5/8	5 7/8	6
4 7/8	6 3/8	6 3/8	6 3/4	6 7/8	7	4 7/8	6	6 1/8
5	6 1/2	6 3/4	6 3/8	7	7 1/8	5	6 1/8	6 1/4
5 1/8	6 3/8	6 3/8	7	7 1/8	7 1/4	5 1/8	6 3/4	6 3/8
5 1/4	6 3/4	7	7 1/8	7 1/4	7 3/8	5 1/4	6 3/4
5 3/8	6 3/4	7 1/8	7 1/4	7 3/8	7 1/2	5 3/8	6 3/4

Rivets Continued Shearing and Bearing Value for Quiescent Loads as Used in Buildings

Diameter of Rivet in In.		Area of Rivet, Square Inches	Single Shear, lbs. per sq. inch, at 12,000	Bearing Value for Different Thicknesses of Plate at 24,000 lbs. per square inch (= Diameter of Rivet \times Thickness of Plate \times 24,000 lbs.)									
Fraction	Decimal			$\frac{1}{8}$ Inch	$\frac{3}{8}$ Inch	$\frac{1}{2}$ Inch	$\frac{5}{8}$ Inch	$\frac{3}{4}$ Inch	$\frac{7}{8}$ Inch	$\frac{1}{2}$ Inch	$\frac{5}{8}$ Inch	$\frac{3}{4}$ Inch	$\frac{7}{8}$ Inch
$\frac{3}{8}$.375	.1104	1320	2810	3940	5250	6000	6750	7500	8440	9380	10310	11250
$\frac{1}{2}$.4375	.1503	1800	3280	4500	5060	5630	6190	6750	7310	7880	8440	9000
$\frac{5}{8}$.5	.1963	2360	3750	4500	5250	6000	6750	7500	8440	9380	10310	11250
$\frac{3}{4}$.5625	.2485	2980	4220	5060	5630	6190	6750	7310	7880	8440	9000	9560
$\frac{7}{8}$.625	.3068	3680	4690	5630	6190	6750	7310	7880	8440	9000	9560	10120
$\frac{1}{16}$.6875	.3712	4450	5160	6190	7220	8250	9280	10310	11250	12190	13130	14060
$\frac{3}{4}$.75	.4418	5300	5630	6750	7880	9000	10130	11250	12190	13130	14060	15000
$\frac{1}{16}$.8125	.5185	6220	6090	7310	8530	9750	10970	12190	13410	14630	15850	17070
$\frac{7}{8}$.875	.6013	7220	6560	7880	9190	10500	11810	13130	14430	15740	17050	18360
$\frac{1}{16}$.9375	.6903	8280	7030	8440	9850	11250	12660	14060	15470	16880	18290	19700
1	1.	.7854	9420	7500	9000	10500	12000	13500	15000	16500	18000	19500	21000
$1\frac{1}{16}$	1.0625	.8866	10640	7970	9560	11160	12750	14350	15940	17530	19125	20720	22300
$1\frac{1}{8}$	1.125	.9940	11930	8440	10125	11810	13500	15190	16875	18560	20250	21940	23626
$1\frac{1}{16}$	1.1875	1.1075	13290	8910	10690	12470	14250	16030	17810	19600	21375	23160	24940

Rivets Continued Shearing and Bearing Value for Moving Loads as Used in Bridges, Craneways, Etc.

Diameter of Rivet in Inches		Area of Rivets, Square Inches	Single Shear at 7500 lbs. per sq. inch	Bearing Value for Different Thicknesses of Plate at 15,000 lbs. per square inch (= Diameter of Rivet X Thickness of Plate X 15,000 lbs.)											
Fraction	Decimal			$\frac{1}{8}$ Inch	$\frac{3}{8}$ Inch	$\frac{1}{2}$ Inch	$\frac{5}{8}$ Inch	$\frac{3}{4}$ Inch	$\frac{7}{8}$ Inch	$\frac{1}{2}$ Inch	$\frac{5}{8}$ Inch	$\frac{3}{4}$ Inch	$\frac{7}{8}$ Inch	$\frac{1}{2}$ Inch	$\frac{3}{4}$ Inch
$\frac{3}{8}$.375	.1104	828	1410
$\frac{7}{16}$.4375	.1503	1130	1640	2050
$\frac{1}{2}$.5	.1963	1470	1880	2340	2810
$\frac{9}{16}$.5625	.2485	1860	2110	2640	3160	3690
$\frac{5}{8}$.625	.3068	2300	2340	2930	3520	4100
$\frac{11}{16}$.6875	.3712	2780	2580	3220	3870	4510	5160
$\frac{3}{4}$.75	.4418	3310	2810	3520	4220	4920	5630	6330
$\frac{13}{16}$.8125	.5185	3890	3050	3810	4570	5330	6090	6860	7620
$\frac{7}{8}$.875	.6013	4510	3280	4100	4920	5740	6560	7380	8200
$\frac{15}{16}$.9375	.6903	5180	3520	4390	5270	6150	7030	7910	8790	9670
1	1	.7854	5890	3750	4690	5620	6560	7500	8440	9380	10310	11250
$1\frac{1}{16}$	1.0625	.8866	6650	3980	4980	5980	6970	7970	8960	9960	10960	11950	12950
$1\frac{1}{8}$	1.125	.9940	7460	4220	5270	6330	7380	8440	9490	10550	11600	12660	13710	14770
$1\frac{3}{8}$	1.1875	1.1075	8310	4450	5570	6680	7790	8910	10020	11130	12250	13360	14470	15590

Rivet values in bearing above heavy horizontal lines are in excess of single shear values.

Rivets

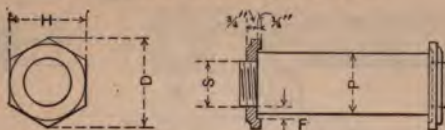
Continued

Average Weight of 100 Round Head Rivets

LENGTH, INCHES	DIAMETER IN INCHES							
	$\frac{3}{8}$	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$	1	$1\frac{1}{8}$	$1\frac{1}{4}$
$1\frac{1}{4}$	5.5	12.9	21.9	29.3	44.0	66.6	93.3	125.5
$1\frac{1}{2}$	6.3	14.2	24.2	32.4	48.2	72.1	100.4	135.7
$1\frac{3}{4}$	7.0	15.6	26.3	35.6	52.4	77.7	107.1	144.8
2	7.9	16.9	28.4	38.7	56.7	83.2	114.2	153.0
$2\frac{1}{4}$	8.7	18.4	30.6	41.8	61.0	88.8	121.4	162.2
$2\frac{1}{2}$	9.4	19.8	32.8	45.0	64.3	94.4	128.5	170.3
$2\frac{3}{4}$	10.2	21.1	35.0	48.0	69.5	100.0	135.7	179.5
3	11.0	22.5	37.1	51.2	73.7	105.1	142.8	187.7
$3\frac{1}{4}$	11.7	24.0	39.4	54.4	78.0	111.2	149.9	196.9
$3\frac{1}{2}$	12.5	25.3	41.5	57.5	82.3	116.3	157.1	205.0
$3\frac{3}{4}$	13.4	26.7	43.7	60.6	86.5	122.4	164.2	214.2
4	14.1	28.1	45.9	63.8	90.8	127.5	170.3	222.4
$4\frac{1}{4}$	14.9	29.5	48.0	66.9	95.1	133.6	177.5	231.5
$4\frac{1}{2}$	15.7	30.9	50.2	70.0	99.3	138.7	184.6	240.7
$4\frac{3}{4}$	16.5	32.2	52.4	73.1	104.0	144.8	191.8	248.9
5	17.2	33.7	54.6	76.3	108.1	149.9	198.9	258.1
$5\frac{1}{4}$	18.1	35.1	56.7	79.4	112.2	156.1	206.0	266.2
$5\frac{1}{2}$	18.8	36.4	58.9	82.5	116.3	161.2	213.2	275.4
$5\frac{3}{4}$	19.6	37.8	61.1	85.7	120.4	166.3	220.3	283.6
6	20.4	39.3	63.2	88.7	124.4	172.4	227.5	292.7
$6\frac{1}{2}$	21.9	42.0	67.6	95.1	133.6	183.6	240.7	310.1
7	23.5	44.8	71.9	101.3	141.8	194.8	255.0	327.4
$7\frac{1}{2}$	25.1	47.5	76.3	108.1	149.9	206.0	269.3	344.8
8	26.6	50.4	80.6	114.2	159.1	217.3	283.6	362.1
$8\frac{1}{2}$	28.2	53.1	85.0	120.3	167.3	227.5	297.8	379.4
9	29.8	55.9	89.4	126.5	176.5	238.7	312.1	396.8
$9\frac{1}{2}$	31.3	58.8	93.6	132.6	184.6	249.9	325.4	410.1
10	32.8	61.5	98.0	138.7	192.8	261.1	339.7	431.5
Heads...	1.8	5.8	11.1	13.7	22.6	38.8	58.1	83.6

In the above table the length is from under the head.

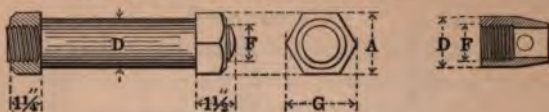
Standard Shouldered Pins



Eight threads per inch.

DIMENSIONS IN INCHES					DIMENSIONS IN INCHES				
P	S	D	F	H	P	S	D	F	H
1 1/4	3/4	2 7/8	3/8	2 1/2	5 1/2	4	7 3/4	7/8	6 3/4
1 3/8	3/4	2 7/8	3/8	2 1/2	5 5/8	4	7 3/4	7/8	6 3/4
1 1/2	1	3 1/8	3/8	2 3/4	5 3/4	4 1/2	8 1/8	3/4	7
1 5/8	1	3 1/8	3/8	2 3/4	5 7/8	4 1/2	8 1/8	3/4	7
1 3/4	1 1/4	3 1/2	3/8	3	6	4 1/2	8 3/8	7/8	7 1/4
1 7/8	1 1/4	3 1/2	3/8	3	6 1/8	4 1/2	8 3/8	7/8	7 1/4
2	1 1/2	4	1/2	3 1/2	6 1/4	4 1/2	8 5/8	1	7 1/2
2 1/8	1 1/2	4	1/2	3 1/2	6 3/8	4 1/2	8 5/8	1	7 1/2
2 1/4	1 1/2	4	1/2	3 1/2	6 1/2	4 1/2	8 5/8	1	7 1/2
2 3/8	1 3/4	4 3/8	1/2	3 3/4	6 5/8	4 1/2	9	1 5/16	7 3/4
2 1/2	1 3/4	4 3/8	1/2	3 3/4	6 3/4	4 1/2	9	1 5/16	7 3/4
2 5/8	1 3/4	4 3/8	1/2	3 3/4	6 7/8	4 1/2	9	1 5/16	7 3/4
2 3/4	2	4 5/8	1/2	4	7	4 1/2	9	1 5/16	7 3/4
2 7/8	2	4 5/8	1/2	4	7 1/4	5	9 7/8	1 3/8	8 1/2
3	2 1/4	4 7/8	1/2	4 1/4	7 1/2	5	9 7/8	1 3/8	8 1/2
3 1/8	2 1/4	4 7/8	1/2	4 1/4	7 3/4	5	9 7/8	1 3/8	8 1/2
3 1/4	2 1/2	5 1/8	1/2	4 1/2	8	5	10 3/4	1 3/4	9 1/4
3 3/8	2 1/2	5 1/8	1/2	4 1/2	8 1/4	5	10 3/4	1 3/4	9 1/4
3 1/2	2 3/4	5 1/2	1/2	4 3/4	8 1/2	5	10 3/4	1 3/4	9 1/4
3 5/8	2 3/4	5 1/2	1/2	4 3/4	8 3/4	6	11 5/8	1 5/8	10
3 3/4	3	5 3/4	1/2	5	9	6	11 5/8	1 5/8	10
3 7/8	3	5 3/4	1/2	5	9 1/4	6	11 5/8	1 5/8	10
4	3 1/4	6 1/8	1/2	5 1/4	9 1/2	6	12 1/8	1 7/8	10 1/2
4 1/8	3 1/4	6 1/8	1/2	5 1/4	9 3/4	6	12 1/8	1 7/8	10 1/2
4 1/4	3 1/4	6 1/8	1/2	5 1/4	10	7	13 1/4	1 7/8	11 1/2
4 3/8	3 1/2	6 5/8	5/8	5 3/4	10 1/4	7	13 1/4	1 7/8	11 1/2
4 1/2	3 1/2	6 5/8	5/8	5 3/4	10 1/2	7	13 1/4	1 7/8	11 1/2
4 5/8	3 1/2	6 5/8	5/8	5 3/4	10 3/4	7	13 1/4	1 7/8	11 1/2
4 3/4	3 1/2	7	5/8	6	11	8	14 3/4	2	12 3/4
4 7/8	3 1/2	7	5/8	6	11 1/4	8	14 3/4	2	12 3/4
5	4	7 1/4	5/8	6 1/4	11 1/2	8	14 3/4	2	12 3/4
5 1/8	4	7 1/4	5/8	6 1/4	11 3/4	8	14 3/4	2	12 3/4
5 1/4	4	7 1/2	3/4	6 1/2	12	8	14 3/4	2	12 3/4
5 3/8	4	7 1/2	3/4	6 1/2					

Bridge Pins, Nuts and Pilot Nuts

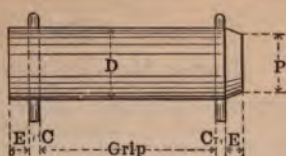


All Threads 8 Per Inch

Pin Nut

PINS			PIN NUTS			Diameter of Holes in Eye Bars
Nominal Diameter, Inches	Turned Diameter D, Inches	Diameter Thread F, Inches	Short Diameter A, Inches	Long Diameter G, Inches	Weight, Pounds	
1 1/2	1 7/16	1 1/4	2	2 5/16	.79	D + 1/16
1 3/4	1 11/16	1 1/2	2 1/2	2 7/8	1.29	D + 1/16
2	1 13/16	1 1/2	2 1/2	2 7/8	1.29	D + 1/16
2 1/4	2 3/16	1 1/2	3	3 1/2	2.12	D + 1/16
2 1/2	2 7/16	2	3	3 1/2	1.75	D + 1/16
2 3/4	2 11/16	2	3 1/2	4 1/16	2.63	D + 1/16
3	2 13/16	2	3 1/2	4 1/16	2.63	D + 1/16
3 1/4	3 3/16	2 1/2	4	4 11/16	3.17	D + 1/16
3 1/2	3 7/16	2 1/2	4	4 11/16	3.17	D + 1/16
3 3/4	3 11/16	2 3/4	4 1/2	5 3/16	4.12	D + 1/16
4	3 13/16	3	4 1/2	5 3/16	3.75	D + 1/16
4 1/4	4 3/16	3 1/2	5	5 11/16	4.25	D + 1/16
4 1/2	4 7/16	3 1/2	5	5 11/16	4.25	D + 1/16
4 3/4	4 11/16	4	5 1/2	6 3/8	4.84	D + 1/16
5	4 13/16	4	5 1/2	6 3/8	4.84	D + 1/16
5 1/4	5 3/16	4	6	6 11/16	6.67	D + 1/16
5 1/2	5 7/16	4	6	6 11/16	6.67	D + 1/16
5 3/4	5 11/16	4	6 1/2	7 1/2	8.49	D + 1/16
6	5 13/16	4	6 1/2	7 1/2	8.49	D + 1/16
6 1/4	6 3/16	4	7	8 1/8	10.64	D + 1/16
6 1/2	6 7/16	4	7	8 1/8	10.64	D + 1/16
6 3/4	6 11/16	4	7 1/2	8 11/16	12.85	D + 1/16
7	6 13/16	4	7 1/2	8 11/16	12.85	D + 1/16

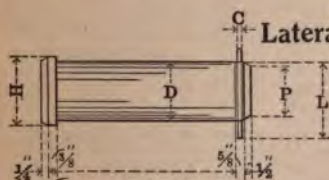
Cold Rolled Steel Cotter Pins



All Dimensions in Inches

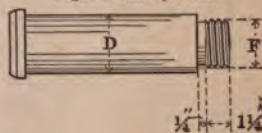
Diameter of Pin	D	1	1 1/4	1 1/2	1 3/4	2	2 1/4	2 1/2	2 3/4	3	3 1/4	3 1/2	3 3/4	4
Diam. of Reduced Pt.	P	7/8	1 1/8	1 1/4	1 1/2	1 3/4	2	2 1/4	2 1/2	2 3/4	3	3 1/4	3 1/2	3 3/4
Lengths of Ends	E	5/16	5/16	1/2	1/2	1/2	1/2	1/2	1/2	7/8	7/8	7/8	7/8	7/8
Diameter of Cotter...	C	5/16	5/16	5/16	5/16	3/8	3/8	3/8	3/8	1/2	1/2	1/2	1/2	1/2

Diameter of pin hole 1/16" greater than diameter of pin.



Lateral Pins

Eight Threads per inch



All Dimensions in Inches

PIN					COTTER	
Rough Diameter of Pin	Diameter of Pin Hole	Finished Diameter of Pin	Reduced Point	Diameter of Thread	Diameter	Length
H	N	D	P	F	C	L
1 1/2	1 1/4	1 7/32	1	1	5/16	2
1 3/4	1 1/2	1 15/32	1 1/4	1 1/4	5/16	2 1/2
2	1 3/4	1 23/32	1 1/2	1 1/2	3/8	2 3/4
2 1/4	2	1 31/32	1 3/4	1 1/2	3/8	3
2 1/2	2 1/4	2 7/32	2	1 1/2	3/8	3 1/4
2 3/4	2 1/2	2 15/32	2 1/4	2	3/8	3 3/4
3	2 3/4	2 23/32	2 1/2	2	1/2	4
3 1/4	3	2 31/32	2 3/4	2	1/2	5
3 1/2	3 1/4	3 7/32	3	2 1/2	1/2	5
3 3/4	3 1/2	3 15/32	3 1/4	2 1/2	1/2	6
4	3 3/4	3 23/32	3 1/2	2 1/2	1/2	6

$$D = H - \frac{5}{16}''$$

$$P = N - \frac{1}{4}''$$

Pins

Bending Moments in Inch Pounds

Bending Moment = (Diameter of Pin)³ × 0.098175 × Stress per Square Inch.

PIN		FIBER STRESS IN POUNDS PER SQUARE INCH						
Diameter, Inches	Area, Square Inches	15000	18000	20000	22000	22500	24000	25000
1	.785	1500	1800	2000	2200	2200	2400	2500
1 $\frac{1}{4}$	1.227	2900	3500	3800	4200	4300	4600	4800
1 $\frac{1}{2}$	1.767	5000	6000	6600	7300	7500	8000	8300
1 $\frac{3}{4}$	2.405	7900	9500	10500	11600	11800	12600	13200
2	3.142	11800	14100	15700	17300	17700	18800	19600
2 $\frac{1}{4}$	3.976	16800	20100	22400	24600	25200	26800	28000
2 $\frac{1}{2}$	4.909	23000	27600	30700	33700	34500	36800	38300
2 $\frac{3}{4}$	5.940	30600	36800	40800	44900	45900	49000	51000
3	7.069	39800	47700	53000	58300	59600	63600	66300
3 $\frac{1}{4}$	8.296	50600	60700	67400	74100	75800	80900	84300
3 $\frac{1}{2}$	9.621	63100	75800	84200	92600	94700	101000	105200
3 $\frac{3}{4}$	11.045	77700	93200	103500	113900	116500	124300	129400
4	12.566	94200	113100	125700	138200	141400	150800	157100
4 $\frac{1}{4}$	14.186	113000	135700	150700	165800	169600	180900	188400
4 $\frac{1}{2}$	15.904	134200	161000	178900	196800	201300	214700	223700
4 $\frac{3}{4}$	17.721	157800	189400	210400	231500	236700	252500	263000
5	19.635	184100	220900	245400	270000	276100	294500	306800
5 $\frac{1}{4}$	21.648	213100	255700	284100	312500	319600	340900	355200
5 $\frac{1}{2}$	23.758	245000	294000	326700	359300	367500	392000	408300
5 $\frac{3}{4}$	25.967	280000	336000	373300	410600	419900	447900	466600
6	28.274	318100	381700	424100	466500	477100	508900	530100
6 $\frac{1}{4}$	30.680	359500	431400	479400	527300	539300	575200	599200
6 $\frac{1}{2}$	33.183	404400	485300	539200	593100	606600	647100	674000
6 $\frac{3}{4}$	35.785	452900	543500	603900	660300	674900	724600	754800
7	38.485	505100	606100	673500	740800	757700	808200	841800
7 $\frac{1}{4}$	41.282	561200	673400	748200	823100	841800	897900	935300
7 $\frac{1}{2}$	44.179	621300	745500	828400	911200	931900	994000	1035400
7 $\frac{3}{4}$	47.173	685500	822600	914000	1005400	1028200	1096800	1142500
8	50.265	754000	904800	1005300	1105800	1131000	1206400	1256600
8 $\frac{1}{4}$	53.456	826900	992300	1102500	1212800	1240400	1323000	1378200
8 $\frac{1}{2}$	56.745	904400	1085300	1205800	1326400	1356600	1447000	1507300
8 $\frac{3}{4}$	60.132	986500	1183900	1315400	1446900	1479800	1578500	1644200
9	63.617	1073500	1288300	1431400	1574500	1610300	1717700	1789200
9 $\frac{1}{4}$	67.201	1165500	1398600	1554000	1709400	1748300	1864800	1942500
9 $\frac{1}{2}$	70.882	1262600	1515100	1683500	1851800	1893900	2020100	2104300
9 $\frac{3}{4}$	74.662	1364900	1637900	1819900	2001900	2047400	2183900	2274900
10	78.540	1472600	1767100	1963500	2159800	2208900	2356200	2454400
10 $\frac{1}{4}$	82.516	1585900	1903000	2114500	2325900	2378800	2537400	2643100
10 $\frac{1}{2}$	86.590	1704700	2045700	2273000	2500300	2557100	2727600	2841200
10 $\frac{3}{4}$	90.763	1829400	2195300	2439200	2683200	2744100	2927100	3049100
11	95.033	1960100	2352100	2613400	2874800	2941000	3136100	3266800
11 $\frac{1}{4}$	99.402	2096800	2516100	2795700	3075200	3145100	3354800	3494600
11 $\frac{1}{2}$	103.869	2239700	2687600	2986200	3284900	3359500	3583500	3732800
11 $\frac{3}{4}$	108.434	2388900	2866700	3185300	3503800	3583400	3822300	3981600
12	113.097	2544700	3053600	3392900	3732200	3817000	4071500	4241200

Pin Plates

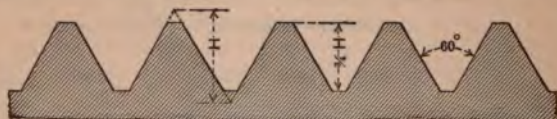
Bearing Values in Pounds on Metal One Inch Thick

Bearing Value = Diameter of Pin \times Bearing Stress per Square Inch

PIN		BEARING STRESSES IN POUNDS PER SQUARE INCH				
Diam- eter, Inches	Area, Square Inches	12000	15000	20000	22000	24000
1	.785	12000	15000	20000	22000	24000
1 $\frac{1}{4}$	1.227	15000	18800	25000	27500	30000
1 $\frac{1}{2}$	1.767	18000	22500	30000	33000	36000
1 $\frac{3}{4}$	2.405	21000	26300	35000	38500	42000
2	3.142	24000	30000	40000	44000	48000
2 $\frac{1}{4}$	3.976	27000	33800	45000	49500	54000
2 $\frac{1}{2}$	4.909	30000	37500	50000	55000	60000
2 $\frac{3}{4}$	5.940	33000	41300	55000	60500	66000
3	7.069	36000	45000	60000	66000	72000
3 $\frac{1}{4}$	8.296	39000	48800	65000	71500	78000
3 $\frac{1}{2}$	9.621	42000	52500	70000	77000	84000
3 $\frac{3}{4}$	11.045	45000	56300	75000	82500	90000
4	12.566	48000	60000	80000	88000	96000
4 $\frac{1}{4}$	14.186	51000	63800	85000	93500	102000
4 $\frac{1}{2}$	15.904	54000	67500	90000	99000	108000
4 $\frac{3}{4}$	17.721	57000	71300	95000	104500	114000
5	19.635	60000	75000	100000	110000	120000
5 $\frac{1}{4}$	21.648	63000	78800	105000	115500	126000
5 $\frac{1}{2}$	23.758	66000	82500	110000	121000	132000
5 $\frac{3}{4}$	25.967	69000	86300	115000	126500	138000
6	28.274	72000	90000	120000	132000	144000
6 $\frac{1}{4}$	30.680	75000	93800	125000	137500	150000
6 $\frac{1}{2}$	33.183	78000	97500	130000	143000	156000
6 $\frac{3}{4}$	35.785	81000	101300	135000	148500	162000
7	38.485	84000	105000	140000	154000	168000
7 $\frac{1}{4}$	41.282	87000	108800	145000	159500	174000
7 $\frac{1}{2}$	44.179	90000	112500	150000	165000	180000
7 $\frac{3}{4}$	47.173	93000	116300	155000	170500	186000
8	50.265	96000	120000	160000	176000	192000
8 $\frac{1}{4}$	53.456	99000	123800	165000	181500	198000
8 $\frac{1}{2}$	56.745	102000	127500	170000	187000	204000
8 $\frac{3}{4}$	60.132	105000	131300	175000	192500	210000
9	63.617	108000	135000	180000	198000	216000
9 $\frac{1}{4}$	67.201	111000	138800	185000	203500	222000
9 $\frac{1}{2}$	70.882	114000	142500	190000	209000	228000
9 $\frac{3}{4}$	74.662	117000	146300	195000	214500	234000
10	78.540	120000	150000	200000	220000	240000
10 $\frac{1}{4}$	82.516	123000	153800	205000	225500	246000
10 $\frac{1}{2}$	86.590	126000	157500	210000	231000	252000
10 $\frac{3}{4}$	90.763	129000	161300	215000	236500	258000
11	95.033	132000	165000	220000	242000	264000
11 $\frac{1}{4}$	99.402	135000	168800	225000	247500	270000
11 $\frac{1}{2}$	103.869	138000	172500	230000	253000	276000
11 $\frac{3}{4}$	108.434	141000	176300	235000	258500	282000
12	113.097	144000	180000	240000	264000	288000

Standard Screw Threads, Nuts and Bolt Heads

Recommended by Franklin Institute, December 15, 1864, and adopted by Navy Department of the United States, by the R. R. Master Mechanics' and Master Car-Builders' Association and by the Jones & Laughlin Steel Company.



Angle of thread 60°. Flat at top and bottom $\frac{1}{8}$ of pitch.

Diameter of Screw, Inches	Threads per Inch	Diameter at Root of Thread, Inches	Diameter of Screw, Inches	Threads per Inch	Diameter at Root of Thread, Inches
$\frac{1}{4}$	20	.185	2	$4\frac{1}{2}$	1.712
$\frac{5}{16}$	18	.240	$2\frac{1}{4}$	$4\frac{1}{2}$	1.962
$\frac{3}{8}$	16	.294	$2\frac{1}{2}$	4	2.176
$\frac{7}{16}$	14	.344	$2\frac{3}{4}$	4	2.426
$\frac{1}{2}$	13	.400	3	$3\frac{1}{2}$	2.629
$\frac{9}{16}$	12	.454	$3\frac{1}{4}$	$3\frac{1}{2}$	2.879
$\frac{5}{8}$	11	.507	$3\frac{1}{2}$	$3\frac{1}{4}$	3.100
$\frac{3}{4}$	10	.620	$3\frac{3}{4}$	3	3.317
$\frac{7}{8}$	9	.731	4	3	3.567
1	8	.837	$4\frac{1}{4}$	$2\frac{7}{8}$	3.798
$1\frac{1}{8}$	7	.940	$4\frac{1}{2}$	$2\frac{3}{4}$	4.028
$1\frac{1}{4}$	7	1.065	$4\frac{3}{4}$	$2\frac{5}{8}$	4.256
$1\frac{3}{8}$	6	1.160	5	$2\frac{1}{2}$	4.480
$1\frac{1}{2}$	6	1.284	$5\frac{1}{4}$	$2\frac{1}{2}$	4.730
$1\frac{5}{8}$	$5\frac{1}{2}$	1.389	$5\frac{1}{2}$	$2\frac{3}{8}$	4.953
$1\frac{3}{4}$	5	1.491	$5\frac{3}{4}$	$2\frac{3}{8}$	5.203
$1\frac{7}{8}$	5	1.616	6	$2\frac{1}{4}$	5.423

Nuts and bolt heads are determined by the following rules, which apply to both square and hexagon nuts:

Short diameter of rough nut = $1\frac{1}{2} \times$ diameter of bolt + $\frac{1}{8}$ -inch.

Short diameter of finished nut = $1\frac{1}{2} \times$ diameter of bolt + $\frac{1}{16}$ -inch.

Thickness of rough nut = diameter of bolt.

Thickness of finished nut = diameter of bolt — $\frac{1}{16}$ -inch.

Short diameter of rough head = $1\frac{1}{2} \times$ diameter of bolt + $\frac{1}{8}$ -inch.

Short diameter of finished head = $1\frac{1}{2} \times$ diameter of bolt + $\frac{1}{16}$ -inch.

Thickness of rough head = $\frac{1}{2}$ short diameter of head.

Thickness of finished head = diameter of bolt — $\frac{1}{16}$ -inch.

The long diameter of a hexagon nut may be obtained by multiplying the short diameter by 1.155 and the long diameter of a square nut by multiplying short diameter by 1.414.

Square Head Machine Bolts

Average Weight of 100 Bolts

Length, Inches	DIAMETER, INCHES								
	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$	1
1 $\frac{1}{2}$	4.0	6.8	10.6	15.0	23.9	40.5	70.0		
1 $\frac{3}{4}$	4.4	7.3	11.3	16.1	25.1	42.7	73.1		
2	4.7	7.8	12.0	17.2	26.3	44.8	76.2		
2 $\frac{1}{4}$	5.1	8.4	12.6	18.2	27.7	47.0	79.3		
2 $\frac{1}{2}$	5.4	8.9	13.3	19.2	29.0	49.2	82.4	120.5	
2 $\frac{3}{4}$	5.8	9.5	14.0	20.2	30.4	51.4	85.5	124.7	
3	6.1	10.0	14.7	21.2	31.8	53.5	88.7	128.9	185.0
3 $\frac{1}{2}$	6.8	11.1	16.0	23.2	34.7	57.9	95.0	137.4	196.0
4	7.5	12.2	17.4	25.2	37.5	62.3	101.2	145.8	207.0
4 $\frac{1}{2}$	8.2	13.2	18.7	27.2	40.2	66.7	107.5	159.2	218.0
5	8.9	14.3	20.0	29.1	43.0	71.0	113.7	167.7	229.0
5 $\frac{1}{2}$	9.6	15.4	21.4	31.2	45.7	75.4	120.0	176.1	240.0
6	10.3	16.5	22.8	33.1	48.4	79.8	126.2	184.6	251.0
6 $\frac{1}{2}$	11.0	17.6	24.1	35.1	51.2	84.1	132.5	193.0	262.0
7	11.7	18.6	25.9	37.1	54.0	88.5	138.7	201.4	273.0
7 $\frac{1}{2}$	12.4	19.7	27.7	39.1	56.7	92.9	145.0	209.9	284.0
8	13.1	20.8	29.5	41.0	59.4	97.2	151.2	218.3	295.0
9			33.1	45.0	64.8	106.0	163.7	240.2	317.0
10			36.7	49.0	70.3	114.7	176.2	257.1	339.0
11			40.4	53.0	75.8	123.5	188.7	273.9	360.0
12			44.0	57.0	81.3	132.2	201.0	290.0	382.0
13					86.7	140.7	213.4	307.7	404.0
14					92.2	149.2	225.9	324.5	426.0
15					97.7	157.6	238.3	341.4	448.0
16					103.1	166.1	250.8	358.3	470.0
17					108.6	174.6	263.2	375.2	492.0
18					114.1	183.1	275.6	392.0	514.0
19					119.5	191.5	288.1	408.9	536.0
20					125.0	200.0	300.5	425.8	558.0
Per inch addi- tional	1.4	2.2	3.6	4.0	5.5	8.5	12.4	16.9	22.0

Nuts and Bolt Heads

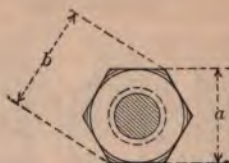
Approximate Weight in Pounds

Diameter of Bolt, Inches	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$
Weight of Hexagon Nut and Head..	.017	.042	.057	.109	.128	.267	.43
Weight of Square Nut and Head...	.021	.049	.069	.120	.164	.320	.55

Diameter of Bolt, Inches	$\frac{7}{8}$	1	1 $\frac{1}{4}$	1 $\frac{1}{2}$	1 $\frac{3}{4}$	2	2 $\frac{1}{2}$
Weight of Hexagon Nut and Head..	.73	1.10	2.14	3.78	5.6	8.75	17.0
Weight of Square Nut and Head...	.88	1.31	2.56	4.42	7.0	10.5	21.0

Hot Pressed Hexagon Nuts

Sizes and Weights—United States Standard

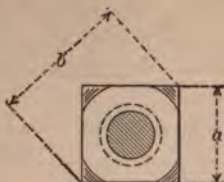


DIMENSIONS		Thick- ness, Inches	SIZE OF HOLE		Size of Bolt, Inches	Weight of 100 Nuts	Number of Nuts in 100 Pounds
a	b						
$1\frac{1}{2}$.58	$\frac{1}{4}$	0.185	$\frac{3}{16}$ scant	$\frac{1}{4}$	1.3	7615
$1\frac{1}{2}$.68	$\frac{1}{4}$	0.240	$\frac{1}{4}$ scant	$\frac{3}{16}$	1.9	5200
$1\frac{1}{2}$.79	$\frac{3}{8}$	0.294	$\frac{1}{4}$ scant	$\frac{3}{8}$	3.3	3000
$1\frac{1}{2}$.90	$\frac{1}{2}$	0.344	$\frac{1}{2}$	$\frac{1}{2}$	5.0	2000
$1\frac{3}{4}$	1.01	$\frac{1}{2}$	0.400	$\frac{3}{4}$ scant	$\frac{1}{2}$	7.0	1430
$1\frac{3}{4}$	1.12	$\frac{3}{4}$	0.454	$\frac{3}{4}$ scant	$\frac{3}{4}$	9.1	1100
$1\frac{3}{4}$	1.23	$\frac{5}{8}$	0.507	$\frac{1}{2}$ full	$\frac{5}{8}$	13.5	740
$1\frac{3}{4}$	1.44	$\frac{3}{4}$	0.620	$\frac{5}{8}$ scant	$\frac{3}{4}$	22.2	450
$1\frac{7}{8}$	1.66	$\frac{7}{8}$	0.731	$\frac{7}{8}$ scant	$\frac{7}{8}$	32.4	309
$1\frac{7}{8}$	1.88	1	0.837	$\frac{7}{8}$ scant	1	46.3	216
$1\frac{7}{8}$	2.09	$1\frac{1}{8}$	0.940	$1\frac{1}{8}$ full	$1\frac{1}{8}$	67.6	148
2	2.31	$1\frac{1}{4}$	1.065	$1\frac{1}{4}$ full	$1\frac{1}{4}$	90.1	111
$2\frac{1}{8}$	2.53	$1\frac{3}{8}$	1.160	$1\frac{3}{8}$ full	$1\frac{3}{8}$	117.5	85
$2\frac{1}{8}$	2.74	$1\frac{1}{2}$	1.284	$1\frac{1}{2}$ full	$1\frac{1}{2}$	147.1	68
$2\frac{1}{8}$	2.96	$1\frac{5}{8}$	1.389	$1\frac{5}{8}$ scant	$1\frac{5}{8}$	178.6	56
$2\frac{1}{4}$	3.18	$1\frac{3}{4}$	1.491	$1\frac{1}{2}$ scant	$1\frac{3}{4}$	250.0	40
$2\frac{1}{2}$	3.39	$1\frac{7}{8}$	1.616	$1\frac{5}{8}$ scant	$1\frac{7}{8}$	285.7	35
$2\frac{1}{2}$	3.61	2	1.712	$1\frac{3}{2}$ scant	2	344.8	29
$2\frac{1}{2}$	3.82	$2\frac{1}{8}$	1.836	$1\frac{3}{2}$ scant	$2\frac{1}{8}$	384.6	26
$2\frac{1}{2}$	4.04	$2\frac{1}{4}$	1.962	$1\frac{3}{2}$ scant	$2\frac{1}{4}$	434.8	23

Both weights and sizes are for unfinished nuts.

Hot Pressed Square Nuts

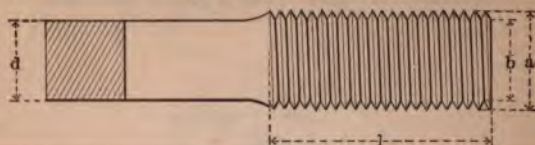
Sizes and Weights—United States Standard



DIMENSIONS		Thick- ness, Inches	SIZE OF HOLE		Size of Bolt, Inches	Weight of 100 Nuts	Number of Nuts in 100 Pounds
a	b						
$\frac{1}{2}$.71	$\frac{1}{4}$	0.185	$\frac{3}{16}$ scant	$\frac{1}{4}$	1.4	7270
$\frac{5}{16}$.84	$\frac{5}{16}$	0.240	$\frac{1}{4}$ scant	$\frac{5}{16}$	2.2	4700
$\frac{11}{16}$.97	$\frac{3}{8}$	0.294	$\frac{19}{64}$ scant	$\frac{3}{8}$	4.3	2350
$\frac{13}{16}$	1.11	$\frac{7}{16}$	0.344	$\frac{1}{2}$	$\frac{7}{16}$	6.1	1630
$\frac{7}{8}$	1.24	$\frac{1}{2}$	0.400	$\frac{13}{32}$ scant	$\frac{1}{2}$	9.0	1120
$\frac{31}{32}$	1.37	$\frac{9}{16}$	0.454	$\frac{29}{64}$	$\frac{9}{16}$	11.2	890
$1\frac{1}{16}$	1.50	$\frac{5}{8}$	0.507	$\frac{1}{2}$ full	$\frac{5}{8}$	15.6	640
$1\frac{1}{4}$	1.77	$\frac{3}{4}$	0.620	$\frac{5}{8}$ scant	$\frac{3}{4}$	26.3	380
$1\frac{7}{16}$	2.03	$\frac{7}{8}$	0.731	$\frac{47}{64}$ scant	$\frac{7}{8}$	35.7	280
$1\frac{5}{8}$	2.30	1	0.837	$\frac{27}{32}$ scant	1	58.8	170
$1\frac{3}{4}$	2.56	$1\frac{1}{8}$	0.940	$\frac{31}{16}$ full	$1\frac{1}{8}$	76.9	130
2	2.83	$1\frac{1}{4}$	1.065	$1\frac{1}{16}$ full	$1\frac{1}{4}$	104.2	96
$2\frac{1}{16}$	3.09	$1\frac{3}{8}$	1.160	$1\frac{5}{8}$ full	$1\frac{3}{8}$	142.8	70
$2\frac{3}{8}$	3.36	$1\frac{1}{2}$	1.284	$1\frac{3}{2}$ full	$1\frac{1}{2}$	172.4	58
$2\frac{5}{8}$	3.62	$1\frac{5}{8}$	1.389	$1\frac{25}{64}$ scant	$1\frac{5}{8}$	227.3	44
$2\frac{3}{4}$	3.89	$1\frac{3}{4}$	1.491	$1\frac{1}{2}$ scant	$1\frac{3}{4}$	294.1	34
$2\frac{15}{16}$	4.15	$1\frac{7}{8}$	1.616	$1\frac{5}{8}$ scant	$1\frac{7}{8}$	370.4	27
$3\frac{1}{8}$	4.42	2	1.712	$1\frac{23}{32}$ scant	2	416.7	24
$3\frac{1}{4}$	4.68	$2\frac{1}{8}$	1.836	$1\frac{27}{32}$ scant	$2\frac{1}{8}$	500.0	20
$3\frac{1}{2}$	4.95	$2\frac{1}{4}$	1.962	$1\frac{31}{32}$ scant	$2\frac{1}{4}$	588.2	17

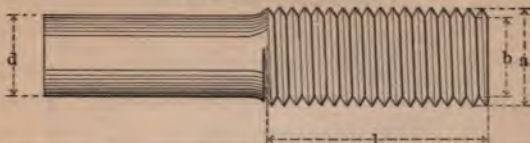
Both weights and sizes are for unfinished nuts.

Upset Screw Ends For Square Bars



BODY OF BAR				UPSET ENDS					
Side of Square <i>a</i> , Inches	Area, Square Inches	Weight per Foot, Pounds	Add for Upset, Inches	Diameter of Screw <i>a</i> , Inches	Length of Upset <i>l</i> , Inches	Area at Root of Thread, Square Inches	Diameter at Root of Thread <i>b</i> , Inches	Number of Threads per Inch	Excess of Area at Root of Thread over that of Body of Bar, %
$\frac{1}{2}$.250	.851	4	$\frac{3}{4}$	$4\frac{1}{4}$.302	.620	10	21
$\frac{5}{8}$.391	1.329	$5\frac{3}{4}$	1	$4\frac{1}{2}$.550	.837	8	41
$\frac{3}{4}$.563	1.914	$4\frac{1}{2}$	$1\frac{1}{8}$	$4\frac{3}{4}$.694	.939	7	23
$\frac{7}{8}$.766	2.605	$5\frac{3}{4}$	$1\frac{3}{8}$	5	1.057	1.160	6	38
1	1.000	3.402	$4\frac{3}{4}$	$1\frac{1}{2}$	5	1.295	1.284	6	29
$1\frac{1}{8}$	1.266	4.306	$4\frac{1}{4}$	$1\frac{5}{8}$	$5\frac{1}{4}$	1.515	1.389	$5\frac{1}{2}$	20
$1\frac{1}{4}$	1.563	5.316	$5\frac{1}{4}$	$1\frac{7}{8}$	$5\frac{1}{2}$	2.048	1.615	5	31
$1\frac{3}{8}$	1.891	6.432	$4\frac{1}{2}$	2	$5\frac{1}{2}$	2.302	1.712	$4\frac{1}{2}$	22
$1\frac{1}{2}$	2.250	7.655	$4\frac{1}{4}$	$2\frac{1}{8}$	$5\frac{3}{4}$	2.650	1.837	$4\frac{1}{2}$	18
$1\frac{5}{8}$	2.641	8.984	5	$2\frac{3}{8}$	6	3.419	2.087	$4\frac{1}{2}$	30
$1\frac{3}{4}$	3.063	10.419	$4\frac{1}{2}$	$2\frac{1}{2}$	6	3.715	2.175	4	21
$1\frac{7}{8}$	3.516	11.961	$4\frac{1}{4}$	$2\frac{5}{8}$	$6\frac{1}{4}$	4.155	2.300	4	18
2	4.000	13.610	5	$2\frac{7}{8}$	$6\frac{1}{2}$	5.108	2.550	4	28
$2\frac{1}{8}$	4.516	15.360	$4\frac{1}{2}$	3	$6\frac{1}{2}$	5.428	2.629	$3\frac{1}{2}$	20
$2\frac{1}{4}$	5.063	17.220	$4\frac{1}{4}$	$3\frac{1}{8}$	$6\frac{3}{4}$	5.957	2.754	$3\frac{1}{2}$	18
$2\frac{3}{8}$	5.641	19.190	$5\frac{1}{4}$	$3\frac{3}{8}$	7	7.087	3.004	$3\frac{1}{2}$	26
$2\frac{1}{2}$	6.250	21.260	$4\frac{3}{4}$	$3\frac{1}{2}$	7	7.548	3.100	$3\frac{1}{4}$	21
$2\frac{5}{8}$	6.891	23.440	$4\frac{1}{2}$	$3\frac{5}{8}$	$7\frac{1}{4}$	8.171	3.225	$3\frac{1}{4}$	19
$2\frac{3}{4}$	7.563	25.73	$5\frac{1}{4}$	$3\frac{7}{8}$	$7\frac{1}{2}$	9.305	3.442	3	23
$2\frac{7}{8}$	8.266	28.12	$4\frac{3}{4}$	4	$7\frac{1}{2}$	9.993	3.567	3	21
3	9.000	30.62	$4\frac{1}{2}$	$4\frac{1}{8}$	$7\frac{3}{4}$	10.706	3.692	3	19
$3\frac{1}{8}$	9.766	33.23	$5\frac{1}{4}$	$4\frac{3}{8}$	8	12.087	3.923	$2\frac{7}{8}$	24
$3\frac{1}{4}$	10.563	35.94	5	$4\frac{1}{2}$	8	12.743	4.028	$2\frac{3}{4}$	21
$3\frac{3}{8}$	11.391	38.75	5	$4\frac{5}{8}$	$8\frac{1}{4}$	13.544	4.153	$2\frac{3}{4}$	19
$3\frac{1}{2}$	12.250	41.68	$5\frac{1}{2}$	$4\frac{7}{8}$	$8\frac{1}{2}$	15.068	4.380	$2\frac{5}{8}$	23
$3\frac{5}{8}$	13.141	44.71	$5\frac{1}{4}$	5	$8\frac{1}{2}$	15.763	4.480	$2\frac{1}{2}$	20
$3\frac{3}{4}$	14.063	47.84	5	$5\frac{1}{8}$	$8\frac{3}{4}$	16.658	4.605	$2\frac{1}{2}$	18
$3\frac{7}{8}$	15.016	51.09	$4\frac{3}{4}$	$5\frac{1}{4}$	$8\frac{3}{4}$	17.572	4.731	$2\frac{1}{2}$	17
4	16.000	54.45	$5\frac{1}{4}$	$5\frac{1}{2}$	9	19.267	4.952	$2\frac{3}{8}$	20

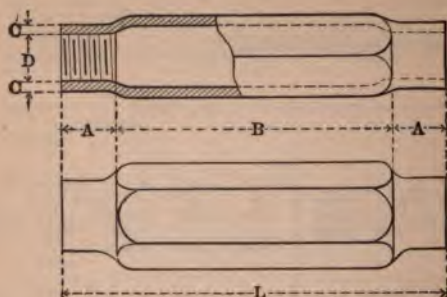
Upset Screw Ends For Round Bars



BODY OF BAR				UPSET ENDS					
Diameter <i>d</i> , Inches	Area, Square Inches	Weight per Foot, Pounds	Add for Upset, Inches	Diameter of Screw <i>a</i> , Inches	Length of Upset <i>l</i> , Inches	Area at Root of Thread, Square Inches	Diameter at Root of Thread <i>b</i> , Inches	Number of Threads per Inch	Excess of Area at Root of Thread over that of Body of Bar, %
$\frac{1}{2}$.196	.668	$6\frac{1}{2}$	$\frac{3}{4}$	$4\frac{1}{4}$.302	.620	10	54
$\frac{5}{8}$.307	1.044	$5\frac{1}{2}$	$\frac{7}{8}$	$4\frac{1}{2}$.420	.731	9	37
$\frac{3}{4}$.442	1.503	$4\frac{1}{2}$	1	$4\frac{1}{2}$.55	.837	8	25
$\frac{7}{8}$.601	2.046	$6\frac{1}{4}$	$1\frac{1}{4}$	$4\frac{3}{4}$.893	1.065	7	48
1	.785	2.672	$5\frac{1}{4}$	$\frac{13}{8}$	5	1.057	1.160	6	35
$1\frac{1}{8}$.994	3.382	$4\frac{3}{4}$	$1\frac{1}{2}$	5	1.295	1.284	6	30
$1\frac{1}{4}$	1.227	4.175	$4\frac{1}{2}$	$1\frac{5}{8}$	$5\frac{1}{4}$	1.515	1.389	$5\frac{1}{2}$	23
$1\frac{3}{8}$	1.485	5.052	4	$1\frac{3}{4}$	$5\frac{1}{4}$	1.744	1.490	5	18
$1\frac{1}{2}$	1.767	6.012	$5\frac{1}{4}$	2	$5\frac{1}{2}$	2.302	1.712	$4\frac{1}{2}$	30
$1\frac{5}{8}$	2.074	7.056	5	$2\frac{1}{8}$	$5\frac{3}{4}$	2.650	1.837	$4\frac{1}{2}$	28
$1\frac{3}{4}$	2.405	8.183	$4\frac{3}{4}$	$2\frac{1}{4}$	$5\frac{3}{4}$	3.023	1.962	$4\frac{1}{2}$	26
$1\frac{7}{8}$	2.761	9.394	$4\frac{1}{2}$	$2\frac{3}{8}$	6	3.419	2.087	$4\frac{1}{2}$	24
2	3.142	10.69	$4\frac{1}{4}$	$2\frac{1}{2}$	6	3.715	2.175	4	18
$2\frac{1}{8}$	3.547	12.06	4	$2\frac{5}{8}$	$6\frac{1}{4}$	4.155	2.300	4	17
$2\frac{1}{4}$	3.976	13.52	$5\frac{1}{4}$	$2\frac{7}{8}$	$6\frac{1}{2}$	5.108	2.550	4	28
$2\frac{3}{8}$	4.430	15.07	$4\frac{3}{4}$	3	$6\frac{1}{2}$	5.428	2.629	$3\frac{1}{2}$	23
$2\frac{1}{2}$	4.909	16.70	$4\frac{3}{4}$	$3\frac{1}{8}$	$6\frac{3}{4}$	5.957	2.754	$3\frac{1}{2}$	21
$2\frac{5}{8}$	5.412	18.41	$4\frac{1}{2}$	$3\frac{1}{4}$	$6\frac{3}{4}$	6.510	2.879	$3\frac{1}{2}$	20
$2\frac{3}{4}$	5.940	20.21	$4\frac{1}{2}$	$3\frac{3}{8}$	7	7.087	3.004	$3\frac{1}{2}$	19
$2\frac{7}{8}$	6.492	22.09	$5\frac{1}{4}$	$3\frac{5}{8}$	$7\frac{1}{4}$	8.171	3.225	$3\frac{1}{4}$	26
3	7.069	24.05	5	$3\frac{3}{4}$	$7\frac{1}{4}$	8.641	3.317	3	22
$3\frac{1}{8}$	7.670	26.10	$5\frac{1}{4}$	$3\frac{7}{8}$	$7\frac{1}{2}$	9.305	3.442	3	21
$3\frac{1}{4}$	8.296	28.23	$4\frac{3}{4}$	4	$7\frac{1}{2}$	9.993	3.567	3	20
$3\frac{3}{8}$	8.946	30.43	$4\frac{3}{4}$	$4\frac{1}{8}$	$7\frac{3}{4}$	10.706	3.692	3	20
$3\frac{1}{2}$	9.621	32.74	$4\frac{1}{2}$	$4\frac{1}{4}$	8	11.329	3.798	$2\frac{7}{8}$	18
$3\frac{5}{8}$	10.321	35.12	$5\frac{1}{4}$	$4\frac{1}{2}$	8	12.743	4.028	$2\frac{3}{4}$	23
$3\frac{3}{4}$	11.045	37.57	$5\frac{1}{4}$	$4\frac{5}{8}$	$8\frac{1}{4}$	13.544	4.153	$2\frac{3}{4}$	23
$3\frac{7}{8}$	11.793	40.13	5	$4\frac{3}{4}$	$8\frac{1}{2}$	14.220	4.255	$2\frac{3}{8}$	

Standard Sleeve Nuts

Dimensions and Weights



Size, Inches	D	L	A	B	C	Size, Inches	D	L	A	B	C
$\frac{3}{4}$	$\frac{3}{4}$	8	1	6	$\frac{1}{4}$	2	2	10	$2\frac{1}{4}$	$5\frac{1}{2}$	$\frac{1}{4}$
$\frac{7}{8}$	$\frac{7}{8}$	8	$1\frac{1}{8}$	$5\frac{3}{4}$	$\frac{1}{4}$	$2\frac{1}{8}$	$2\frac{1}{8}$	10	$2\frac{3}{8}$	$5\frac{1}{4}$	$\frac{1}{4}$
1	1	8	$1\frac{1}{4}$	$5\frac{1}{2}$	$\frac{5}{16}$	$2\frac{1}{4}$	$2\frac{1}{4}$	10	$2\frac{1}{2}$	5	$\frac{1}{4}$
$1\frac{1}{8}$	$1\frac{1}{8}$	8	$1\frac{3}{8}$	$5\frac{1}{4}$	$\frac{5}{16}$	$2\frac{3}{8}$	$2\frac{3}{8}$	10	$2\frac{5}{8}$	$4\frac{3}{4}$	$\frac{5}{16}$
$1\frac{1}{4}$	$1\frac{1}{4}$	8	$1\frac{1}{2}$	5	$\frac{5}{16}$	$2\frac{1}{2}$	$2\frac{1}{2}$	10	$2\frac{3}{4}$	$4\frac{1}{2}$	$\frac{5}{16}$
$1\frac{3}{8}$	$1\frac{3}{8}$	8	$1\frac{5}{8}$	$4\frac{3}{4}$	$\frac{3}{8}$	$2\frac{5}{8}$	$2\frac{5}{8}$	10	$2\frac{7}{8}$	$4\frac{1}{4}$	$\frac{3}{8}$
$1\frac{1}{2}$	$1\frac{1}{2}$	8	$1\frac{3}{4}$	$4\frac{1}{2}$	$\frac{3}{8}$	$2\frac{3}{4}$	$2\frac{3}{4}$	10	3	4	$\frac{5}{8}$
$1\frac{5}{8}$	$1\frac{5}{8}$	8	$1\frac{7}{8}$	$4\frac{1}{4}$	$\frac{7}{16}$	$2\frac{7}{8}$	$2\frac{7}{8}$	10	$3\frac{1}{8}$	$3\frac{3}{4}$	$\frac{5}{8}$
$1\frac{3}{4}$	$1\frac{3}{4}$	8	2	4	$\frac{7}{16}$	3	3	10	$3\frac{1}{4}$	$3\frac{1}{2}$	$\frac{11}{16}$
$1\frac{7}{8}$	$1\frac{7}{8}$	8	$2\frac{1}{8}$	$3\frac{3}{4}$	$\frac{7}{16}$

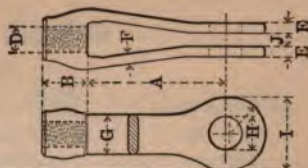
JONES & LAUGHLIN STEEL COMPANY

Standard Clevis Nuts

Dimensions and Weights

Diameter of Head for Various Given
Sizes of Pins

Used with Steel Rods 68,000 lbs. per sq. in.



D	A	B	SIZES OF PIN															
			1	1 1/4	1 1/2	1 3/4	2	2 1/4	2 1/2	2 3/4	3	3 1/4	3 1/2	3 3/4	4			
3/4	5 1/2	1 1/8	2 3/4	2 3/4	2 3/4	3
7/8	5 1/2	1 3/8	2 3/4	2 3/4	3	3
1	6	1 1/2	2 3/4	2 3/4	3	3 1/4	3 1/2
1 1/8	6	1 3/4	...	2 3/4	3	3 1/4	3 1/2	3 3/4
1 1/4	6 1/2	1 7/8	...	3	3 1/4	3 1/2	3 1/2	3 3/4
1 3/8	6 1/2	2 1/8	...	3 1/4	3 1/2	3 3/4	4	4 3/8	4 3/8
1 1/2	7	2 1/4	3 3/4	4	4 3/8	4 3/8	4 3/4
1 5/8	7	2 1/2	3 3/4	4	4 3/8	4 3/4	5 1/4
1 3/4	8	2 5/8	4 3/8	4 3/4	5 1/4	5 1/4	5 1/4
1 7/8	8	2 7/8	5 1/4	5 1/4	5 1/4	5 3/4
2	9	3	5 1/4	5 1/4	5 3/4	5 3/4	6 3/4
2 1/8	9	3 1/4	5 3/4	5 3/4	6 3/4	6 3/4	6 3/4
2 1/4	10	3 1/4	6 3/4	6 3/4	6 3/4	6 3/4
2 3/8	10	3 1/2	6 3/4	6 3/4	6 3/4	6 3/4	8
2 1/2	10	3 3/4	6 3/4	6 3/4	8	8	8
2 5/8	10	4	6 3/4	8	8	8	8	8
2 3/4	12	4 1/4	8	8	8	8	8	8	8	8	8
2 7/8	12	4 1/4	8	8	8	8	8	8	9	9	9
3	12	4 1/2	8	8	9	9	9	9	9	9

All Clevis Nuts with Diameter I—8 in. or larger Dimension A will be 12 in.

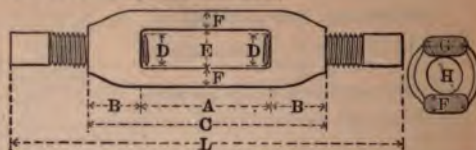
Dimension E, F, G for Various Diameters I

I	E	F	G	I	E	F	G	WEIGHTS OF CLEVISES	
								Diameter D, Inches	Weight, Pounds
2 3/4	1 7/16	1 1/2	1 1/2	4 3/4	2 5/8	2 3/8	2 1/2	3/4 to 1 1/2	5 to 8
3	1 7/16	1 1/2	1 5/8	5 1/4	2 7/8	2 3/8	2 3/4	1 5/8 to 2	9 to 15
3 1/4	1 7/16	1 5/8	1 3/4	5 3/4	2 7/8	2 3/8	3	2 1/8 to 2 1/2	20 to 25
3 1/2	1 7/16	1 5/8	1 7/8	6 3/4	2 7/8	2 3/8	3 1/4	2 5/8 to 3	30 to 40
3 3/4	1 7/16	1 5/8	2	8	2 7/8	2 3/8	4		
4	1 7/16	1 5/8	2 1/8	9	2 7/8	2 3/8	4 1/2		
4 3/8	1 7/16	1 5/8	2 1/4						

Dimension J to suit requirements.

Standard Turnbuckles

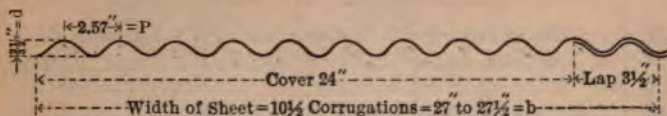
All Dimensions
Given in
Inches



Size	Clear Distance Between Heads	Length of Tapped Heads	Length of Buckle	Clear Width Inside	Thickness		Long Diameter	Length	Weight of Buckle, Pounds	Weight of Buckle & Stub Ends, Pounds
D	A	B	C	E	F	G	H	L		
$\frac{3}{8}$	6	$\frac{9}{16}$	$7\frac{1}{8}$	$\frac{9}{16}$	$\frac{3}{16}$	$\frac{1}{2}$	$1\frac{1}{16}$	22	1	$1\frac{1}{2}$
$\frac{7}{16}$	6	$\frac{3}{4}$	$7\frac{1}{2}$	$\frac{5}{8}$	$\frac{1}{4}$	$\frac{5}{8}$	$1\frac{3}{8}$	22	1	$1\frac{3}{4}$
$\frac{1}{2}$	6	$\frac{3}{4}$	$7\frac{1}{2}$	$\frac{5}{8}$	$\frac{1}{4}$	$\frac{5}{8}$	$1\frac{3}{8}$	22	1	2
$\frac{9}{16}$	6	$\frac{3}{4}$	$7\frac{1}{2}$	$\frac{5}{8}$	$\frac{1}{4}$	$\frac{3}{4}$	$1\frac{9}{16}$	22	$1\frac{1}{4}$	$2\frac{1}{2}$
$\frac{5}{8}$	6	$\frac{3}{4}$	$7\frac{1}{2}$	$\frac{5}{8}$	$\frac{1}{4}$	$\frac{3}{4}$	$1\frac{9}{16}$	22	$1\frac{1}{2}$	3
$\frac{3}{4}$	6	$1\frac{1}{8}$	$8\frac{1}{4}$	$1\frac{1}{8}$	$\frac{3}{8}$	$\frac{7}{8}$	2	23	2	4
$\frac{7}{8}$	6	$1\frac{1}{8}$	$8\frac{1}{4}$	$1\frac{1}{8}$	$\frac{3}{8}$	$\frac{7}{8}$	2	24	3	6
1	6	$1\frac{1}{2}$	9	$1\frac{5}{8}$	$\frac{7}{16}$	$1\frac{1}{4}$	$2\frac{1}{16}$	25	4	8
$1\frac{1}{8}$	6	$1\frac{1}{2}$	$9\frac{3}{8}$	$1\frac{5}{8}$	$\frac{7}{16}$	$1\frac{1}{4}$	$2\frac{1}{16}$	25	5	11
$1\frac{1}{4}$	6	$1\frac{7}{8}$	$9\frac{3}{4}$	$1\frac{9}{8}$	$\frac{1}{2}$	$1\frac{1}{2}$	$2\frac{3}{4}$	26	6	13
$1\frac{3}{8}$	6	$2\frac{1}{8}$	$10\frac{1}{8}$	$1\frac{11}{8}$	$\frac{1}{2}$	$1\frac{5}{8}$	$3\frac{1}{16}$	27	7	16
$1\frac{1}{2}$	6	$2\frac{1}{4}$	$10\frac{1}{2}$	$1\frac{5}{4}$	$\frac{5}{8}$	$1\frac{3}{4}$	$3\frac{3}{16}$	27	8	19
$1\frac{5}{8}$	6	$2\frac{1}{8}$	$10\frac{7}{8}$	2	$\frac{5}{8}$	$1\frac{7}{8}$	$3\frac{1}{2}$	28	10	23
$1\frac{3}{4}$	6	$2\frac{5}{8}$	$11\frac{1}{4}$	$2\frac{1}{8}$	$\frac{5}{8}$	2	$3\frac{3}{4}$	28	11	26
$1\frac{7}{8}$	6	$2\frac{1}{2}$	$11\frac{5}{8}$	$2\frac{3}{8}$	$\frac{11}{16}$	$2\frac{1}{8}$	$3\frac{7}{8}$	29	12	30
2	6	3	12	$2\frac{5}{8}$	$\frac{1}{2}$	$2\frac{1}{4}$	$4\frac{1}{4}$	29	14	35
$2\frac{1}{8}$	6	$3\frac{3}{8}$	$12\frac{3}{8}$	$2\frac{1}{2}$	$\frac{23}{32}$	$2\frac{1}{2}$	$4\frac{1}{2}$	29	17	41
$2\frac{1}{4}$	6	$3\frac{5}{8}$	$12\frac{3}{4}$	$2\frac{1}{2}$	$\frac{23}{32}$	$2\frac{1}{2}$	$4\frac{3}{4}$	30	20	47
$2\frac{3}{8}$	6	$3\frac{9}{8}$	$13\frac{1}{8}$	$2\frac{3}{4}$	$\frac{13}{16}$	$2\frac{3}{4}$	$4\frac{7}{8}$	31	22	53
$2\frac{1}{2}$	6	$3\frac{3}{4}$	$13\frac{1}{2}$	$3\frac{1}{8}$	$\frac{3}{2}$	3	$5\frac{5}{8}$	32	25	61
$2\frac{5}{8}$	6	$3\frac{11}{8}$	$13\frac{3}{4}$	$3\frac{1}{4}$	$\frac{15}{16}$	3	$5\frac{9}{16}$	32	30	70
$2\frac{3}{4}$	6	$4\frac{1}{8}$	$14\frac{1}{4}$	$3\frac{1}{4}$	$\frac{15}{16}$	$3\frac{1}{4}$	$5\frac{5}{4}$	33	33	78
$2\frac{7}{8}$	6	$4\frac{5}{8}$	$14\frac{3}{8}$	$3\frac{7}{8}$	$1\frac{1}{2}$	$3\frac{1}{4}$	$6\frac{1}{16}$	33	36	86
3	6	$4\frac{1}{2}$	15	$3\frac{5}{8}$	$1\frac{3}{2}$	$3\frac{1}{2}$	$6\frac{3}{8}$	34	40	96
$3\frac{1}{4}$	6	$4\frac{7}{8}$	$15\frac{3}{4}$	36	50	120
$3\frac{1}{2}$	6	$5\frac{1}{4}$	$16\frac{1}{2}$	37	65	150
$3\frac{3}{4}$	6	$5\frac{5}{8}$	$17\frac{1}{4}$	39
4	6	6	18	41
$4\frac{1}{4}$	9	$6\frac{1}{4}$	$21\frac{1}{2}$
$4\frac{1}{2}$	9	$6\frac{3}{4}$	$22\frac{1}{2}$
$4\frac{3}{4}$	9	$7\frac{1}{4}$	$23\frac{1}{2}$
5	9	$7\frac{1}{2}$	24

Dimensions E, F, G, H depend upon the specification of the bars with which the turnbuckles are to be used.

Corrugated Sheets



Note—Allowing a lap of one and one-half corrugations, one sheet will cover 24 inches.

No. by U. S. Standard Gauge	Thickness in Inches = t	Weight in Pounds						Weight per square of 100 sq. ft. of Corrugated Sheets (Black) when laid, allowing 6-inch lap in length and 3½ inches or 1½ corrugations in width of sheet for sheet length of:					
		Weights of Sheets Black			Weights of Sheets Galvanized								
		Per Sq. Ft. Flat	Per Sq. Ft. Corrugated	Per Lin. Ft. of Sheet	Per Sq. Ft. Flat	Per Sq. Ft. Corrugated	Per Lin. Ft. of Sheet						
		5'	6'	7'	8'	9	10'						
16	.0625	2.55	2.83	6.48	2.89	3.21	7.34	360	353	349	346	343	341
18	.05	2.04	2.27	5.19	2.38	2.64	6.05	288	283	280	277	275	273
20	.0375	1.53	1.70	3.89	1.87	2.07	4.75	216	212	210	208	206	205
22	.03125	1.275	1.423	2.24	1.62	1.79	4.10	180	177	175	173	171	170
24	.025	1.02	1.132	.59	1.36	1.51	3.45	144	142	140	138	137	136
26	.01875	0.765	0.851	.94	1.11	1.22	2.80	108	106	105	104	103	102

For weight of sheets painted, add 5 to 10 pounds per square of 100 square feet.

For weight of sheets galvanized, add 42 to 46 pounds per square of 100 square feet.

For weight of Clips and Rivets, add 3 per cent of weight of corrugated iron.

For weight per square laid with two laps, add to above 5 per cent.

Sheets are $30\frac{1}{2}$ inches wide before, and 27 to $27\frac{1}{2}$ inches wide after corrugating.

Sheets can be corrugated any length not exceeding 10 feet.

It is not advisable to use over 6'0" clear spans on roofs.

L = Unsupported length of sheet in inches.

t = Thickness of sheet in inches.

b = Width of sheet in inches.

d = Depth of corrugations in inches.

W = Safe load distributed in pounds.

$$W = \frac{25000 \, t \, b \, d}{L}$$

Standard Steam, Gas and Water Pipe

Nominal Size, Inches	ORDINARY PIPE			X STRONG PIPE			XX STRONG PIPE		
	Inside Diameter	Actual Outside Diameter	Weight per Foot, Pounds	Inside Diameter	Actual Outside Diameter	Weight per Foot, Pounds	Inside Diameter	Actual Outside Diameter	Weight per Foot
$\frac{1}{8}$.27	.405	.24	.205	.405	.29
$\frac{1}{4}$.364	.540	.42	.294	.540	.54
$\frac{3}{8}$.494	.675	.56	.421	.675	.74
$\frac{1}{2}$.623	.84	.84	.542	.84	1.09	.244	.84	1
$\frac{3}{4}$.824	1.05	1.12	.736	1.05	1.39	.422	1.05	2
1	1.048	1.315	1.67	.951	1.315	2.17	.587	1.315	3
$1\frac{1}{4}$	1.38	1.66	2.24	1.272	1.66	3.00	.885	1.66	5
$1\frac{1}{2}$	1.611	1.90	2.68	1.494	1.90	3.63	1.088	1.90	6
2	2.067	2.375	3.61	1.933	2.375	5.02	1.491	2.375	9
$2\frac{1}{2}$	2.468	2.875	5.74	2.315	2.875	7.67	1.755	2.875	13
3	3.067	3.50	7.54	2.892	3.50	10.25	2.284	3.50	18
$3\frac{1}{2}$	3.548	4.00	9.00	3.358	4.00	12.47	2.716	4.00	22
4	4.026	4.50	10.66	3.818	4.50	14.97	3.136	4.50	27
$4\frac{1}{2}$	4.508	5.00	12.49	4.28	5.00	18.22	3.564	5.00	32
5	5.045	5.563	14.50	4.813	5.563	20.54	4.063	5.563	38
6	6.065	6.625	18.76	5.75	6.625	28.58	4.875	6.625	53
7	7.023	7.625	23.27	6.625	7.625	37.67	5.875	7.625	62
8	7.982	8.625	28.18	7.625	8.625	43.00	6.875	8.625	71
9	8.937	9.625	33.70
10	10.019	10.75	40.00

Wooden Beams

The following tables of safe loads for wooden beams are based upon the unit stresses recommended by the American Railway Engineering Association, and are founded upon a unit having a rectangular section one inch thick, the uniformly distributed safe load for which is given in the tables. This is the most convenient arrangement as the safe load for a beam of any width can readily be found by multiplying the tabular value given for the beam one inch wide by the width of the beam for which the safe load is desired.

These loads, as given, include the weights of the beams themselves and it is assumed that the beams will be so braced as to secure them against lateral or side deflection.

There will also be found in these tables the maximum and minimum spans on which these beams should be used and the co-efficients of deflection.

The maximum load that it has been considered safe to put on these beams is that load which is indicated by the maximum allowable shearing stress along the horizontal axis of the beam. This is given by the formula—maximum safe load equals four times area of section divided by three times safe unit stress for longitudinal shear.

These limits which are indicated by horizontal lines in the tables, should not be exceeded. This will avoid the failure of the beam in a direction parallel to the grain of the wood. Usually this is in the horizontal.

The deflection under a uniformly distributed load at the center of the span is obtained by dividing the coefficient of deflection by the depth of the beam in inches. This deflection considers loads that are permanently applied only and will approximate the actual deflection, but owing to the modulus of elasticity of the material varying with the amount of moisture contained, it cannot be considered as more than approximate. It is usually considered well to limit the deflection to $1/360$ of the span where plastered ceilings are involved. This limit will also be found indicated in the tables.

For concentrated loads at center of span one-half of the tabular values should be used and four-fifths of the deflection coefficient.

Working Stresses per Square Inch for Structural Timber

The stresses per square inch, as given in this table, are based upon the stresses recommended by the American Railway Engineering Association for railroad structures.

For highway structures the stresses can be safely increased about one-fourth, while for buildings and similar structures, where the timber is protected from the effects of the weather and where the load is practically steady, these unit stresses can safely be increased by one-half.

Where beams remain under load for long continued periods only fifty per cent of the corresponding modulus of elasticity need be used in computing the deflection.

Unit Stresses in Pounds Per Square Inch

Kind of Timber	BENDING			SHEARING			COMPRESSION				
	Extreme Fiber Stress		Modulus of Elasticity	Parallel to the Grain		Longitudinal Shear in Beams	Perpendicular to the Grain		Parallel to the Grain		Working Stresses for Columns
	Average	Working		Average	Working		Elastic Limit	Working Stress	Average Ultimate	Working Stress	
Douglas Fir....	6100	1200	1510000	690	170	270	630	310	3600	1200	1200 (1 — $\frac{60d}{1}$)
Longleaf Pine...	6500	1300	1610000	720	180	300	520	260	3800	1300	1300 (1 — $\frac{60d}{1}$)
Shortleaf Pine..	5600	1100	1480000	710	170	330	340	170	3400	1100	1100 (1 — $\frac{60d}{1}$)
White Pine....	4400	900	1130000	400	100	180	290	150	3000	1000	1000 (1 — $\frac{60d}{1}$)

Unit Stresses in Pounds per Square Inch—Continued

Kind of Timber	BENDING			SHEARING				COMPRESSION				
	Extreme Fiber Stress	Modulus of Elasticity	Parallel to the Grain	Longitudinal Shear in Beams		Perpendicular to the Grain	Parallel to the Grain	Average Ultimate	Working Stress	Length under 15d	Working Stresses for Columns	Length over 15d
	Average Ultimate	Average Stress	Average Ultimate	Average Ultimate	Working Stress	Elastic Limit						
Spruce.....	4800	1000	1310000	600	150	70	370	180	3200	1100	825	1100 (1—60d)
Norway Pine...	4200	800	1190000	590*	130	100	150	2600*	800	600	800 (1—60d)
Tamarack.....	4600	900	1220000	670	170	100	220	3200*	1000	750	1000 (1—60d)
Western Hemlock....	5800	1100	1480000	630	160	270*	440	220	3500	1200	900	1200 (1—60d)
Redwood.....	5000	900	800000	300	80	400	150	3300	900	675	900 (1—60d)
Bald Cypress..	4800	900	1150000	500	120	340	170	3900	1100	825	1100 (1—60d)
Red Cedar.....	4200	800	800000	470	230	2800	900	675	900 (1—60d)
White Oak.....	5700	1100	1150000	840	210	110	920	450	3500	1300	975	1300 (1—60d)

Unit stresses are for green timber and are to be used without increasing the live load stresses for impact. Values noted * are partially air dry timbers.

In the formulae given for columns, l = length of column, in inches, and d = least side or diameter, in inches.

Wooden Beams

Examples of Use of Tables

Example 1.—Required the thickness and the approximate deflection of a beam of white pine, 16 inches deep, supporting a uniformly distributed and permanent dead and live load of 13000 pounds over a span of 20 feet.

The tabular value for a beam one inch thick and for a span of 20 feet is 1280 pounds; the required thickness is therefore $13000 \div 1280 = 10$ inches, and the deflection is $19.09 \div 16 = 1.19$ inches.

Example 2.—Required the safe load of a beam of white oak 10 inches deep and 8 inches thick, without exceeding the longitudinal shearing stress.

The table gives for a corresponding beam 1 inch thick a safe load of 1467 pounds; the total safe load is therefore $8 \times 1467 = 11736$ pounds, or the safe load which can be safely supported over a span of 8.3 feet.

Example 3.—Required the safe load, concentrated in the center of a span 25 feet long and the deflection of a beam of spruce 20 inches deep and 16 inches thick.

The table gives for a corresponding beam 1 inch thick a uniformly distributed safe load of 1422 pounds, or for a load in center of span $1778 \div 2 = 889$ pounds; for a beam 16 inches wide the safe load is therefore $889 \times 16 = 14224$ pounds, and the deflection is approximately $4/5 \times 28.63 \div 20 = 1.15$ inches.

Rectangular Wooden Beams—One Inch Thick

Greatest Safe Loads and Span Limits

Depth of Beam, Inches	White Oak		Longleaf Pine		Shortleaf Pine		White Pine		Douglas Fir		Western Hemlock		Spruce	
	Max. Load, Lbs.	Min. Span, Ft.	Max. Load, Lbs.	Min. Span, Ft.	Max. Load, Lbs.	Min. Span, Ft.	Max. Load, Lbs.	Min. Span, Ft.	Max. Load, Lbs.	Min. Span, Ft.	Max. Load, Lbs.	Min. Span, Ft.	Max. Load, Lbs.	Min. Span, Ft.
2	293	1.7	320	1.8	347	1.5	187	2.1	293	1.8	267	1.8	187	2.4
4	587	3.3	640	3.6	693	3.1	373	4.3	587	3.6	533	3.7	373	4.8
6	880	5.0	960	5.4	1040	4.6	560	6.4	880	5.5	800	5.5	560	7.1
8	1173	6.7	1280	7.2	1387	6.2	747	8.6	1173	7.3	1067	7.3	747	9.5
10	1467	8.3	1600	9.0	1733	7.7	933	10.7	1467	9.1	1333	9.2	933	11.9
12	1760	10.0	1920	10.8	2080	9.2	1120	12.9	1760	10.9	1600	11.0	1120	14.3
14	2053	11.7	2240	12.6	2427	10.8	1307	15.0	2053	12.7	1867	12.8	1307	16.7
16	2347	13.3	2560	14.4	2773	12.3	1493	17.1	2347	14.5	2133	14.7	1493	19.0
18	2640	15.0	2880	16.3	3120	13.8	1680	19.3	2640	16.4	2400	16.5	1680	21.4
20	2933	16.7	3200	18.1	3467	15.4	1867	21.4	2933	18.2	2667	18.3	1867	23.8
22	3227	18.3	3520	19.9	3813	16.9	2053	23.6	3227	20.0	2933	20.2	2053	26.2
24	3520	20.0	3840	21.7	4160	18.5	2240	25.7	3520	21.8	3200	22.0	2240	28.6

Coefficients of Deflection for Constant Loading

Span in Feet	White Oak	Long-leaf Pine	Short-leaf Pine, Western Hemlock	White Pine, Douglas Fir	Spruce	Span in Feet	White Oak	Long-leaf Pine	Short-leaf Pine, Western Hemlock	White Pine, Douglas Fir	Spruce
1	0.06	0.05	0.05	0.05	0.05	21	25.31	21.37	19.67	21.05	20.20
2	0.23	0.19	0.18	0.19	0.18	22	27.78	23.44	21.59	23.10	22.17
3	0.52	0.44	0.40	0.43	0.41	23	30.37	25.63	23.59	25.25	24.23
4	0.92	0.78	0.71	0.76	0.73	24	33.06	27.91	25.69	27.49	26.38
5	1.44	1.21	1.12	1.19	1.15	25	35.88	30.28	27.88	29.83	28.63
6	2.07	1.74	1.61	1.72	1.65	26	38.80	32.75	30.15	32.27	30.96
7	2.81	2.37	2.19	2.34	2.24	27	41.85	35.32	32.51	34.80	33.39
8	3.67	3.10	2.85	3.06	2.93	28	45.00	37.99	34.97	37.42	35.91
9	4.65	3.92	3.61	3.87	3.71	29	48.27	40.75	37.51	40.14	38.52
10	5.74	4.85	4.46	4.77	4.58	30	51.66	43.61	40.14	42.96	41.22
11	6.95	5.86	5.40	5.78	5.54	31	55.16	46.56	42.86	45.87	44.01
12	8.27	6.98	6.42	6.87	6.60	32	58.78	49.61	45.67	48.88	46.90
13	9.70	8.19	7.54	8.07	7.74	33	62.51	52.76	48.57	51.98	49.88
14	11.25	9.50	8.74	9.36	8.98	34	66.35	56.01	51.56	55.18	52.95
15	12.92	10.90	10.04	10.74	10.31	35	70.32	59.35	54.64	58.47	56.11
16	14.69	12.40	11.42	12.22	11.73	36	74.39	62.79	57.80	61.86	59.36
17	16.59	14.00	12.89	13.79	13.24	37	78.58	66.33	61.06	65.34	62.70
18	18.60	15.70	14.45	15.47	14.84	38	82.89	69.96	64.40	68.92	66.14
19	20.72	17.49	16.10	17.23	16.53	39	87.31	73.69	67.84	72.60	69.66
20	22.96	19.38	17.84	19.09	18.32	40	91.84	77.52	71.36	76.37	73.28

Greatest Span in Feet for Constant Loading

Species of Timber	Depth of Beam in Inches											
	2	4	6	8	10	12	14	16	18	20	22	24
White Oak	2.3	4.7	7.0	9.3	11.6	13.9	16.3	18.6	20.9	23.2	25.6	27.9
Longleaf Pine	2.8	5.5	8.3	11.0	13.8	16.5	19.3	22.0	24.8	27.6	30.3	33.1
Shortleaf Pine	3.0	6.0	9.0	12.0	15.0	17.9	20.9	23.9	26.9	29.9	32.9	35.9
Western Hemlock	3.0	6.0	9.0	12.0	15.0	17.9	20.9	23.9	26.9	29.9	32.9	35.9
White Pine, Douglas Fir	2.8	5.6	8.4	11.2	14.0	16.7	19.5	22.3	25.1	27.9	30.7	33.5
Spruce	2.9	5.8	8.7	11.6	14.6	17.5	20.4	23.3	26.2	29.1	32.0	34.9

Rectangular Wooden Beams—One Inch Thick

Continued

Douglas Fir

Allowable uniform loads in pounds.
Extreme fibre stress, 1200 pounds per square inch.

Span in Feet	DEPTH OF BEAM IN INCHES											
	2	4	6	8	10	12	14	16	18	20	22	24
2	293											
3	267											
4	178	587										
5	133	533										
6	107	427										
7			880									
8	89	356	800									
9	76	305	686	1173								
10	67	267	600	1067								
11		237	533	948	1467							
12		213	480	853	1333							
13						1760						
14		194	436	776	1212	1745						
15		178	400	711	1111	1600	2053					
16			369	656	1026	1477	2010					
17			343	610	952	1371	1867					
18			320	569	889	1280	1742	2276				
19												
20			300	533	833	1200	1633	2133	2640			
21				502	784	1129	1537	2008	2541			
22				474	741	1067	1452	1896	2400	2933		
23				449	702	1011	1375	1796	2274	2807	3227	
24				427	667	960	1307	1707	2160	2667	3227	
25												
26					635	914	1244	1625	2057	2540	3073	3520
27					606	873	1188	1552	1964	2424	2933	3491
28					580	835	1136	1484	1878	2319	2806	3339
29					556	800	1089	1422	1800	2222	2689	3200
30						768	1045	1365	1728	2133	2581	3072
31												
32						738	1005	1313	1662	2051	2482	2954
33						711	968	1264	1600	1975	2390	2844
34						686	933	1219	1543	1905	2305	2743
35							901	1177	1490	1839	2225	2648
36							871	1138	1440	1778	2151	2560
37												
38						843	1101	1394	1720	2082	2477	
39						817	1067	1350	1667	2017	2400	
40								1034	1309	1616	1956	2327
								1004	1271	1569	1898	2259
								975	1234	1524	1844	2194
								948	1200	1481	1793	2133
									1168	1441	1744	2076
									1137	1404	1698	2021
									1108	1368	1655	1969
									1080	1333	1613	1920

Horizontal lines indicate the limit for shear in the direction of the grain.

Rectangular Wooden Beams—One Inch Thick

Continued

Longleaf Pine

Allowable uniform loads in pounds.

Extreme fibre stress, 1300 pounds per square inch.

Span in Feet	DEPTH OF BEAM IN INCHES											
	2	4	6	8	10	12	14	16	18	20	22	24
2	320											
3	289											
4	193	640										
5	144	578										
6	116	462										
7			960									
8	96	385	867									
9	83	330	743	1280								
10	72	289	650	1156								
11		257	578	1027	1600							
12		231	520	924	1444							
13						1920						
14		210	473	840	1313	1891						
15		193	433	770	1204	1733	2240					
16			400	711	1111	1600	2178					
17			371	660	1032	1486	2022	2560				
18			347	616	963	1387	1887	2465				
19												
20			325	578	903	1300	1769	2311	2880			
21				544	850	1224	1665	2175	2753			
22				514	802	1156	1573	2054	2600	3200		
23				487	760	1095	1490	1946	2463	3041	3620	
24				462	722	1040	1416	1849	2340	2889	3496	
25												
26					688	991	1348	1761	2229	2751	3329	3840
27					657	945	1287	1681	2127	2626	3178	3782
28					628	904	1231	1608	2035	2512	3040	3617
29					602	867	1180	1541	1950	2407	2913	3467
30						832	1132	1479	1872	2311	2796	3328
31												
32						800	1089	1422	1800	2222	2689	3200
33						770	1049	1370	1733	2140	2589	3082
34						743	1011	1321	1671	2064	2497	2971
35							976	1275	1614	1992	2411	2869
36							944	1233	1560	1926	2330	2773
37												
38							913	1193	1510	1864	2255	2684
39							885	1156	1463	1806	2185	2600
40								1121	1418	1751	2119	2521
								1088	1377	1699	2056	2447
								1057	1337	1651	1998	2377
								1027	1300	1605	1942	2311
									1265	1562	1890	2249
									1232	1521	1840	2189
									1200	1482	1793	2133
									1170	1444	1748	2080

Horizontal lines indicate the limit for shear in the direction of the grain

Rectangular Wooden Beams—One Inch Thick

Continued

Shortleaf Pine, Western Hemlock and White Oak

Allowable uniform loads in pounds.

Extreme fibre stress, 1100 pounds per square inch.

Span in Feet	DEPTH OF BEAM IN INCHES											
	2	4	6	8	10	12	14	16	18	20	22	24
2	347											
3	245	693										
4	163	652										
5	122	489	1040									
6	98	391	880									
7				1387								
8	82	326	733	1304								
9	70	279	629	1117	1733							
10	61	245	550	978	1528	2080						
11		217	489	869	1358	1956	2427					
12		196	440	782	1222	1760	2396					
13		178	400	711	1111	1600	2178	2773				
14		163	367	652	1019	1467	1996	2607	3120			
15			338	602	940	1354	1843	2407	3046			
16			314	559	873	1257	1711	2235	2829	3467		
17			293	522	816	1173	1597	2086	2640	3259		
18											3813	
19			275	489	764	1100	1497	1956	2475	3055	3697	4160
20				460	719	1035	1409	1841	2329	2876	3480	4141
21				435	679	978	1331	1738	2200	2716	3287	3911
22				412	643	926	1261	1647	2084	2573	3113	3705
23				391	611	880	1198	1564	1980	2444	2958	3520
24					583	838	1141	1490	1886	2328	2817	3352
25					556	800	1089	1422	1800	2222	2689	3200
26					531	765	1042	1361	1722	2126	2572	3061
27					509	733	998	1304	1650	2037	2465	2933
28						704	958	1252	1584	1956	2366	2816
29						677	921	1203	1523	1880	2275	2708
30						652	887	1159	1467	1811	2191	2608
31						629	856	1118	1414	1746	2113	2514
32							826	1079	1366	1686	2040	2428
33							799	1043	1320	1630	1973	2348
34							773	1009	1278	1577	1908	2271
35							749	978	1238	1528	1849	2200
36								948	1200	1482	1793	2133
37								920	1165	1438	1740	2071
38								894	1131	1397	1690	2011
39								869	1100	1358	1643	1956
40									1070	1321	1599	1903
									1042	1287	1557	1853
									1015	1254	1517	1805
									990	1222	1479	1760

Upper, middle and lower horizontal lines indicate the limits for shear in the section of the grain of Shortleaf Pine, White Oak and Hemlock respectively.

Rectangular Wooden Beams—One Inch Thick

Continued

White Pine

Allowable uniform loads in pounds.

Extreme fibre stress, 900 pounds per square inch.

Span in Feet	DEPTH OF BEAM IN INCHES											
	2	4	6	8	10	12	14	16	18	20	22	24
2	187											
3	133											
4	100	373										
5	80	320										
6	67	267	560									
7	57	229	514									
8	50	200	450	747								
9		178	400	711								
10		160	360	640	933							
11		145	327	582	909							
12		133	300	533	833	1120						
13			277	492	769	1108						
14			257	457	714	1029	1307					
15			240	427	667	960	1307					
16			225	400	625	900	1225					
17				377	588	847	1153	1493				
18				356	556	800	1089	1422				
19				337	526	758	1032	1347	1680			
20				320	500	720	980	1280	1620			
21					476	686	933	1210	1543	1867		
22					455	655	891	1164	1473	1818		
23					435	626	852	1113	1409	1739	2053	
24					417	600	817	1067	1350	1667	2017	
25						576	784	1024	1296	1600	1936	2240
26						554	754	985	1246	1538	1862	2215
27						533	726	948	1200	1481	1793	2133
28						514	700	914	1157	1429	1729	2057
29							676	883	1117	1379	1669	1986
30							653	853	1080	1333	1613	1920
31							632	826	1045	1290	1561	1858
32							613	800	1013	1250	1513	1800
33								776	982	1212	1467	1746
34								753	953	1176	1424	1694
35								731	926	1143	1383	1646
36								711	900	1111	1344	1600
37									876	1081	1308	1557
38									853	1053	1274	1516
39									831	1026	1241	1477
40									810	1000	1210	1440

Horizontal lines indicate the limit for shear in the direction of the

JONES & LAUGHLIN STEEL COMPANY

Rectangular Wooden Beams—One Inch Thick

Continued

Spruce

Allowable uniform loads in pounds.
Extreme fibre stress, 1000 pounds per square inch.

Span in Feet	DEPTH OF BEAM IN INCHES											
	2	4	6	8	10	12	14	16	18	20	22	24
2	187											
3	148											
4	111	373										
5	89	356										
6	74	296										
7	63	254	560									
8	56	222	500									
9		198	444	747								
10		178	400	711								
11		162	364	646	923							
12		148	333	593	926							
13			308	547	855							
14			286	508	794	1120						
15			267	474	741	1067						
16			250	444	694	1000	1307					
17				418	654	941	1281					
18				395	617	889	1210					
19				374	585	842	1146	1493				
20				356	556	800	1089	1422				
21					529	762	1037	1354	1680			
22					505	727	990	1293	1636			
23					483	696	947	1237	1565	1867		
24					463	667	907	1185	1500	1852		
25						640	871	1138	1440	1778		
26						615	838	1094	1385	1709	2053	
27						593	807	1053	1333	1646	1992	
28						571	778	1016	1286	1587	1921	2340
29							751	981	1241	1533	1854	2207
30							726	948	1200	1481	1793	2133
31							703	918	1161	1434	1735	2065
32							681	889	1125	1389	1681	2000
33								862	1091	1347	1630	1939
34								837	1059	1307	1582	1882
35								813	1029	1270	1537	1829
36								790	1000	1235	1494	1778
37									973	1201	1453	1730
38									947	1169	1415	1684
39									923	1140	1379	1641
40									900	1111	1344	1600

Horizontal lines indicate the limit for shear in the direction of the grain.

Wooden Posts

The following tables of safe loads for wooden posts are based on the working stresses per square inch recommended by the American Railway Engineering Association, and give the recommended direct compressive load for both round and square posts.

For rectangular posts other than square, the safe loads may be found from the tables giving safe loads for the square posts by increasing the tabular load in direct proportion to the areas of the respective posts. The square post used for purposes of comparison should of course be the square whose side is equal to the least side of the rectangular section that it is proposed to use.

The table below gives the safe load in pounds per square inch of sectional area for posts having ratio of length to least side, or diameter ranging between 15 and 30.

Example—Required the allowable load for a post of white pine 6"x8", 10 ft. long. The safe load as per table for the white pine post 6"x6", 10 ft. long, is given as 18900 pounds. The load for the 6"x8" section would therefore be 8/6 of this or 25200 pounds.

Working Stresses in Pounds Per Square Inch

$\frac{l}{d}$	Longleaf Pine, White Oak	Douglas Fir, Western Hemlock	Shortleaf Pine, Spruce, Bald Cypress	White Pine, Tamarack	Red Cedar, Redwood	Norway Pine
	$1300(1-\frac{1}{60d})$	$1200(1-\frac{1}{60d})$	$1100(1-\frac{1}{60d})$	$1000(1-\frac{1}{60d})$	$900(1-\frac{1}{60d})$	$800(1-\frac{1}{60d})$
15	975	900	825	750	675	600
16	953	880	807	733	660	587
17	931	860	788	717	645	573
18	910	840	770	700	630	560
19	888	820	752	683	615	547
20	867	800	733	667	600	533
21	845	780	715	650	585	520
22	823	760	697	633	570	507
23	802	740	678	617	555	493
24	780	720	660	600	540	480
25	758	700	642	583	525	467
26	737	680	623	567	510	453
27	715	660	605	550	495	440
28	693	640	587	533	480	427
29	672	620	568	517	465	413
30	650	600	550	500	450	400

JONES & LAUGHLIN STEEL COMPANY

Square Wooden Posts Safe Loads in Thousands of Pounds

American Railway Engineering Association Formulae.

		Length, Feet	SIDE OF SQUARE, INCHES							
			4	6	8	10	12	14	16	18
LONGLEAF PINE WHITE OAK 1300 (1 — $\frac{1}{60}$)	5	15.6								
	6	15.6								
	7	14.6								
	8	13.5	35.1							
	9	12.5	34.3							
	10	11.4	32.8	62.4						
	11	10.4	31.2	62.4						
	12		29.6	60.3						
	14		28.1	58.2	97.5					
	16		25.0	54.1	93.6	140.4				
	18			49.9	88.4	137.3	191.1			
20			45.8	83.2	131.0	189.3	249.6			
			41.6	78.0	124.8	182.0	249.6	315.9	390.0	
DOUGLAS FIR WESTERN HEMLOCK 1200 (1 — $\frac{1}{60}$)	5	14.4								
	6	14.4								
	7	13.4								
	8	12.5	32.4							
	9	11.5	31.7							
	10	10.6	30.2	57.6						
	11	9.6	28.8	57.6						
	12		27.4	55.7						
	14		25.9	53.8	90.0					
	16		23.0	49.9	86.4	129.6				
	18			46.1	81.6	126.7	176.4			
20			42.2	76.8	121.0	174.7	230.4			
			38.4	72.0	115.2	168.0	230.4	291.6	360.0	
SHORTLEAF PINE SPRUCE 1100 (1 — $\frac{1}{60}$)	5	13.2								
	6	13.2								
	7	12.3								
	8	11.4	29.7							
	9	10.6	29.0							
	10	9.7	27.7	52.8						
	11	8.8	26.4	52.8						
	12		25.1	51.0						
	14		23.8	49.3	82.5					
	16		21.1	45.8	79.2	118.8				
	18			42.2	74.8	116.2	161.7			
20			38.7	70.4	110.9	160.2	211.2			
			35.2	66.0	105.6	154.0	211.2	267.3	330.0	
WHITE PINE TAMARACK 1000 (1 — $\frac{1}{60}$)	5	12.0								
	6	12.0								
	7	11.2								
	8	10.4	27.0							
	9	9.6	26.4							
	10	8.8	25.2	48.0						
	11	8.0	24.0	48.0						
	12		22.8	46.4						
	14		21.6	44.8	75.0					
	16		19.2	41.6	72.0	108.0				
	18			38.4	68.0	105.6	147.0			
20			35.2	64.0	100.8	145.6	192.0			
			32.0	60.0	96.0	140.0	192.0	243.0	300.0	

Round Wooden Posts

Safe Loads in Thousands of Pounds

American Railway Engineering Association Formulae.

		DIAMETER, INCHES								
		4	6	8	10	12	14	16	18	20
LONGLEAF PINE WHITE OAK 1300 (1 — 60d)	5	12.3								
	6	12.3								
	7	11.4								
	8	10.6	27.6							
	9	9.8	27.0							
	10	9.0	25.7	49.0						
	11	8.2	24.5	49.0						
	12		23.3	47.4						
	13		22.1	45.7	76.6					
	14		19.6	42.5	73.5	110.3				
	16			39.2	69.4	107.8	150.1			
	18			35.9	65.3	102.9	148.7	196.0		
20			32.7	61.3	98.0	142.9	196.0	248.1	306.3	
DOUGLAS FIR WESTERN HEMLOCK 1200 (1 — 60d)	5	11.3								
	6	11.3								
	7	10.6								
	8	9.8	25.4							
	9	9.1	24.9							
	10	8.3	23.7	45.2						
	11	7.5	22.6	45.2						
	12		21.5	43.7						
	13		20.4	42.2	70.7					
	14		18.1	39.2	67.9	101.8				
	16			36.2	64.1	99.5	138.5			
	18			33.2	60.3	95.0	137.2	181.0		
20			30.2	56.5	90.5	132.0	181.0	229.0	282.7	
SHORTLEAF PINE SPRUCE 1100 (1 — 60d)	5	10.4								
	6	10.4								
	7	9.7								
	8	9.0	23.3							
	9	8.3	22.8							
	10	7.6	21.8	41.5						
	11	6.9	20.7	41.5						
	12		19.7	40.1						
	13		18.7	38.7	64.8					
	14		16.6	35.9	62.2	93.3				
	16			33.2	58.7	91.2	127.0			
	18			30.4	55.3	87.1	125.8	165.9		
20			27.6	51.8	82.9	121.0	165.9	209.9	259.2	
WHITE PINE TAMARACK 1000 (1 — 60d)	5	9.4								
	6	9.4								
	7	8.8								
	8	8.2	21.2							
	9	7.5	20.7							
	10	6.9	19.8	37.7						
	11	6.3	18.9	37.7						
	12		17.9	36.4						
	13		17.0	35.2	58.9					
	14		15.1	32.7	56.5	84.8				
	16			30.2	53.4	82.9	115.5			
	18			27.6	50.3	79.2	114.4	150.8		
20			25.1	47.1	75.4	110.0	150.8	190.5		

Figures above horizontal lines indicate greatest permissible loading.

Weights of Various Materials and Loads for Storage Warehouses

Material Stored	Weights per Cubic Foot of Space, Pounds	Height of Pile, Feet	Weights per Square Foot of Floor, Pounds	Recom- mended Live Loads, Pounds per Square Foot
Groceries, Wines, Liquors, Etc.				
Beans, in bags.....	40	8	320	250 to 300
Canned Goods, in cases..	58	6	348	
Coffee, Roasted, in bags.	33	8	264	
Coffee, Green, in bags...	39	8	312	
Dates, in cases.....	55	6	330	
Figs, in cases.....	74	5	370	
Flour, in barrels.....	40	5	200	
Molasses, in barrels.....	48	5	240	
Rice, in bags.....	58	6	348	
Sal Soda, in barrels.....	46	5	230	
Salt, in bags.....	70	5	350	
Soap Powder, in cases...	38	8	304	
Starch, in barrels.....	25	6	150	
Sugar, in barrels.....	43	5	215	
Sugar, in cases.....	51	6	306	
Tea, in chests.....	25	8	200	
Wines and Liquors, in barrels.....	38	6	228	
Dry Goods, Cotton, Wool, Etc.				
Burlap, in bales.....	43	6	258	200 to 250
Coir Yarn, in bales.....	33	8	264	
Cotton, in bales, com- pressed.....	18	8	144	
Cotton Bleached Goods, in cases.....	28	8	224	
Cotton Flannel, in cases.	12	8	96	
Cotton Sheeting, in cases	23	8	184	
Cotton Yarn, in cases...	25	8	200	
Excelsior, compressed...	19	8	152	
Hemp, Italian, com- pressed.....	22	8	176	
Hemp, Manila, com- pressed.....	30	8	240	
Jute, compressed.....	41	8	328	

Continued on next page.

Weights of Various Materials and Loads for Storage Warehouses

Continued

Material Stored	Weights per Cubic Foot of Space, Pounds	Height of Pile, Feet	Weights per Square Foot of Floor, Pounds	Recom- mended Live Loads, Pounds per Square Foot
y Goods, Cotton, Wool, Etc.				
Continued				
1 Damask, in cases...	50	5	250	200 to 250
1 Goods, in cases...	30	8	240	
1 Towels, in cases...	40	6	240	
, compressed.....	21	8	168	
, compressed.....	29	8	232	
, in bales, com- pressed.....	48	
, in bales, not com- pressed.....	13	8	104	300 to 400
, Worsteds, in cases.	27	8	216	
uilding Materials				
ent, Natural.....	59	6	354	300 to 400
ent, Portland.....	73	6	438	
and Plaster.....	53	5	265	
Hardware, Etc.				
Checks.....	45	300 to 400
es.....	64	
s, in cases, packed..	31	
Fasteners.....	48	
ws.....	101	
t Tin, in boxes.....	278	2	556	
Cables, on reels....	425	300 to 400
, Insulated Copper, coils.....	63	5	315	
, Galvanized Iron, in ls.....	74	4½	333	
, Magnet, on spools..	75	6	450	

ntinued on next page.

Weights of Various Materials and Loads for Storage Warehouses

Continued

Material Stored	Weights per Cubic Foot of Space, Pounds	Height of Pile, Feet	Weights per Square Foot of Floor, Pounds	Recom- mended Live Loads, Pounds per Square Foot
Drugs, Paints, Oil, Etc.				
Alum, Pearl, in barrels...	33	6	198	200 to 300
Bleaching Powder, in hogsheads.....	31	3½	102	
Blue Vitriol, in barrels..	45	5	226	
Glycerine, in cases.....	52	6	312	
Linseed Oil, in barrels...	36	6	216	
Linseed Oil, in iron drums	45	4	180	
Logwood Extract, in boxes.....	70	5	350	
Rosin, in barrels.....	48	6	288	
Shellac, Gum.....	38	6	228	
Soda Ash, in hogsheads..	62	2¾	167	
Soda, Caustic, in iron drums.....	88	3½	294	
Soda, Silicate, in barrels.	53	6	318	
Sulphuric Acid.....	60	1½	100	
White Lead Paste, in cans	174	3½	610	
White Lead, dry.....	86	4¾	408	
Red Lead and Litharge, dry.....	132	3¾	495	
Miscellaneous				
Glass and Chinaware, in crates.....	40	8	320	300
Hides and Leather, in bales.....	20	8	160	
Hides, Buffalo, in bundles	37	8	296	
Paper, Newspaper, and Strawboards.....	35	6	210	
Paper, Writing and Cal- endered.....	60	6	360	
Rope, in coils.....	32	6	192	

Expansion of Bodies by Heat

The linear coefficient of expansion of a body is the rate at which the unit of length changes, under constant pressure, with an increase of unit or one degree of temperature. The square surface coefficient of expansion is, approximately, two times and the cubical or volumetric coefficient three times the linear coefficient of expansion. A bar, if not fixed, undergoes a change in length = ln , where l is the length of the bar in inches, t the number of degrees and n the corresponding linear coefficient. If fixed at both ends, the internal stress per unit of area = tnE , pounds per square inch, where E is the modulus of elasticity, and the total temperature stress = $AtnE$, pounds, where A is the cross section of the bar in square inches.

To find the increase of a bar due to an increase in temperature, from the following table, multiply the number of degrees by the coefficient given for 100 degrees and divide by 100.

Co-efficients of Expansion for 100 Degrees = $100n$

Substance	Linear Expansion		Substance	Linear Expansion	
	Centi- grade	Fahren- heit		Centi- grade	Fahren- heit
Metals and Alloys			Stone and Masonry		
Aluminum, wrought	.00231	.00128	Ashlar masonry	.00063	.00035
Brass	.00188	.00104	Brick masonry	.00055	.00031
" wire	.00193	.00107	Cement, Portland	.00107	.00059
Bronze	.00181	.00101	Concrete	.00143	.00079
Copper	.00168	.00093	" masonry	.00120	.00067
German Silver	.00183	.00102	Granite	.00084	.00047
Gold	.00150	.00083	Limestone	.00080	.00044
Iron, cast, gray	.00106	.00059	Marble	.00100	.00056
" wrought	.00120	.00067	Plaster	.00166	.00092
" wire	.00124	.00069	Rubble masonry	.00063	.00035
Lead	.00286	.00159	Sandstone	.00110	.00061
Nickel	.00126	.00070	Slate	.00104	.00058
Platinum	.00090	.00050	Timber		
Platinum-Iridium, 15%			Fir	.00037	.00021
Ir	.00081	.00045	Maple	.00064	.00036
Silver	.00192	.00107	Oak	.00049	.00027
Steel, cast	.00110	.00061	Pine	.00054	.00030
" hard	.00132	.00073	Fir	.00058	.00032
" medium	.00120	.00067	Maple	.00048	.00027
" soft	.00110	.00061	Oak	.00054	.00030
Tin	.00210	.00117	Pine	.00034	.00019
Zinc, rolled	.00311	.00173	Liquid Substances		
Miscellaneous Solids			Volumetric Expansion		
Glass	.00085	.00047	Alcohol	.104	.058
Graphite	.00079	.00044	Acid, nitric	.110	.061
Gutta-percha	.05980	.03322	" sulphuric	.063	.035
Paraffin	.02785	.01547	Mercury	.018	.010
Porcelain	.00036	.00020	Oil, turpentine	.090	.050

Expansion of Water, Maximum Density = 1.

C°	Volume	C°	Volume	C°	Volume	C°	Volume	C°	Volume	C°	Volume
0	1.000126	10	1.000257	30	1.004234	50	1.011877	70	1.022384	90	1.036383
4	1.000000	20	1.001732	40	1.007627	60	1.016954	80	1.029033	100	1.043000

Weight and Specific Gravity

Various Materials

Water at 39.2° F.

Substance	Specific Gravity	Weight per Cu. Ft. Lbs.	Substance	Specific Gravity	Weight per Cu. Ft. Lbs.
Metals, Alloys, Ores			Various Solids Continued		
Aluminum, cast-hammered.....	2.55-2.75	165	Leather.....	0.86-1.02	59
Aluminum, bronze.....	7.7	481	Paper.....	0.70-1.15	58
Brass, cast-rolled.....	8.4-8.7	534	Potatoes, piled.....		42
Bronze, 7.9 to 14% Sn.....	7.4-8.9	509	Rubber, caoutchouc.....	0.92-0.96	59
Copper, cast-rolled.....	8.8-9.0	556	Rubber goods.....	1.0-2.0	94
" ore, pyrites.....	4.1-4.3	262	Salt, granulated, piled.....	.77	48
Gold, cast-hammered.....	19.25-19.35	1205	Saltpeter.....	1.07	67
Iron, cast, pig.....	7.2	450	Starch.....	1.53	96
" wrought.....	7.6-7.9	485	Sulphur.....	1.93-2.07	125
" steel.....	7.8-7.9	490	Wool.....	1.32	82
" Spiegel-Eisen.....	7.5	468			
" ferro-silicon.....	6.7-7.3	437	Timber, U. S.		
" ore, hematite.....	5.2	325	Seasoned		
" limonite.....	3.6-4.0	237	Ash, white-red.....	0.62-0.65	40
" magnetite.....	4.9-5.2	315	Cedar, white-red.....	0.32-0.38	22
" slag.....	2.5-3.0	172	Chestnut.....	0.66	41
Lead.....	11.37	710	Cypress.....	0.48	30
" ore, Galena.....	7.3-7.6	465	Fir, Douglas spruce.....	0.51	32
Manganese.....	7.2-8.0	475	" eastern.....	0.40	25
" ore, pyrolusite.....	3.7-4.6	259	Elm, white.....	0.72	45
Mercury.....	13.6	849	Hemlock.....	0.42-0.52	29
Nickel.....	8.9-9.2	565	Hickory.....	0.74-0.84	49
" monel metal.....	8.8-9.0	556	Locust.....	0.73	46
Platinum, cast-hammered.....	21.1-21.5	1330	Maple, hard.....	0.68	43
Silver, cast-hammered.....	10.4-10.6	656	" white.....	0.53	33
Tin, cast-hammered.....	7.2-7.5	459	Oak, chestnut.....	0.86	54
" ore, cassiterite.....	6.4-7.0	418	" live.....	0.95	59
Zinc, cast-rolled.....	6.9-7.2	440	" red, black.....	0.65	41
" ore, blende.....	3.9-4.2	253	" white.....	0.74	46
Various Solids			Pine, Oregon.....	0.51	32
Cereals, oats, bulk.....		32	" red.....	0.48	30
" barley, bulk.....		39	" white.....	0.41	26
" corn, rye, bulk.....		48	" yellow, longleaf.....	0.70	44
" wheat, bulk.....		48	" shortleaf.....	0.61	38
Hay and Straw, bales.....		20	Poplar.....	0.48	30
Cotton, Flax, Hemp.....	1.47-1.50	93	Redwood, California.....	0.42	26
Fats.....	0.90-0.97	58	Spruce, white, black.....	0.40-0.46	27
Flour, loose.....	0.40-0.50	28	Walnut, black.....	0.61	38
" pressed.....	0.70-0.80	47	" white.....	0.41	26
Glass, common.....	2.40-2.60	156	MOISTURE CONTENTS:		
" plate or crown.....	2.45-2.72	161	Seasoned timber 15		
" crystal.....	2.90-3.00	184	to 20%.....		
			Green timber up		
			to 50%.....		

continued on next page.

Weight and Specific Gravity

Various Materials

Continued

Water at 39.2° F.

Substance	Specific Gravity	Weight per Cu. Ft. Lbs.	Substance	Specific Gravity	Weight per Cu. Ft., Lbs.
Various Liquids			Brick Masonry		
Alcohol, 100%.....	0.79	49	Pressed brick.....	2.2-2.3	140
Acids, muriatic...40%.	1.20	75	Common brick.....	1.8-2.0	120
" nitric.....91%.	1.50	94	Soft brick.....	1.5-1.7	100
" sulphuric..87%.	1.80	112			
Lye, soda.....66%.	1.70	106			
Oils, vegetable.....	0.91-0.94	58			
" mineral, lubricants	0.90-0.93	57			
Water, 4°C, max. density	1.0	62.428			
" 100°C.....	0.9584	59.830	Concrete Masonry		
" ice.....	0.88-0.92	56	Cement, stone, sand...	2.2-2.4	144
" snow, fresh fallen	.125	8	" slag, etc.....	1.9-2.3	130
" sea water.....	1.02-1.03	64	" cinder, etc...	1.5-1.7	100
Gases, Air=1			Various Building Material		
Air, 0°C, 760 mm.....	1.0	1/773	Ashes, cinders.....		40-45
Ammonia.....	0.5920		Cement, Portland,		
Carbon dioxide.....	1.5291		loose.....		90
Carbon monoxide.....	0.9673		Cement, Portland, set.	2.7-3.2	183
Gas, illuminating.....	0.35-0.45		Lime, gypsum, loose..		53-64
" natural.....	0.47-0.48		Mortar, set.....	1.4-1.9	103
Hydrogen.....	0.0693		Slags, bank slag.....		67-72
Nitrogen.....	0.9714		" bank screenings..		98-117
Oxygen.....	1.1056		" machine slag.....		96
			" slag sand.....		49-55
Ashlar Masonry			Excavated Earth, Etc.,		
Granite, syenite, gneiss	2.3-3.0	165	Clay, dry.....		63
Limestone, marble....	2.3-2.8	160	" damp, plastic.....		110
Sandstone, bluestone..	2.1-2.4	140	Clay and gravel, dry..		100
			Earth, dry, loose.....		76
			" dry, packed.....		95
			" moist, loose.....		78
			" moist, packed.....		96
			" mud, flowing.....		108
			" mud, packed.....		115
			Riprap, limestone.....		80-85
			" sandstone.....		90
			" shale.....		105
			Sand, gravel, dry, loose		90-105
			" " " packed.....		100-120
			" " " wet.....		118-120
Mortar Rubble Masonry					
Granite, syenite, gneiss	2.2-2.8	155			
Limestone, marble....	2.2-2.6	150			
Sandstone, bluestone..	2.0-2.2	130			
Dry Rubble Masonry					
Granite, syenite, gneiss	1.9-2.3	130			
Limestone, marble....	1.9-2.1	125			
Sandstone, bluestone..	1.8-1.9	110			

Continued on next page.

Weight and Specific Gravity

Various Materials

Continued

Water at 39.2° F.

Substance	Specific Gravity	Weight, per Cu. Ft. Lbs.	Substance	Specific Gravity	Weight per Cu. Ft. Lbs.
Excavations in Water			Stone, Quarried, Piled		
Sand or gravel.....		60	Basalt, granite gneiss.....		96
Sand or gravel and clay.....		65	Limestone, marble, quartz.....		95
Clay.....		80	Sandstone.....		82
River mud.....		90	Shale.....		92
Soil.....		70	Greenstone, hornblende.....		107
Stone riprap.....		65	Bituminous Substances		
Minerals			Asphaltum.....	1.1-1.5	81
Asbestos.....	2.1-2.8	153	Coal, anthracite.....	1.4-1.7	97
Barytes.....	4.50	281	" bituminous.....	1.2-1.5	84
Basalt.....	2.7-3.2	184	" lignite.....	1.1-1.4	78
Bauxite.....	2.55	159	" peat, turf, dry.....	0.65-0.85	47
Borax.....	1.7-1.8	109	" charcoal, pine.....	0.28-0.44	23
Chalk.....	1.8-2.6	137	" oak.....	0.47-0.57	33
Clay, marl.....	1.8-2.6	137	" coke.....	1.0-1.4	75
Dolomite.....	2.9	181	Graphite.....	1.9-2.3	131
Feldspar, orthoclase.....	2.5-2.6	159	Paraffine.....	0.87-0.91	56
Gneiss, serpentine.....	2.4-2.7	159	Petroleum.....	0.87	54
Granite, syenite.....	2.5-3.1	175	" refined.....	0.79-0.82	50
Greenstone, trap.....	2.8-3.2	187	" benzine.....	0.73-0.75	46
Gypsum, alabaster.....	2.3-2.8	159	" gasoline.....	0.66-0.69	42
Hornblende.....	3.0	187	Pitch.....	1.07-1.15	69
Limestone, marble.....	2.5-2.8	165	Tar, bituminous.....	1.20	75
Magnesite.....	3.0	187	Coal and Coke, Piled		
Phosphate rock apatite.....	3.2	200	Coal, anthracite.....		47-58
Porphyry.....	2.6-2.9	172	" bituminous.....		40-54
Pumice, natural.....	0.37-0.90	40	" lignite.....		20-26
Quartz, flint.....	2.5-2.8	165	" peat, turf.....		10-14
Sandstone, bluestone.....	2.2-2.5	147	" charcoal.....		23-32
Shale, slate.....	2.7-2.9	175	" coke.....		
Soapstone, talc.....	2.6-2.8	169			

Strength of Materials

Stresses Per Square Inch

METALS AND ALLOYS	STRESSES IN THOUSANDS OF POUNDS					Modulus of Elasticity, Pounds	Elongation, %
	Tension, Ultimate	Elastic Limit	Compression, Ultimate	Bending, Ultimate	Shearing, Ultimate		
Aluminum, cast.....	15	6.5	12	12	11,000,000
" bars, sheets.....	24-28	12-14
" wire, hard.....	30-65	16-30
" wire, annealed.....	20-35	14
" Bronze, 5% to 7½% Alumin.	75	40	120
" " 10% Aluminum.....	85-100	60
Copper, cast.....	25	6	40	22	30	10,000,000
" plates, rods, bolts.....	32-35	10	32
" wire, hard.....	55-65	18,000,000
" wire, annealed.....	36	10	15,000,000
Brass, 17% Zinc.....	32.6	8.2	23.2	26.7
" 23% ".....	7.6	42	22.3	35.8
" 30% ".....	28.1	8.6	26.9	20.7
" 39% ".....	41.1	17.4	75	39	20.7
" 50% ".....	31	17.9	117	33.5	5.0
" cast, common.....	18-24	6	30	20	36	9,000,000
" wire, hard.....	80
" wire, annealed.....	50	16	14,000,000
Bronze 8% Tin.....	28.5	19	42	43.7	10,000,000	5.5
" 13% ".....	29.4	20	53	34.5	3.3
" 20% ".....	33	78	56.7	0.04
" 24% ".....	22	22	114	32	0.
" 30% ".....	5.6	5.6	147	12.1	0.
" gun metal, 9 Copper, 1 Tin.....	25-55	10	52	10,000,000
" Manganese, cast 10% Tin.....	60	30	125
" " rolled 2% Mn.....	100	80
" Phosphorus, cast 9% Tin.....	50	24
" " wire 1% Phos.....	100
" Silicon, cast, 3% Silicon.....	55
" " 5% Silicon.....	75
" " wire.....	108
" Tobin, cast 38% Zinc.....	66
" " rolled 1½% Tin.....	80	40	4,500,000
" " cold rolled 1½% Lead.....	100
Delta Metal, cast 55-60% Copper.....	45
" plates 38-40% Zinc.....	68
" bars 2-4% Iron.....	85
" wire 1-2% Tin.....	100
German Silver, 25% Zinc, 20% Nickel.....
Gold, cast.....	20	4	8,000,000
" wire.....	30
" copper, 5 gold, 1 copper.....	50
Lead, cast.....	1.8	1,000,000
" pipe, wire.....	2.2-2.5	1,000,000
" rolled sheets.....	3.3	720,000
Platinum, wire, unannealed.....	53
" annealed.....	32
Silver, cast.....	40
Tin, cast.....	3.5-4.6	1.5-1.8	6	4	4,000,000
" antimony, 10 tin, 1 antimony.....	11
Zinc, cast.....	4-6	4	18	7	13,000,000
" rolled sheets.....	7-16

Strength of Materials

Continued

Stresses in Pounds per Square Inch

BUILDING MATERIALS	AVERAGE ULTIMATE STRESSES			Modulus of Elasticity	SAFE WORKING STRESSES		
	Com-press.	Tension	Bending		Com-press.	Bearing	Shearing
Stone							
Bluestone.....	12,000	1,200	2,500	7,000,000	1,200	1,200	200
Granite, gneiss.....	12,000	1,200	1,600	7,000,000	1,200	1,200	200
Limestone, marble....	8,000	800	1,500	7,000,000	800	800	150
Sandstone.....	5,000	150	1,200	3,000,000	500	500	150
Slate.....	10,000	3,000	5,000	14,000,000	1,000	1,000	175
Brick							
Common, good.....	10,000	200	600				
" medium burned.....	11,000						
" hard burned.....	15,000						
Pressed and paving....	6,000						
Cement, Portland							
Neat, 28 days.....	7,040	740					
" 90 days.....	7,350	740					
1:3 sand, 28 days.....	1,290	320					
" 90 days.....	1,490	340					
Concrete, P. C.							
1:1½:3, hard stone....	2,650			Elastic	2,000,000 if ult. compression is up to 2,200.		
" soft stone.....	1,800			Modulus	2,500,000 if ult. compression is over 2,200.		
" cinders.....	700				3,000,000 if ult. compression is over 2,900.		
1:2:4, hard stone....	2,100			Com-pression	22.5% of ult. compression on piers or columns of lengths not exceeding 12 dia.		
" soft stone.....	1,500				32.5% of ult. compression on surfaces of at least twice the loaded area.		
" cinders.....	600			Bearing	2.0% of ult. compression, horizontal bars.		
1:2½:5, hard stone....	1,700				3.0% for reinforcement with bent-up bars.		
" soft stone.....	1,200			Shearing	6.0% for thoroughly reinforced webs.		
" cinders.....	500				4% of ult. compression for plain bars.		
1:3:6, hard stone....	1,350			Bond....	2% for drawn wire.		
" soft stone.....	1,000						
" cinders.....	400						
Masonry							
Granite.....					420	600	
Limestone, bluestone..					350	500	
Sandstone.....					280	400	
Rubble.....					140	250	
" coursed.....					168	250	
Concrete, P.C., 1:2:4..					350	600	
" 1:2½:5.....					280	500	
Brick, common.....					168	300	
" hard burned....					210	300	
Miscellaneous							
Glass, common.....	30,000	3,000	3,000	8,000,000			
" flooring.....	10,000	3,000	3,000				
Plaster.....	700	70					
Terra cotta.....	5,000						
Ropes, cast steel hoist.		80,000					
Ropes, standing, der'k		70,000					
Ropes, Manila.....		8,000					
Belts, sol. woven, cot'n		7,300					
Belts, solid woven flax		9,900					

For ultimate and working stresses of Structural Timber, see page 272.

United States Standard Gauge

For Sheet and Plate Iron and Steel

Gauge Number	Thickness in Fractions of an Inch	Thickness in Decimals of an Inch	Approximate Thickness in Millimeters	Weight per Square Foot, in Pounds, Iron	Weight per Square Foot, in Pounds, Steel	Weight per Square Meter, in Kilograms, Steel
0000000	$\frac{1}{32}$.5	12.70	20.	20.4	99.601
000000	$\frac{1}{16}$.46875	11.91	18.75	19.125	93.376
00000	$\frac{3}{32}$.4375	11.11	17.50	17.85	87.151
0000	$\frac{1}{8}$.40625	10.32	16.25	16.575	80.926
000	$\frac{3}{16}$.375	9.53	15.	15.3	74.701
00	$\frac{1}{4}$.34375	8.73	13.75	14.025	68.476
0	$\frac{3}{8}$.3125	7.94	12.50	12.75	62.251
1	$\frac{7}{16}$.28125	7.14	11.25	11.475	56.026
2	$\frac{1}{2}$.265625	6.75	10.625	10.8375	52.913
3	$\frac{5}{8}$.25	6.35	10.	10.2	49.800
4	$\frac{3}{4}$.234375	5.95	9.375	9.5625	46.688
5	$\frac{7}{8}$.21875	5.56	8.75	8.925	43.575
6	$\frac{15}{16}$.203125	5.16	8.125	8.2875	40.463
7	1	.1875	4.76	7.5	7.65	37.350
8	$1\frac{1}{16}$.171875	4.37	6.875	7.0125	34.238
9	$1\frac{1}{8}$.15625	3.97	6.25	6.375	31.125
10	$1\frac{1}{4}$.140625	3.57	5.625	5.7375	28.013
11	$1\frac{3}{8}$.125	3.18	5.	5.1	24.900
12	$1\frac{1}{2}$.109375	2.78	4.375	4.4625	21.788
13	$1\frac{5}{8}$.09375	2.38	3.75	3.825	18.675
14	$1\frac{3}{4}$.078125	1.98	3.125	3.1875	15.563
15	$1\frac{7}{8}$.0703125	1.79	2.8125	2.86875	14.006
16	2	.0625	1.59	2.5	2.55	12.450
17	$2\frac{1}{16}$.05625	1.43	2.25	2.295	11.205
18	$2\frac{1}{8}$.05	1.27	2.	2.04	9.960
19	$2\frac{1}{4}$.04375	1.11	1.75	1.785	8.715
20	$2\frac{3}{8}$.0375	0.953	1.50	1.53	7.470
21	$2\frac{1}{2}$.034375	0.873	1.375	1.4025	6.848
22	$2\frac{5}{8}$.03125	0.794	1.25	1.275	6.225
23	$2\frac{3}{4}$.028125	0.714	1.125	1.1475	5.603
24	$2\frac{7}{8}$.025	0.635	1.	1.02	4.980
25	3	.021875	0.556	.875	.8925	4.358
26	$3\frac{1}{16}$.01875	0.476	.75	.765	3.735
27	$3\frac{1}{8}$.0171875	0.437	.6875	.70125	3.424
28	$3\frac{1}{4}$.015625	0.397	.625	.6375	3.113
29	$3\frac{3}{8}$.0140625	0.357	.5625	.57375	2.801
30	$3\frac{1}{2}$.0125	0.318	.5	.51	2.490
31	$3\frac{5}{8}$.0109375	0.278	.4375	.44625	2.179
32	$3\frac{3}{4}$.01015625	0.258	.40625	.414375	2.023
33	$3\frac{7}{8}$.009375	0.238	.375	.3825	1.868
34	4	.00859375	0.218	.34375	.350625	1.712
35	$4\frac{1}{16}$.0078125	0.198	.3125	.31875	1.556
36	$4\frac{1}{8}$.00703125	0.179	.28125	.286875	1.401
37	$4\frac{3}{8}$.006640625	0.169	.265625	.2709375	1.323
38	$4\frac{1}{2}$.00625	0.159	.25	.255	1.245

The United States Standard Gauge was legalized by Act of Congress March 3, 1893, as a standard gauge for sheet and plate iron and steel.

Since the use of numbers to express thickness or size leads to confusion, decimal parts of an inch should be employed when fractions can not be used conveniently.

Birmingham Wire Gauge
Equivalents in Inches
Corresponding Weights of Flat Rolled Steel

Gauge Number	Thickness, Inches	Pounds per Square Foot	THICKNESS, INCHES		Pounds per Square Foot
			Fractional	Decimal	
.....	$\frac{1}{2}$.5	20.4
0000	.454	18.5232	$\frac{11}{16}$.46875	19.125
000	.425	17.34	$\frac{3}{4}$.4375	17.85
..	$\frac{5}{8}$.40625	16.575
00	.380	15.504	$\frac{7}{8}$.375	15.3
0	.340	13.872	$\frac{1}{2}$.34375	14.025
.....	$\frac{5}{16}$.3125	12.75
1	.300	12.24	$\frac{3}{8}$.296875	12.1125
2	.284	11.5872	$\frac{1}{4}$.28125	11.475
3	.259	10.5672	$\frac{3}{16}$.265625	10.8375
..	$\frac{1}{8}$.25	10.2
4	.238	9.7104	$\frac{3}{16}$.234375	9.5625
5	.220	8.976	$\frac{1}{4}$.21875	8.925
6	.203	8.2824	$\frac{5}{16}$.203125	8.2875
7	.180	7.344	$\frac{3}{8}$.1875	7.65
8	.165	6.732	$\frac{1}{2}$.171875	7.0125
9	.148	6.0384	$\frac{5}{8}$.15625	6.375
10	.134	5.4672	$\frac{3}{4}$.140625	5.7375
11	.120	4.896	$\frac{7}{8}$.125	5.1
12	.109	4.4472	$\frac{1}{2}$.109375	4.4625
13	.095	3.876	$\frac{3}{4}$.09375	3.825
14	.083	3.3864	$\frac{5}{8}$.078125	3.1875
15	.072	2.9376
16	.065	2.651	$\frac{1}{2}$.0625	2.55
17	.058	2.3664
18	.049	1.9992	$\frac{3}{4}$.046875	1.9125
19	.042	1.7136
20	.035	1.428
21	.032	1.3056	$\frac{1}{2}$.03125	1.275
22	.028	1.1424
23	.025	1.02
24	.022	0.8976
25	.020	0.816
26	.018	0.7344
27	.016	0.6528	$\frac{3}{4}$.015625	0.6375
28	.014	0.5712
29	.013	0.5304
30	.012	0.4896
31	.010	0.408
32	.009	0.3672
33	.008	0.3264	$\frac{1}{2}$.0078125	0.31875
34	.007	0.2856
35	.005	0.2040
36	.004	0.1632	$\frac{1}{4}$.00390625	0.159375

Comparison of Gauges In Decimal Parts of an Inch

Gauge Number	J & L Gauge	Birmingham Wire (B.W.G.) also known as Stubbs Iron Wire	American Wire or Browne & Sharpe	British Imperial Standard Wire (S. W. G.)	Standard Birmingham Sheet and Hoop (B. G.)	United States Standard for Sheet and Plate Iron and Steel
0000000	.4900500500
000000	.4615580000	.46446875
00000	.4305516500	.4324375
0000	.3938	.500	.460000	.40040625
000	.3625	.425	.409642	.372	.5000	.375
00	.3310	.380	.364796	.348	.4452	.34375
0	.3065	.340	.324861	.324	.3964	.3125
1	.2830	.300	.289297	.300	.3532	.28125
2	.2625	.284	.257627	.276	.3147	.265625
3	.2437	.259	.229423	.252	.2804	.25
4	.2253	.238	.204307	.232	.2500	.234375
5	.2070	.220	.181940	.212	.2225	.21875
6	.1920	.203	.162023	.192	.1981	.203125
7	.1770	.180	.144285	.176	.1764	.1875
8	.1620	.165	.128490	.160	.1570	.171875
9	.1483	.148	.114423	.144	.1398	.15625
10	.1350	.134	.101897	.128	.1250	.140625
11	.1205	.120	.090742	.116	.1113	.125
12	.1055	.109	.080808	.104	.0991	.109375
13	.0915	.095	.071962	.092	.0882	.09375
14	.0800	.083	.064084	.080	.0785	.078125
15	.0720	.072	.057068	.072	.0699	.0703125
16	.0625	.065	.050821	.064	.0625	.0625
17	.0540	.058	.045257	.056	.0556	.05625
18	.0475	.049	.040303	.048	.0495	.05
19	.0410	.042	.035890	.040	.0440	.04375
20	.0348	.035	.031961	.036	.0392	.0375
21	.03175	.032	.028462	.032	.0349	.034375
22	.0286	.028	.025346	.028	.03125	.03125
23	.0258	.025	.022572	.024	.02782	.028125
24	.0230	.022	.020101	.022	.02476	.025
25	.0204	.020	.017900	.020	.02204	.021875
26	.0181	.018	.015941	.018	.01961	.01875
27	.0173	.016	.014195	.0164	.01745	.0171875
28	.0162	.014	.012641	.0148	.015625	.015625
29	.0150	.013	.011257	.0136	.0139	.0140625
30	.0140	.012	.010025	.0124	.0123	.0125
31	.0132	.010	.008928	.0116	.0110	.0109375
32	.0128	.009	.007950	.0108	.0098	.01015625
33	.0118	.008	.007080	.0100	.0087	.009375
34	.0104	.007	.006305	.0092	.0077	.00859375
35	.0095	.005	.005615	.0084	.0069	.0078125
36	.0090	.004	.005000	.0076	.0061	.00703125
37	.0085004453	.0068	.0054	.006640625
38	.0080003965	.0060	.0048	.00625
39	.0075003531	.0052
40	.0070003144	.0048

Birmingham Wire Gauge is used for No. 8, No. 9 and No. 10 sheared plates also bands and hoops.

United States Standard Gauge is used for No. 11 sheared plates also for Black Plates (Tin mill sizes). Tin Plate is rolled to weight per base box.

J & L Gauge, which corresponds to Washburn & Moen Gauge, is used for all common wire products, unless otherwise specified.

Since the use of numbers to express thickness or size leads to confusion, parts of an inch should be employed when fractions can not be used conveniently.

Comparison of Inches and Fractions With Decimals of a Foot

Inch	0"	1"	2"	3"	4"	5"	6"	7"	8"	9"	10"	11"
0	.0	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167
$\frac{1}{16}$.0013	.0846	.1680	.2513	.3346	.4180	.5013	.5846	.6680	.7513	.8346	.9180
$\frac{1}{8}$.0026	.0859	.1693	.2526	.3359	.4193	.5026	.5859	.6693	.7526	.8359	.9193
$\frac{3}{16}$.0039	.0872	.1706	.2539	.3372	.4206	.5039	.5872	.6706	.7539	.8372	.9206
$\frac{1}{4}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219
$\frac{5}{16}$.0065	.0898	.1732	.2565	.3398	.4232	.5065	.5898	.6732	.7565	.8398	.9232
$\frac{3}{8}$.0078	.0911	.1745	.2578	.3411	.4245	.5078	.5911	.6745	.7578	.8411	.9245
$\frac{7}{16}$.0091	.0924	.1758	.2591	.3424	.4258	.5091	.5924	.6758	.7591	.8424	.9258
$\frac{1}{2}$.0104	.0937	.1771	.2604	.3437	.4271	.5104	.5937	.6771	.7604	.8437	.9271
$\frac{9}{16}$.0117	.0951	.1784	.2617	.3451	.4284	.5117	.5951	.6784	.7617	.8451	.9284
$\frac{5}{8}$.0130	.0964	.1797	.2630	.3464	.4297	.5130	.5964	.6797	.7630	.8464	.9297
$\frac{11}{16}$.0143	.0977	.1810	.2643	.3477	.4310	.5143	.5977	.6810	.7643	.8477	.9310
$\frac{3}{4}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323
$\frac{13}{16}$.0169	.1003	.1836	.2669	.3503	.4336	.5169	.6003	.6836	.7669	.8503	.9336
$\frac{7}{8}$.0182	.1016	.1849	.2682	.3516	.4349	.5182	.6016	.6849	.7682	.8516	.9349
$\frac{15}{16}$.0195	.1029	.1862	.2695	.3529	.4362	.5195	.6029	.6862	.7695	.8529	.9362
$\frac{1}{1}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375
$\frac{17}{16}$.0221	.1055	.1888	.2721	.3555	.4388	.5221	.6055	.6888	.7721	.8555	.9388
$\frac{9}{8}$.0234	.1068	.1901	.2734	.3568	.4401	.5234	.6068	.6901	.7734	.8568	.9401
$\frac{19}{16}$.0247	.1081	.1914	.2747	.3581	.4414	.5247	.6081	.6914	.7747	.8581	.9414
$\frac{5}{4}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427
$\frac{21}{16}$.0273	.1107	.1940	.2773	.3607	.4440	.5273	.6107	.6940	.7773	.8607	.9440
$\frac{11}{8}$.0286	.1120	.1953	.2786	.3620	.4453	.5286	.6120	.6953	.7786	.8620	.9453
$\frac{23}{16}$.0299	.1133	.1966	.2799	.3633	.4466	.5299	.6133	.6966	.7799	.8633	.9466
$\frac{3}{2}$.0312	.1146	.1979	.2812	.3646	.4479	.5312	.6146	.6979	.7812	.8646	.9479
$\frac{25}{16}$.0326	.1159	.1992	.2826	.3659	.4492	.5326	.6159	.6992	.7826	.8659	.9492
$\frac{13}{8}$.0339	.1172	.2005	.2839	.3672	.4505	.5339	.6172	.7005	.7839	.8672	.9505
$\frac{27}{16}$.0352	.1185	.2018	.2852	.3685	.4518	.5352	.6185	.7018	.7852	.8685	.9518
$\frac{7}{4}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531
$\frac{29}{16}$.0378	.1211	.2044	.2878	.3711	.4544	.5378	.6211	.7044	.7878	.8711	.9544
$\frac{15}{8}$.0391	.1224	.2057	.2891	.3724	.4557	.5391	.6224	.7057	.7891	.8724	.9557
$\frac{31}{16}$.0404	.1237	.2070	.2904	.3737	.4570	.5404	.6237	.7070	.7904	.8737	.9570
$\frac{8}{4}$.0517	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583

Continued on next page.

Comparison of Inches and Fractions

With Decimals of a Foot

Continued

Inch	0"	1"	2"	3"	4"	5"	6"	7"	8"	9"	10"	11"
$\frac{1}{16}$.0430	.1263	.2096	.2930	.3763	.4596	.5430	.6263	.7096	.7930	.8763	.9596
$\frac{3}{32}$.0443	.1276	.2109	.2943	.3776	.4609	.5443	.6276	.7109	.7943	.8776	.9609
$\frac{1}{8}$.0456	.1289	.2122	.2956	.3789	.4622	.5456	.6289	.7122	.7956	.8789	.9622
$\frac{5}{16}$.0469	.1302	.2135	.2969	.3802	.4635	.5469	.6302	.7135	.7969	.8802	.9635
$\frac{3}{8}$.0482	.1315	.2148	.2982	.3815	.4648	.5482	.6315	.7148	.7982	.8815	.9648
$\frac{7}{16}$.0495	.1328	.2161	.2995	.3828	.4661	.5495	.6328	.7161	.7995	.8828	.9661
$\frac{1}{2}$.0508	.1341	.2174	.3008	.3841	.4674	.5508	.6341	.7174	.8008	.8841	.9674
$\frac{9}{16}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688
$\frac{5}{8}$.0534	.1367	.2201	.3034	.3867	.4701	.5534	.6367	.7201	.8034	.8867	.9701
$\frac{11}{16}$.0547	.1380	.2214	.3047	.3880	.4714	.5547	.6380	.7214	.8047	.8880	.9714
$\frac{3}{4}$.0560	.1393	.2227	.3060	.3893	.4727	.5560	.6393	.7227	.8060	.8893	.9727
$\frac{7}{8}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740
$\frac{15}{16}$.0586	.1419	.2253	.3086	.3919	.4753	.5586	.6419	.7253	.8086	.8919	.9753
$\frac{1}{1}$.0599	.1432	.2266	.3099	.3932	.4766	.5599	.6432	.7266	.8099	.8932	.9766
$\frac{1}{1}$.0612	.1445	.2279	.3112	.3955	.4779	.5612	.6445	.7279	.8112	.8945	.9779
$\frac{1}{1}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792
$\frac{1}{1}$.0638	.1471	.2305	.3138	.3971	.4805	.5638	.6471	.7305	.8138	.8971	.9805
$\frac{1}{1}$.0651	.1484	.2318	.3151	.3984	.4818	.5651	.6484	.7318	.8151	.8984	.9818
$\frac{1}{1}$.0664	.1497	.2331	.3164	.3997	.4831	.5664	.6497	.7331	.8164	.8997	.9831
$\frac{1}{1}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844
$\frac{1}{1}$.0690	.1523	.2357	.3190	.4023	.4857	.5690	.6523	.7357	.8190	.9023	.9857
$\frac{1}{1}$.0703	.1536	.2370	.3203	.4036	.4870	.5703	.6536	.7370	.8203	.9036	.9870
$\frac{1}{1}$.0716	.1549	.2383	.3216	.4049	.4883	.5716	.6549	.7383	.8216	.9049	.9883
$\frac{1}{1}$.0729	.1562	.2396	.3229	.4062	.4896	.5729	.6562	.7396	.8229	.9062	.9896
$\frac{1}{1}$.0742	.1576	.2409	.3242	.4076	.4909	.5742	.6576	.7409	.8242	.9076	.9909
$\frac{1}{1}$.0755	.1589	.2422	.3255	.4089	.4922	.5755	.6589	.7422	.8255	.9089	.9922
$\frac{1}{1}$.0768	.1602	.2435	.3268	.4102	.4935	.5768	.6602	.7435	.8268	.9102	.9935
$\frac{1}{1}$.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948
$\frac{1}{1}$.0794	.1628	.2461	.3294	.4128	.4961	.5794	.6628	.7461	.8294	.9128	.9961
$\frac{1}{1}$.0807	.1641	.2474	.3307	.4141	.4974	.5807	.6641	.7474	.8307	.9141	.9974
$\frac{1}{1}$.0820	.1654	.2487	.3320	.4154	.4987	.5820	.6654	.7487	.8320	.9154	.9987
1	1.0000

Comparison of Fractions With Decimals of an Inch

FRACTIONS				DECIMALS	FRACTIONS				DECIMALS
64ths	32nds	16ths	8ths		64ths	32nds	16ths	8ths	
$\frac{1}{64}$.015625	$\frac{1}{32}$.515625
	$\frac{1}{32}$.03125		$\frac{1}{16}$.53125
$\frac{1}{32}$.046875	$\frac{1}{16}$.546875
		$\frac{1}{16}$.0625			$\frac{1}{8}$.5625
$\frac{1}{16}$.078125	$\frac{1}{8}$.578125
	$\frac{1}{16}$.09375		$\frac{1}{4}$.59375
$\frac{1}{8}$.109375	$\frac{1}{4}$.609375
			$\frac{1}{8}$.125				$\frac{3}{8}$.625
$\frac{3}{64}$.140625	$\frac{3}{64}$.640625
	$\frac{1}{8}$.15625		$\frac{1}{2}$.65625
$\frac{1}{4}$.171875	$\frac{1}{2}$.671875
		$\frac{1}{8}$.1875			$\frac{1}{2}$.6875
$\frac{5}{64}$.203125	$\frac{5}{64}$.703125
	$\frac{1}{4}$.21875		$\frac{3}{4}$.71875
$\frac{3}{16}$.234375	$\frac{3}{16}$.734375
			$\frac{1}{4}$.25				$\frac{3}{4}$.75
$\frac{7}{64}$.265625	$\frac{7}{64}$.765625
	$\frac{1}{4}$.28125		$\frac{1}{2}$.78125
$\frac{1}{2}$.296875	$\frac{1}{2}$.796875
		$\frac{1}{8}$.3125			$\frac{1}{2}$.8125
$\frac{9}{64}$.328125	$\frac{9}{64}$.828125
	$\frac{3}{8}$.34375		$\frac{3}{4}$.84375
$\frac{5}{16}$.359375	$\frac{5}{16}$.859375
			$\frac{3}{8}$.375				$\frac{3}{4}$.875
$\frac{11}{64}$.390625	$\frac{11}{64}$.890625
	$\frac{1}{2}$.40625		$\frac{1}{2}$.90625
$\frac{3}{8}$.421875	$\frac{3}{8}$.921875
		$\frac{1}{8}$.4375			$\frac{1}{2}$.9375
$\frac{13}{64}$.453125	$\frac{13}{64}$.953125
	$\frac{3}{4}$.46875		$\frac{3}{4}$.96875
$\frac{7}{8}$.484375	$\frac{7}{8}$.984375
			$\frac{1}{2}$.5				1	1.00

JONES & LAUGHLIN STEEL COMPANY

Metric Conversion Table

Inches² to Centimeters² — 1 in.² = 6.451625 cm.².

TENS	UNITS									
	0	1	2	3	4	5	6	7	8	9
0	6.452	12.903	19.355	25.807	32.258	38.710	45.161	51.613	58.065
10	64.516	70.968	77.420	83.871	90.323	96.774	103.226	109.678	116.129	122.581
20	129.003	135.484	141.936	148.387	154.839	161.291	167.742	174.194	180.646	187.097
30	193.549	200.000	206.452	212.904	219.355	225.807	232.259	238.710	245.162	251.613
40	258.065	264.517	270.968	277.420	283.872	290.323	296.775	303.226	309.678	316.130
50	322.581	329.033	335.485	341.936	348.388	354.839	361.291	367.743	374.194	380.646
60	387.098	393.549	400.001	406.452	412.904	419.356	425.807	432.259	438.711	445.162
70	451.614	458.065	464.517	470.969	477.420	483.872	490.324	496.775	503.227	509.678
80	516.130	522.582	529.033	535.485	541.937	548.388	554.840	561.291	567.743	574.195
90	580.646	587.098	593.550	600.001	606.453	612.904	619.356	625.808	632.259	638.711

Centimeters² to Inches² — 1 cm.² = 0.15499969 in.².

TENS	UNITS									
	0	1	2	3	4	5	6	7	8	9
0	0.1550	0.3100	0.4650	0.6200	0.7750	0.9300	1.0850	1.2400	1.3950
10	1.5500	1.7050	1.8600	2.0150	2.1700	2.3250	2.4800	2.6350	2.7900	2.9450
20	3.1000	3.2550	3.4100	3.5650	3.7200	3.8750	4.0300	4.1850	4.3400	4.4950
30	4.6500	4.8050	4.9600	5.1150	5.2700	5.4250	5.5800	5.7350	5.8900	6.0450
40	6.2000	6.3550	6.5100	6.6650	6.8200	6.9750	7.1300	7.2850	7.4400	7.5950
50	7.7500	7.9050	8.0600	8.2150	8.3700	8.5250	8.6800	8.8350	8.9900	9.1450
60	9.3000	9.4550	9.6100	9.7650	9.9200	10.0750	10.2300	10.3850	10.5400	10.6950
70	10.8500	11.0050	11.1600	11.3150	11.4700	11.6250	11.7800	11.9350	12.0900	12.2450
80	12.4000	12.5550	12.7100	12.8650	13.0200	13.1750	13.3300	13.4850	13.6400	13.7950
90	13.9500	14.1050	14.2600	14.4150	14.5700	14.7250	14.8800	15.0350	15.1900	15.3450

Inches³ to Centimeters³ — 1 in.³ = 16.38716 cm.³.

TENS	UNITS									
	0	1	2	3	4	5	6	7	8	9
0	16.39	32.77	49.16	65.55	81.94	98.32	114.71	131.10	147.48
10	163.87	180.26	196.65	213.03	229.42	245.81	262.19	278.58	294.97	311.36
20	327.74	344.13	360.52	376.90	393.29	409.68	426.07	442.45	458.84	475.23
30	491.61	508.00	524.39	540.78	557.16	573.55	589.94	606.32	622.71	639.10
40	655.49	671.87	688.26	704.65	721.04	737.42	753.81	770.20	786.58	802.97
50	819.36	835.75	852.13	868.52	884.91	901.29	917.68	934.07	950.46	966.84
60	983.23	999.62	1016.00	1032.39	1048.78	1065.17	1081.55	1097.94	1114.33	1130.71
70	1147.10	1163.49	1179.88	1196.26	1212.65	1229.04	1245.42	1261.81	1278.20	1294.59
80	1310.97	1327.36	1343.75	1360.13	1376.52	1392.91	1409.30	1425.68	1442.07	1458.46
90	1474.84	1491.23	1507.62	1524.01	1540.39	1556.78	1573.17	1589.55	1605.94	1622.33

Centimeters³ to Inches³ — 1 cm.³ = 0.0610234 in.³.

TENS	UNITS									
	0	1	2	3	4	5	6	7	8	9
0	0.06102	0.12205	0.18307	0.24409	0.30512	0.36614	0.42716	0.48819	0.54921
10	0.61023	0.67126	0.73228	0.79330	0.85433	0.91535	0.97637	1.03740	1.09842	1.15944
20	1.22047	1.28149	1.34251	1.40354	1.46456	1.52559	1.58661	1.64763	1.70866	1.76968
30	1.83070	1.89173	1.95275	2.01377	2.07480	2.13582	2.19684	2.25787	2.31889	2.37991
40	2.44094	2.50196	2.56298	2.62401	2.68503	2.74605	2.80708	2.86810	2.92912	2.99015
50	3.05117	3.11219	3.17322	3.23424	3.29526	3.35629	3.41731	3.47833	3.53936	3.60038
60	3.66140	3.72243	3.78345	3.84447	3.90550	3.96652	4.02754	4.08857	4.14959	4.21061
70	4.27164	4.33266	4.39368	4.45471	4.51573	4.57675	4.63778	4.69880	4.75983	4.82085
80	4.88187	4.94290	5.00392	5.06494	5.12597	5.18699	5.24801	5.30904	5.37006	5.43108
90	5.49211	5.55313	5.61415	5.67518	5.73620	5.79722	5.85825	5.91927	5.98029	6.04131

Metric Conversion Table

Continued

Pounds per Sq. Inch to Kg. per Sq. Cm.—1 lb./in.² = 0.0703067 kg/cm².

TENS	UNITS									
	0	1	2	3	4	5	6	7	8	9
0	0.07031	0.14061	0.21092	0.28123	0.35153	0.42184	0.49215	0.56245	0.63276
10	0.70307	0.77337	0.84368	0.91399	0.98429	1.05460	1.12491	1.19521	1.26552	1.33583
20	1.40613	1.47644	1.54675	1.61705	1.68736	1.75767	1.82797	1.89828	1.96859	2.03889
30	2.10920	2.17951	2.24981	2.32012	2.39043	2.46073	2.53104	2.60135	2.67165	2.74196
40	2.81227	2.88257	2.95288	3.02319	3.09349	3.16380	3.23411	3.30441	3.37472	3.44503
50	3.51534	3.58564	3.65595	3.72626	3.79656	3.86687	3.93718	4.00748	4.07779	4.14810
60	4.21840	4.28871	4.35902	4.42932	4.49963	4.56994	4.64024	4.71055	4.78086	4.85116
70	4.92147	4.99178	5.06208	5.13239	5.20270	5.27300	5.34331	5.41362	5.48392	5.55423
80	5.62454	5.69484	5.76515	5.83546	5.90576	5.97607	6.04638	6.11668	6.18699	6.25730
90	6.32760	6.39791	6.46822	6.53852	6.60883	6.67914	6.74944	6.81975	6.89006	6.96036

Kg. per Sq. Cm. to Pounds per Sq. Inch—1 kg/cm² = 14.2234 lbs./in.².

TENS	UNITS									
	0	1	2	3	4	5	6	7	8	9
0	14.22	28.45	42.67	56.89	71.12	85.34	99.56	113.79	128.01
10	142.23	156.46	170.68	184.90	199.13	213.35	227.57	241.80	256.02	270.24
20	284.47	298.69	312.91	327.14	341.36	355.59	369.81	384.03	398.26	412.48
30	426.70	440.93	455.15	469.37	483.60	497.82	512.04	526.27	540.49	554.71
40	568.94	583.16	597.38	611.61	625.83	640.05	654.28	668.50	682.72	696.95
50	711.17	725.39	739.62	753.84	768.06	782.29	796.51	810.73	824.96	839.18
60	853.40	867.63	881.85	896.07	910.30	924.52	938.74	952.97	967.19	981.41
70	995.64	1009.86	1024.08	1038.31	1052.53	1066.76	1080.98	1095.20	1109.43	1123.65
80	1137.87	1152.10	1166.32	1180.54	1194.77	1208.99	1223.21	1237.44	1251.66	1265.88
90	1280.11	1294.33	1308.55	1322.78	1337.00	1351.22	1365.45	1379.67	1393.89	1408.12

Kilograms per Meter to Pounds per Foot—1 kg/m = 0.67197 lb./ft.

TENS	UNITS									
	0	1	2	3	4	5	6	7	8	9
0	0.6720	1.3439	2.0159	2.6879	3.3599	4.0318	4.7038	5.3758	6.0477
10	6.7197	7.3917	8.0636	8.7356	9.4076	10.0796	10.7515	11.4235	12.0955	12.7674
20	13.4394	14.1114	14.7833	15.4553	16.1273	16.7993	17.4712	18.1432	18.8152	19.4871
30	20.1591	20.8311	21.5030	22.1750	22.8470	23.5190	24.1909	24.8629	25.5349	26.2068
40	26.8788	27.5508	28.2227	28.8947	29.5667	30.2387	30.9106	31.5826	32.2546	32.9265
50	33.5985	34.2705	34.9424	35.6144	36.2864	36.9584	37.6303	38.3022	38.9743	39.6462
60	40.3182	40.9902	41.6621	42.3341	43.0061	43.6781	44.3500	45.0220	45.6940	46.3659
70	47.0379	47.7099	48.3818	49.0538	49.7258	50.3978	51.0697	51.7417	52.4137	53.0856
80	53.7576	54.4296	55.1015	55.7735	56.4455	57.1175	57.7894	58.4614	59.1334	59.8053
90	60.4773	61.1493	61.8212	62.4932	63.1652	63.8372	64.5091	65.1811	65.8531	66.5250

Pounds per Foot to Kilograms per Meter—1 lb./ft. = 1.48816 kg/m.

TENS	UNITS									
	0	1	2	3	4	5	6	7	8	9
0	1.488	2.976	4.464	5.953	7.441	8.929	10.417	11.905	13.393
10	14.882	16.370	17.858	19.346	20.834	22.322	23.811	25.299	26.787	28.275
20	29.763	31.251	32.740	34.228	35.716	37.204	38.692	40.180	41.669	43.157
30	44.645	46.133	47.621	49.109	50.597	52.086	53.574	55.062	56.550	58.038
40	59.526	61.015	62.503	63.991	65.479	66.967	68.455	69.944	71.432	72.920
50	74.408	75.896	77.384	78.873	80.361	81.849	83.337	84.825	86.313	87.802
60	89.290	90.778	92.266	93.754	95.242	96.730	98.219	99.707	101.195	102.683
70	104.171	105.659	107.148	108.636	110.124	111.612	113.100	114.588	116.077	117.565
80	119.053	120.541	122.029	123.517	125.006	126.494	127.982	129.470	130.958	132.446
90	133.934	135.423	136.911	138.399	139.887	141.375	142.863	144.352	145.840	147.328

JONES & LAUGHLIN STEEL COMPANY

Metric Conversion Table

Continued

Inches to Centimeters — 1 in. = 2.540005 cm.

TENS	UNITS									
	0	1	2	3	4	5	6	7	8	9
0	2.540	5.080	7.620	10.160	12.700	15.240	17.780	20.320	22.860
10	25.400	27.940	30.480	33.020	35.560	38.100	40.640	43.180	45.720	48.260
20	50.800	53.340	55.880	58.420	60.960	63.500	66.040	68.580	71.120	73.660
30	76.200	78.740	81.280	83.820	86.360	88.900	91.440	93.980	96.520	99.060
40	101.600	104.140	106.680	109.220	111.760	114.300	116.840	119.380	121.920	124.460
50	127.000	129.540	132.080	134.620	137.160	139.700	142.240	144.780	147.320	149.860
60	152.400	154.940	157.480	160.020	162.560	165.100	167.640	170.180	172.720	175.260
70	177.800	180.340	182.880	185.420	187.960	190.500	193.040	195.580	198.120	200.660
80	203.200	205.740	208.280	210.820	213.360	215.900	218.440	220.980	223.520	226.060
90	228.600	231.140	233.680	236.220	238.760	241.300	243.840	246.380	248.920	251.460

Centimeters to Inches — 1 cm = 0.3937 in.

TENS	UNITS									
	0	1	2	3	4	5	6	7	8	9
0	0.3937	0.7874	1.1811	1.5748	1.9685	2.3622	2.7559	3.1496	3.5433
10	3.9370	4.3307	4.7244	5.1181	5.5118	5.9055	6.2992	6.6929	7.0866	7.4803
20	7.8740	8.2677	8.6614	9.0551	9.4488	9.8425	10.2362	10.6299	11.0236	11.4173
30	11.8110	12.2047	12.5984	12.9921	13.3858	13.7795	14.1732	14.5669	14.9606	15.3543
40	15.7480	16.1417	16.5354	16.9291	17.3228	17.7165	18.1102	18.5039	18.8976	19.2913
50	19.6850	20.0787	20.4724	20.8661	21.2598	21.6535	22.0472	22.4409	22.8346	23.2283
60	23.6220	24.0157	24.4094	24.8031	25.1968	25.5905	25.9842	26.3779	26.7716	27.1653
70	27.5590	27.9527	28.3464	28.7401	29.1338	29.5275	29.9212	30.3149	30.7086	31.1023
80	31.4960	31.8897	32.2834	32.6771	33.0708	33.4645	33.8582	34.2519	34.6456	35.0393
90	35.4330	35.8267	36.2204	36.6141	37.0078	37.4015	37.7952	38.1889	38.5826	38.9763

Feet to Meters — 1 ft. = 0.3048006 m.

TENS	UNITS									
	0	1	2	3	4	5	6	7	8	9
0	0.3048	0.6096	0.9144	1.2192	1.5240	1.8288	2.1336	2.4384	2.7432
10	3.0480	3.3528	3.6576	3.9624	4.2672	4.5720	4.8768	5.1816	5.4864	5.7912
20	6.0960	6.4008	6.7056	7.0104	7.3152	7.6200	7.9248	8.2296	8.5344	8.8392
30	9.1440	9.4488	9.7536	10.0584	10.3632	10.6680	10.9728	11.2776	11.5824	11.8872
40	12.1920	12.4968	12.8016	13.1064	13.4112	13.7160	14.0208	14.3256	14.6304	14.9352
50	15.2400	15.5448	15.8496	16.1544	16.4592	16.7640	17.0688	17.3736	17.6784	17.9832
60	18.2880	18.5928	18.8976	19.2024	19.5072	19.8120	20.1168	20.4216	20.7264	21.0312
70	21.3360	21.6408	21.9456	22.2504	22.5552	22.8600	23.1648	23.4696	23.7744	24.0792
80	24.3840	24.6888	24.9936	25.2984	25.6032	25.9080	26.2128	26.5176	26.8224	27.1272
90	27.4320	27.7368	28.0416	28.3464	28.6512	28.9560	29.2608	29.5656	29.8704	30.1752

Meters to Feet — 1 m = 3.2808333 ft.

TENS	UNITS									
	0	1	2	3	4	5	6	7	8	9
0	3.281	6.562	9.843	13.123	16.404	19.685	22.966	26.247	29.528
10	32.808	36.089	39.370	42.651	45.932	49.213	52.494	55.775	59.056	62.337
20	65.617	68.898	72.179	75.459	78.740	82.021	85.302	88.583	91.864	95.144
30	98.425	101.706	104.987	108.268	111.548	114.829	118.110	121.391	124.672	127.953
40	131.233	134.514	137.795	141.076	144.357	147.638	150.919	154.199	157.480	160.761
50	164.042	167.323	170.603	173.884	177.165	180.446	183.727	187.008	190.289	193.569
60	196.850	200.131	203.412	206.693	209.973	213.254	216.535	219.816	223.097	226.378
70	229.658	232.939	236.220	239.501	242.782	246.063	249.343	252.624	255.905	259.186
80	262.467	265.748	269.028	272.309	275.590	278.871	282.152	285.433	288.713	291.994
90	295.275	298.556	301.837	305.118	308.398	311.679	314.960	318.241	321.522	324.803

Metric Conversion Table

Continued

Inches to Millimeters

39.37 inches, U. S. Standard = 1 meter = 100 centimeters = 1000 millimeters.

Inches	0	$\frac{1}{16}$	$\frac{1}{8}$	$\frac{3}{16}$	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$
0	0.00	1.59	3.18	4.76	6.35	7.94	9.53	11.11
1	25.40	26.99	28.58	30.16	31.75	33.34	34.93	36.51
2	50.80	52.39	53.98	55.56	57.15	58.74	60.33	61.91
3	76.20	77.79	79.38	80.96	82.55	84.14	85.73	87.31
4	101.60	103.19	104.78	106.36	107.95	109.54	111.13	112.71
5	127.00	128.59	130.18	131.76	133.35	134.94	136.53	138.11
6	152.40	153.99	155.58	157.16	158.75	160.34	161.93	163.51
7	177.80	179.39	180.98	182.56	184.15	185.74	187.33	188.91
8	203.20	204.79	206.38	207.96	209.55	211.14	212.73	214.31
9	228.60	230.19	231.78	233.36	234.95	236.54	238.13	239.71
10	254.00	255.59	257.18	258.76	260.35	261.94	263.53	265.11
11	279.40	280.99	282.58	284.16	285.75	287.34	288.93	290.51
12	304.80	306.39	307.98	309.56	311.15	312.74	314.33	315.91
13	330.20	331.79	333.38	334.96	336.55	338.14	339.73	341.31
14	355.60	357.19	358.78	360.36	361.95	363.54	365.13	366.71
15	381.00	382.59	384.18	385.76	387.35	388.94	390.53	392.11
16	406.40	407.99	409.58	411.16	412.75	414.34	415.93	417.51
17	431.80	433.39	434.98	436.56	438.15	439.74	441.33	442.91
18	457.20	458.79	460.38	461.96	463.55	465.14	466.73	468.31
19	482.60	484.19	485.78	487.36	488.95	490.54	492.13	493.71
20	508.00	509.59	511.18	512.76	514.35	515.94	517.53	519.11
21	533.40	534.99	536.58	538.16	539.75	541.34	542.93	544.51
22	558.80	560.39	561.98	563.56	565.15	566.74	568.33	569.91
23	584.20	585.79	587.38	588.96	590.55	592.14	593.73	595.31
24	609.60	611.19	612.78	614.36	615.95	617.54	619.13	620.71
25	635.00	636.59	638.18	639.76	641.35	642.94	644.53	646.11
26	660.40	661.99	663.58	665.16	666.75	668.34	669.93	671.51
27	685.80	687.39	688.98	690.56	692.15	693.74	695.33	696.91
28	711.20	712.79	714.38	715.96	717.55	719.14	720.73	722.31
29	736.60	738.19	739.78	741.36	742.95	744.54	746.13	747.71
30	762.00	763.59	765.18	766.76	768.35	769.94	771.53	773.11
31	787.40	788.99	790.58	792.16	793.75	795.34	796.93	798.51
32	812.80	814.39	815.98	817.56	819.15	820.74	822.33	823.91
33	838.20	839.79	841.38	842.96	844.55	846.14	847.73	849.31
34	863.60	865.19	866.78	868.36	869.95	871.54	873.13	874.71
35	889.00	890.59	892.18	893.76	895.35	896.94	898.53	900.11
36	914.40	915.99	917.58	919.16	920.75	922.34	923.93	925.51
37	939.80	941.39	942.98	944.56	946.15	947.74	949.33	950.91
38	965.20	966.79	968.38	969.96	971.55	973.14	974.73	976.31
39	990.60	992.19	993.78	995.36	996.95	998.54	1000.13	1001.71
40	1016.00	1017.59	1019.18	1020.76	1022.35	1023.94	1025.53	1027.11
41	1041.40	1042.99	1044.58	1046.16	1047.75	1049.34	1050.93	1052.51
42	1066.80	1068.39	1069.98	1071.56	1073.15	1074.74	1076.33	1077.91
43	1092.20	1093.79	1095.38	1096.96	1098.55	1100.14	1101.73	1103.31
44	1117.60	1119.19	1120.78	1122.36	1123.95	1125.54	1127.13	1128.71
45	1143.00	1144.59	1146.18	1147.76	1149.35	1150.94	1152.53	1154.11
46	1168.40	1169.99	1171.58	1173.16	1174.75	1176.34	1177.93	1179.51
47	1193.80	1195.39	1196.98	1198.56	1200.15	1201.74	1203.33	1204.91
48	1219.20	1220.79	1222.38	1223.96	1225.55	1227.14	1228.73	1230.31
49	1244.60	1246.19	1247.78	1249.36	1250.95	1252.54	1254.13	1255.71
50	1270.00	1271.59	1273.18	1274.76	1276.35	1277.94	1279.53	1281.11

Continued on next page.

Metric Conversion Table

Continued

Inches to Millimeters

39.37 inches, U. S. Standard = 1 meter = 100 centimeters = 1000 millimeters.

Inches	$\frac{1}{2}$	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{3}{4}$
0	12.70	14.29	15.88	17.46	19.05	20.64	22.23	23.81
1	35.10	39.69	41.28	42.86	44.45	46.04	47.63	49.21
2	63.50	65.09	66.68	68.26	69.85	71.44	73.03	74.61
3	88.90	90.49	92.08	93.66	95.25	96.84	98.43	100.01
4	114.30	115.89	117.48	119.06	120.65	122.24	123.83	125.41
5	139.70	141.29	142.88	144.46	146.05	147.64	149.23	150.81
6	165.10	166.69	168.28	169.86	171.45	173.04	174.63	176.21
7	190.50	192.09	193.68	195.26	196.85	198.44	200.03	201.61
8	215.90	217.49	219.08	220.66	222.25	223.84	225.43	227.01
9	241.30	242.89	244.48	246.06	247.65	249.24	250.83	252.41
10	266.70	268.29	269.88	271.46	273.05	274.64	276.23	277.81
11	292.10	293.69	295.28	296.86	298.45	300.04	301.63	303.21
12	317.50	319.09	320.68	322.26	323.85	325.44	327.03	328.61
13	342.90	344.49	346.08	347.66	349.25	350.84	352.43	354.01
14	368.30	369.89	371.48	373.06	374.65	376.24	377.83	379.41
15	393.70	395.29	396.88	398.46	400.05	401.64	403.23	404.81
16	419.10	420.69	422.28	423.86	425.45	427.04	428.63	430.21
17	444.50	446.09	447.68	449.26	450.85	452.44	454.03	455.61
18	469.90	471.49	473.08	474.66	476.25	477.84	479.43	481.01
19	495.30	496.89	498.48	500.06	501.65	503.24	504.83	506.41
20	520.70	522.29	523.88	525.46	527.05	528.64	530.23	531.81
21	546.10	547.69	549.28	550.86	552.45	554.04	555.63	557.21
22	571.50	573.09	574.68	576.26	577.85	579.44	581.03	582.61
23	596.90	598.49	600.08	601.66	603.25	604.84	606.43	608.01
24	622.30	623.89	625.48	627.06	628.65	630.24	631.83	633.41
25	647.70	649.29	650.88	652.46	654.05	655.64	657.23	658.81
26	673.10	674.69	676.28	677.86	679.45	681.04	682.63	684.21
27	698.50	700.09	701.68	703.26	704.85	706.44	708.03	709.61
28	723.90	725.49	727.08	728.66	730.25	731.84	733.43	735.01
29	749.30	750.89	752.48	754.06	755.65	757.24	758.83	760.41
30	774.70	776.29	777.88	779.46	781.05	782.64	784.23	785.81
31	800.10	801.69	803.28	804.86	806.45	808.04	809.63	811.21
32	825.50	827.09	828.68	830.26	831.85	833.44	835.03	836.61
33	850.90	852.49	854.08	855.66	857.25	858.84	860.43	862.01
34	876.30	877.89	879.48	881.06	882.65	884.24	885.83	887.41
35	901.70	903.29	904.88	906.46	908.05	909.64	911.23	912.81
36	927.10	928.69	930.28	931.86	933.45	935.04	936.63	938.21
37	952.50	954.09	955.68	957.26	958.85	960.44	962.03	963.61
38	977.90	979.49	981.08	982.66	984.25	985.84	987.43	989.01
39	1003.30	1004.89	1006.48	1008.06	1009.65	1011.24	1012.83	1014.41
40	1028.70	1030.29	1031.88	1033.46	1035.05	1036.64	1038.23	1039.81
41	1054.10	1055.69	1057.28	1058.86	1060.45	1062.04	1063.63	1065.21
42	1079.50	1081.09	1082.68	1084.26	1085.85	1087.44	1089.03	1090.61
43	1104.90	1106.49	1108.08	1109.66	1111.25	1112.84	1114.43	1116.01
44	1130.30	1131.89	1133.48	1135.06	1136.65	1138.24	1139.83	1141.41
45	1155.70	1157.29	1158.88	1160.46	1162.05	1163.64	1165.23	1166.81
46	1181.10	1182.69	1184.28	1185.86	1187.45	1189.04	1190.63	1192.21
47	1206.50	1208.09	1209.68	1211.26	1212.85	1214.44	1216.03	1217.61
48	1231.90	1233.49	1235.08	1236.66	1238.25	1239.84	1241.43	1243.01
49	1257.30	1258.89	1260.48	1262.06	1263.65	1265.24	1266.83	1268.41
50	1282.70	1284.29	1285.88	1287.46	1289.05	1290.64	1292.23	1293.81

Metric Conversion Table

Continued

Pounds Avoirdupois to Kilograms

1 Pound = 0.45359 Kilograms

Lbs.	0	1	2	3	4	5	6	7	8	9
0	0.45	0.91	1.36	1.81	2.27	2.72	3.18	3.63	4.08
1	4.54	4.99	5.44	5.90	6.35	6.80	7.26	7.71	8.16	8.62
2	9.07	9.53	9.98	10.43	10.89	11.34	11.79	12.25	12.70	13.15
3	13.61	14.06	14.51	14.97	15.42	15.88	16.33	16.78	17.24	17.69
4	18.14	18.60	19.05	19.50	19.96	20.41	20.87	21.32	21.77	22.23
5	22.68	23.13	23.59	24.04	24.49	24.95	25.40	25.85	26.31	26.76
6	27.22	27.67	28.12	28.58	29.03	29.48	29.94	30.39	30.84	31.30
7	31.75	32.21	32.66	33.11	33.57	34.02	34.47	34.93	35.38	35.83
8	36.29	36.74	37.19	37.65	38.10	38.56	39.01	39.46	39.92	40.37
9	40.82	41.28	41.73	42.18	42.64	43.09	43.54	44.00	44.45	44.91
10	45.36	45.81	46.27	46.72	47.17	47.63	48.08	48.53	48.99	49.44
11	49.90	50.35	50.80	51.26	51.71	52.16	52.62	53.07	53.52	53.98
12	54.43	54.88	55.34	55.79	56.25	56.70	57.15	57.61	58.06	58.51
13	58.97	59.42	59.87	60.33	60.78	61.23	61.69	62.14	62.60	63.05
14	63.50	63.96	64.41	64.86	65.32	65.77	66.22	66.68	67.13	67.59
15	68.04	68.49	68.95	69.40	69.85	70.31	70.76	71.21	71.67	72.12
16	72.57	73.03	73.48	73.94	74.39	74.84	75.30	75.75	76.20	76.66
17	77.11	77.56	78.02	78.47	78.93	79.38	79.83	80.29	80.74	81.19
18	81.65	82.10	82.55	83.01	83.46	83.91	84.37	84.82	85.28	85.73
19	86.18	86.64	87.09	87.54	88.00	88.45	88.90	89.36	89.81	90.26
20	90.72	91.17	91.63	92.08	92.53	92.99	93.44	93.89	94.35	94.80
21	95.25	95.71	96.16	96.62	97.07	97.52	97.98	98.43	98.88	99.34
22	99.79	100.24	100.70	101.15	101.60	102.06	102.51	102.97	103.42	103.87
23	104.33	104.78	105.23	105.69	106.14	106.59	107.05	107.50	107.96	108.41
24	108.86	109.32	109.77	110.22	110.68	111.13	111.58	112.04	112.49	112.94
25	113.40	113.85	114.31	114.76	115.21	115.67	116.12	116.57	117.03	117.48
26	117.93	118.39	118.84	119.29	119.75	120.20	120.66	121.11	121.56	122.02
27	122.47	122.92	123.38	123.83	124.28	124.74	125.19	125.65	126.10	126.55
28	127.01	127.46	127.91	128.37	128.82	129.27	129.73	130.18	130.63	131.09
29	131.54	132.00	132.45	132.90	133.36	133.81	134.26	134.72	135.17	135.62
30	136.08	136.53	136.98	137.44	137.89	138.35	138.80	139.25	139.71	140.16
31	140.61	141.07	141.52	141.97	142.43	142.88	143.34	143.79	144.24	144.70
32	145.15	145.60	146.06	146.51	146.96	147.42	147.87	148.32	148.78	149.23
33	149.69	150.14	150.59	151.05	151.50	151.95	152.41	152.86	153.31	153.77
34	154.22	154.68	155.13	155.58	156.04	156.49	156.94	157.40	157.85	158.30
35	158.76	159.21	159.66	160.12	160.57	161.03	161.48	161.93	162.39	162.84
36	163.29	163.75	164.20	164.65	165.11	165.56	166.01	166.47	166.92	167.38
37	167.83	168.28	168.74	169.19	169.64	170.10	170.55	171.00	171.46	171.91
38	172.37	172.82	173.27	173.73	174.18	174.63	175.09	175.54	175.99	176.45
39	176.90	177.35	177.81	178.26	178.72	179.17	179.62	180.08	180.53	180.98
40	181.44	181.89	182.34	182.80	183.25	183.70	184.16	184.61	185.07	185.52
41	185.97	186.43	186.88	187.33	187.79	188.24	188.69	189.15	189.60	190.06
42	190.51	190.96	191.42	191.87	192.32	192.78	193.23	193.68	194.14	194.59
43	195.04	195.50	195.95	196.41	196.86	197.31	197.77	198.22	198.67	199.13
44	199.58	200.03	200.49	200.94	201.40	201.85	202.30	202.76	203.21	203.66
45	204.12	204.57	205.02	205.48	205.93	206.38	206.84	207.29	207.75	208.20
46	208.65	209.11	209.56	210.01	210.47	210.92	211.37	211.83	212.28	212.73
47	213.19	213.64	214.10	214.55	215.00	215.46	215.91	216.36	216.82	217.27
48	217.72	218.18	218.63	219.09	219.54	219.99	220.45	220.90	221.35	221.81
49	222.26	222.71	223.17	223.62	224.07	224.53	224.98	225.44	225.89	226.34

Continued on next page.

Metric Conversion Table

Continued

Pounds Avoirdupois to Kilograms

1 Pound = 0.45359 Kilograms

Lbs.	0	1	2	3	4	5	6	7	8	9
50	226.80	227.25	227.70	228.16	228.61	229.06	229.52	229.97	230.42	230.88
51	231.33	231.79	232.24	232.69	233.15	233.60	234.05	234.51	234.96	235.41
52	235.87	236.32	236.78	237.23	237.68	238.14	238.59	239.04	239.50	239.95
53	240.40	240.86	241.31	241.76	242.22	242.67	243.13	243.58	244.03	244.49
54	244.94	245.39	245.85	246.30	246.75	247.21	247.66	248.12	248.57	249.02
55	249.48	249.93	250.38	250.84	251.29	251.74	252.20	252.65	253.10	253.56
56	254.01	254.47	254.92	255.37	255.83	256.28	256.73	257.19	257.64	258.09
57	258.55	259.00	259.45	259.91	260.36	260.82	261.27	261.72	262.18	262.63
58	263.08	263.54	263.99	264.44	264.90	265.35	265.81	266.26	266.71	267.17
59	267.62	268.07	268.53	268.98	269.43	269.89	270.34	270.79	271.25	271.70
60	272.16	272.61	273.06	273.52	273.97	274.42	274.88	275.33	275.78	276.24
61	276.69	277.14	277.60	278.05	278.51	278.96	279.41	279.87	280.32	280.77
62	281.23	281.68	282.13	282.59	283.04	283.50	283.95	284.40	284.86	285.31
63	285.76	286.22	286.67	287.12	287.58	288.03	288.48	288.94	289.39	289.85
64	290.30	290.75	291.21	291.66	292.11	292.57	293.02	293.47	293.93	294.38
65	294.84	295.29	295.74	296.20	296.65	297.10	297.56	298.01	298.46	298.92
66	299.37	299.82	300.28	300.73	301.19	301.64	302.09	302.55	303.00	303.45
67	303.91	304.36	304.81	305.27	305.72	306.17	306.63	307.08	307.54	307.99
68	308.44	308.90	309.35	309.80	310.26	310.71	311.16	311.62	312.07	312.53
69	312.98	313.43	313.89	314.34	314.79	315.25	315.70	316.15	316.61	317.06
70	317.51	317.97	318.42	318.88	319.33	319.78	320.24	320.69	321.14	321.60
71	322.05	322.50	322.96	323.41	323.86	324.32	324.77	325.23	325.68	326.13
72	326.59	327.04	327.49	327.95	328.40	328.85	329.31	329.76	330.22	330.67
73	331.12	331.58	332.03	332.48	332.94	333.39	333.84	334.30	334.75	335.20
74	335.66	336.11	336.57	337.02	337.47	337.93	338.38	338.83	339.29	339.74
75	340.19	340.65	341.10	341.56	342.01	342.46	342.92	343.37	343.82	344.28
76	344.73	345.18	345.64	346.09	346.54	347.00	347.45	347.91	348.36	348.81
77	349.27	349.72	350.17	350.63	351.08	351.53	351.99	352.44	352.89	353.35
78	353.80	354.26	354.71	355.16	355.62	356.07	356.52	356.98	357.43	357.88
79	358.34	358.79	359.25	359.70	360.15	360.61	361.06	361.51	361.97	362.42
80	362.87	363.33	363.78	364.23	364.69	365.14	365.60	366.05	366.50	366.96
81	367.41	367.86	368.32	368.77	369.22	369.68	370.13	370.59	371.04	371.49
82	371.95	372.40	372.85	373.31	373.76	374.21	374.67	375.12	375.57	376.03
83	376.48	376.94	377.39	377.84	378.30	378.75	379.20	379.66	380.11	380.56
84	381.02	381.47	381.92	382.38	382.83	383.29	383.74	384.19	384.65	385.10
85	385.55	386.01	386.46	386.91	387.37	387.82	388.28	388.73	389.18	389.64
86	390.09	390.54	391.00	391.45	391.90	392.36	392.81	393.26	393.72	394.17
87	394.63	395.08	395.53	395.99	396.44	396.89	397.35	397.80	398.25	398.71
88	399.16	399.61	400.07	400.52	400.98	401.43	401.88	402.34	402.79	403.24
89	403.78	404.15	404.60	405.06	405.51	405.97	406.42	406.87	407.33	407.78
90	408.23	408.69	409.14	409.59	410.05	410.50	410.95	411.41	411.86	412.32
91	412.77	413.22	413.68	414.13	414.58	415.14	415.49	415.94	416.40	416.85
92	417.31	417.76	418.21	418.67	419.12	419.57	420.03	420.48	420.93	421.39
93	421.84	422.29	422.75	423.20	423.66	424.11	424.56	425.02	425.47	425.92
94	426.38	426.83	427.28	427.74	428.19	428.64	429.10	429.55	430.01	430.46
95	430.91	431.37	431.82	432.27	432.73	433.18	433.63	434.09	434.54	435.00
96	435.45	435.90	436.36	436.81	437.26	437.72	438.17	438.62	439.08	
97	439.98	440.44	440.89	441.35	441.80	442.25	442.71	443.16	443.61	
98	444.52	444.97	445.43	445.88	446.33	446.79	447.24	447.70	448.15	
99	449.06	449.51	449.96	450.42	450.87	451.32	451.78	452.23	452.68	

Properties of the Circle

Circumference of Circle of Diameter 1 = $\pi = 3.14159265$

Circumference of Circle = $2 \pi r$

Diameter of Circle = Circumference $\times 0.31831$

Diameter of Circle of equal periphery as square

= side $\times 1.27324$

Side of Square of equal periphery as circle = diameter $\times 0.78540$

Diameter of Circle circumscribed about square = side $\times 1.41421$

Side of Square inscribed in circle = diameter $\times 0.70711$

Arc, $a = \frac{\pi r A^\circ}{180} = 0.017453 r A^\circ$

Angle, $A = \frac{180^\circ a}{\pi r} = 57.29578 \frac{a}{r}$

Radius, $r = \frac{4 b^2 + c^2}{8 b}$ Diameter, $d = \frac{4 b^2 + c^2}{4 b}$

Chord, $c = 2 \sqrt{2 b r - b^2} = 2 r \sin \frac{A^\circ}{2}$

Rise, $b = r - \frac{1}{2} \sqrt{4 r^2 - c^2} = \frac{c}{2} \tan \frac{A^\circ}{4} = 2 r \sin^2 \frac{A}{4}$

Rise, $b = r + y - \sqrt{r^2 - x^2}$ $y = b - r + \sqrt{r^2 - x^2}$

$x = \sqrt{r^2 - (r + y - b)^2}$

$\pi = 3.14159265$, $\log = 0.4971499$

$\frac{1}{\pi} = 0.3183099$, $\log = \overline{1.5028501}$

$\pi^2 = 9.8696044$, $\log = 0.9942997$

$\frac{1}{\pi^2} = 0.1013212$, $\log = \overline{1.0057003}$

$\sqrt{\pi} = 1.7724539$, $\log = 0.2485749$

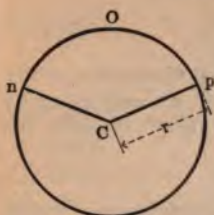
$\sqrt{\frac{1}{\pi}} = 0.5641896$, $\log = \overline{1.7514251}$

$\frac{\pi}{180} = 0.0174533$, $\log = \overline{2.2418774}$

$\frac{180}{\pi} = 57.2957795$, $\log = 1.7581226$

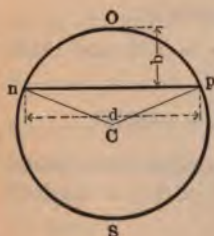


Areas of Circular Sections



Circular Sector, $n c p o$

$$\begin{aligned}\text{Area} &= \frac{1}{2} (\text{length of arc, } n o p \times \text{radius } r) \\ &= \text{Area of circle} \times \frac{\text{Arc, } n o p, \text{ in degrees}}{360} \\ &= 0.0087266 \times \text{square of radius, } r^2 \times \\ &\quad \text{angle of arc, } n o p, \text{ in degrees.}\end{aligned}$$



Circular Segment, $n o p$, less than half circle.

$$\begin{aligned}\text{Area} &= \text{Area of sector, } n c p o, - \text{area of} \\ &\quad \text{triangle, } n c p \\ &= \frac{(\text{length of arc, } n o p, \times \text{radius, } r) -}{2} \\ &\quad \frac{(\text{radius, } r, - \text{rise, } b) \times \text{chord, } d}{2}\end{aligned}$$

Circular Segment, $n s p$, greater than half circle.

$$\text{Area} = \text{Area of circle} - \text{area of segment, } n p o$$

Circular Segment

Given: Rise, c , and chord, d

Area = Product of rise and chord, $c \times d$, multiplied by the coefficient given opposite the quotient of $\frac{c}{d}$:



Intermediate coefficients for values of $\frac{c}{d}$ not given in tables are obtained by interpolation.

Example—Given: Rise = 3.00 and chord = 10.39

$$\frac{c}{d} = \frac{3.00}{10.39} = 0.2887. \text{ Coefficient} = 0.7092$$

$$\text{Area} = c \times d \times \text{coeff.} = 3.00 \times 10.39 \times 0.7092 = 22.10576$$

Areas of Circular Sections

Continued

Circular Segment

Given: Rise, c , and diameter, $d = 2r$
 Area = Square of diameter, d^2 , multiplied by
 the coefficient given opposite the
 quotient of $\frac{c}{d}$

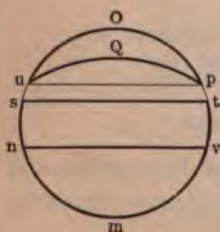


Intermediate coefficients for values
 of $\frac{c}{d}$ not given in tables are ob-
 tained by interpolation.

Example—Given: Rise = 3.78 and diam-
 eter = 8.25

$$\frac{c}{d} = 3.78 \div 8.25 = 0.458181$$

Coefficient by interpolation = 0.350929
 Area = $d^2 \times \text{coeff.} = 8.25 \times 8.25 \times 0.350929$
 = 23.8851



Circular Zone, $stvn$

Area = Area of circle — (area of segment, sot
 + area of segment, $n m v$)

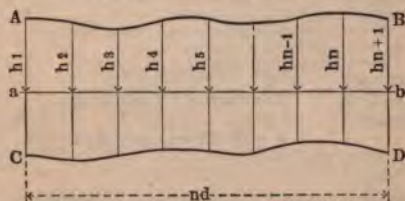
Circular Lune, $u o p q$

Area = Segment, $u o p$ — segment $u q p$

Areas of Plane Figures

Triangle:	Base $\times \frac{1}{2}$ perpendicular height $\sqrt{s(s-a)(s-b)(s-c)}$, $s = \frac{1}{2}$ sum of the three sides, a , b and c
Trapezium:	Sum of area of the two triangles
Trapezoid:	$\frac{1}{2}$ sum of parallel sides \times perpendicular height
Parallelogram:	Base \times perpendicular height
Regular Polygon:	$\frac{1}{2}$ sum of sides \times inside radius
Circle:	$\pi r^2 = 0.78540 \times \text{diameter}^2 = 0.07958 \times \text{circumference}^2$
Sector of Circle:	$\frac{\pi r^2 A^\circ}{360} = 0.0087266 r^2 A^\circ = \text{arc} \times \frac{1}{2} \text{ radius}$
Segment of Circle	$\frac{r^2}{2} \left(\frac{\pi A^\circ}{180} - \sin A^\circ \right)$
Circle of same area as square:	diameter = side $\times 1.12838$
Square of same area as circle:	side = diameter $\times 0.88623$
Ellipse:	Long diameter \times short diameter $\times 0.78540$
Parabola:	Base $\times \frac{2}{3}$ perpendicular height

Irregular Plane Surface



Divide any plane surface A, B, C, D , along a line $a-b$ into an even number, n , of parallel and sufficiently small strips, d , whose ordinates are $h_1, h_2, h_3, h_4, h_5, \dots, h_{n-1}, h_n, h_{n+1}$, and considering contours between three ordinates as parabolic curves, then for section $ABCD$,

$$\text{Area} = \frac{d}{3} \left[h_1 + h_{n+1} + 4(h_2 + h_4 + h_6 \dots + h_n) + 2(h_3 + h_5 + \dots + h_{n-1}) \right]$$

or, approximately, Area = Sum of ordinates $\times \frac{d}{3}$

Surface and Volume of Solids

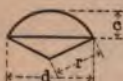
S = Lateral or Convex Surface V = Volume



Sphere

$$S = 4 \pi r^2 = \pi d^2 = 3.14159265 d^2$$

$$V = \frac{4}{3} \pi r^3 = \frac{1}{6} \pi d^3 = 0.52359878 d^3$$



Spherical Sector

$$S = \frac{1}{2} \pi r (4c + d)$$

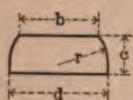
$$V = \frac{2}{3} \pi r^2 c$$



Spherical Segment

$$S = 2 \pi r c = \frac{1}{4} \pi (4c^2 + d^2)$$

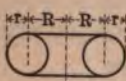
$$V = \frac{1}{3} \pi c^2 (3r - c) = \frac{1}{24} \pi c (3d^2 + 4c^2)$$



Spherical Zone

$$S = 2 \pi r c$$

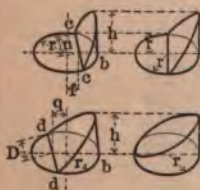
$$V = \frac{1}{24} \pi c (3b^2 + 3d^2 + 4c^2)$$



Circular Ring

$$S = 4 \pi^2 R r$$

$$V = 2 \pi^2 R r^2$$



Ungula of Right, Regular Cylinder

Base = Segment $c b c$

$$S = (2 r n - f \times \text{arc}, c b c) \frac{h}{r - f}$$

Base = Half Circle

$$V = (\frac{1}{2} n^3 - f \times \text{area}, c b c) \frac{h}{r - f}$$

$$S = \frac{2}{3} r h$$

$$V = \frac{2}{3} r^2 h$$

Base = Segment $d b d$

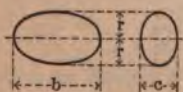
$$S = (2 r D + q \times \text{arc}, d b d) \frac{h}{r + q}$$

Base = Circle

$$V = (\frac{1}{2} D^3 + q \times \text{area}, d b d) \frac{h}{r + q}$$

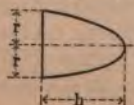
$$S = \frac{2}{3} r h$$

$$V = \frac{1}{2} r^2 \pi h$$



Ellipsoid

$$V = \frac{1}{3} \pi a b c$$



Paraboloid

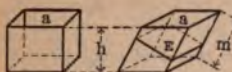
$$V = \frac{1}{2} \pi r^2 h$$

Ratio of corresponding volumes of a cone, paraboloid sphere, and cylinder of equal height : $\frac{1}{3} : \frac{1}{2} : \frac{2}{3} : 1$.

Surface and Volume of Solids

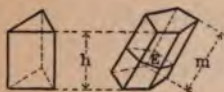
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S=Lateral or Convex Surface V=Volume



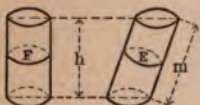
Parallelepiped

- V = Area of any face $a \times$ perpendicular distance h to the opposite face.
 V = Area of cross section E (perpendicular to the sides) \times actual length m .



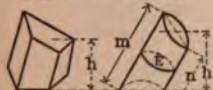
Prism, Right or Oblique, Regular or Irregular

- V = Area of one end \times perpendicular distance h to the other end.
 V = Area of cross section E (perpendicular to the sides) \times actual length m .



Cylinder, Right or Oblique, Circular or Elliptic

- S = Circumference (perpendicular to sides) as at F , or E , \times actual length h or m .
 V = Area of one end \times perpendicular distance h to other end.
 V = Area of cross section (perpendicular to sides) as at F , or $E \times$ actual length h or m .

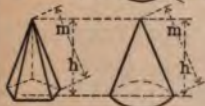


Frustum of any Prism or Cylinder

- V = Area of base \times perpendicular distance h from base to center of gravity of other end.

For Cylinder

- V = Area of cross section E (perpendicular to sides) $\times \frac{1}{2} (m + n)$.



Pyramid or Cone, Right or Regular

- V = Area of base $\times \frac{1}{3}$ perpendicular height h .
 S = Perimeter of base $\times \frac{1}{2}$ slant height m .

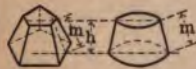
Pyramid or Cone, Right or Oblique, Regular or Irregular

- V = Area of base $\times \frac{1}{3}$ perpendicular height h .
 V = $\frac{1}{3}$ volume of prism or cylinder having same area of base and same perpendicular height.
 V = $\frac{1}{3}$ volume of hemisphere of same base and same perpendicular height.



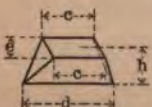
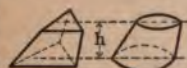
Frustum of Pyramid or Cone Right and Regular Parallel Ends

- S = Sum of perimeter of base and top $\times \frac{1}{2}$ slant height m .
 V = $\frac{1}{3} \times$ perpendicular height \times (area of top + area of base + $\sqrt{\text{area of top} \times \text{area of base}}$).



Frustum of any Pyramid or Cone, Parallel Ends

- V = $\frac{1}{3} \times$ perpendicular height $h \times$ (area of top + area of base + $\sqrt{\text{area of top} \times \text{area of base}}$).



Wedge, Parallelogram Face

- V = $\frac{1}{6}$ (sum of three edges c , d , $c \times$ perpendicular height $h \times$ perpendicular width e).

Trigonometrical Formulae

$$\text{Radius, } 1 = \sin^2 A + \cos^2 A$$

$$= \sin A \operatorname{cosec} A = \cos A \sec A = \tan A \cot A$$



$$\text{Sine } A = \frac{\cos A}{\cot A} = \frac{1}{\operatorname{cosec} A} = \cos A \tan A = \sqrt{1 - \cos^2 A}$$

$$\text{Cosine } A = \frac{\sin A}{\tan A} = \frac{r}{\sec A} = \sin A \cot A = \sqrt{1 - \sin^2 A}$$

$$\text{Tangent } A = \frac{\sin A}{\cos A} = \frac{1}{\cot A} = \sin A \sec A$$

$$\text{Cotangent } A = \frac{\cos A}{\sin A} = \frac{1}{\tan A} = \cos A \operatorname{cosec} A$$

$$\text{Secant } A = \frac{\tan A}{\sin A} = \frac{1}{\cos A}$$

$$\text{Cosecant } A = \frac{\cot A}{\cos A} = \frac{1}{\sin A}$$

$$\sin(A \pm B) = \sin A \cos B \pm \cos A \sin B \quad \tan(A \pm B) = \frac{\tan A \pm \tan B}{1 \mp \tan A \tan B}$$

$$\cos(A \pm B) = \cos A \cos B \mp \sin A \sin B \quad \cot(A \pm B) = \frac{\cot A \cot B \mp 1}{\cot B \pm \cot A}$$

$$\sin A + \sin B = 2 \sin \frac{1}{2}(A+B) \cos \frac{1}{2}(A-B) \quad \tan A + \tan B = \frac{\sin(A+B)}{\cos A \cos B}$$

$$\sin A - \sin B = 2 \cos \frac{1}{2}(A+B) \sin \frac{1}{2}(A-B) \quad \tan A - \tan B = \frac{\sin(A-B)}{\cos A \cos B}$$

$$\cos A + \cos B = 2 \cos \frac{1}{2}(A+B) \cos \frac{1}{2}(A-B) \quad \cot A + \cot B = \frac{\sin(B+A)}{\sin A \sin B}$$

$$\cos B - \cos A = 2 \sin \frac{1}{2}(A+B) \sin \frac{1}{2}(A-B) \quad \cot A - \cot B = \frac{\sin(B-A)}{\sin A \sin B}$$

$$\sin 2A = 2 \sin A \cos A \quad \tan 2A = \frac{2 \tan A}{1 - \tan^2 A}$$

$$\cos 2A = \cos^2 A - \sin^2 A \quad \cot 2A = \frac{\cot^2 A - 1}{2 \cot A}$$

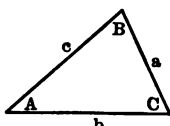
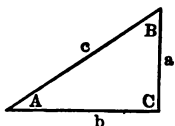
$$\sin \frac{1}{2}A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2}A = \sqrt{\frac{1 + \cos A}{2}} \quad \tan \frac{1}{2}A = \frac{\sin A}{1 + \cos A} \quad \cot \frac{1}{2}A = \frac{\sin A}{1 - \cos A}$$

$$\sin^2 A = \frac{1 - \cos 2A}{2} \quad \cos^2 A = \frac{1 + \cos 2A}{2} \quad \tan^2 A = \frac{1 - \cos 2A}{1 + \cos 2A} \quad \cot^2 A = \frac{1 + \cos 2A}{1 - \cos 2A}$$

$$\sin^2 A - \sin^2 B = \sin(A+B) \sin(A-B) \quad \cos^2 A - \sin^2 B = \cos(A+B) \cos(A-B)$$

$$\frac{\sin A \pm \sin B}{\cos A \mp \cos B} = \tan \frac{1}{2}(A \pm B) \quad \frac{\sin A \pm \sin B}{\cos B - \cos A} = \cot \frac{1}{2}(A \mp B)$$

Trigonometrical Solution of Triangles



$$S = \frac{a+b+c}{2}$$

Given	Sought	Formulae
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RIGHT-ANGLED TRIANGLES

a, c	A, B, b	$\sin A = \frac{a}{c}, \quad \cos B = \frac{a}{c}, \quad b = \sqrt{c^2 - a^2}$
	Area	$\text{Area} = \frac{a}{2} \sqrt{c^2 - a^2}$
a, b	A, B, c	$\tan A = \frac{a}{b}, \quad \tan B = \frac{b}{a}, \quad c = \sqrt{a^2 + b^2}$
	Area	$\text{Area} = \frac{a b}{2}$
A, a	B, b, c	$B = 90^\circ - A, \quad b = a \cot A, \quad c = \frac{a}{\sin A}$
	Area	$\text{Area} = \frac{a^2 \cot A}{2}$
A, b	B, a, c	$B = 90^\circ - A, \quad a = b \tan A, \quad c = \frac{b}{\cos A}$
	Area	$\text{Area} = \frac{b^2 \tan A}{2}$
A, c	B, a, b	$B = 90^\circ - A, \quad a = c \sin A, \quad b = c \cos A$
	Area	$\text{Area} = \frac{c^2 \sin A \cos A}{2} \text{ or } \frac{c^2 \sin 2A}{4}$

OBLIQUE-ANGLED TRIANGLES

a, b, c	A	$\sin \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{b c}}, \cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{b c}}, \tan \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}}$
	B	$\sin \frac{1}{2} B = \sqrt{\frac{(s-a)(s-c)}{a c}}, \cos \frac{1}{2} B = \sqrt{\frac{s(s-b)}{a c}}, \tan \frac{1}{2} B = \sqrt{\frac{(s-a)(s-c)}{s(s-b)}}$
	C	$\sin \frac{1}{2} C = \sqrt{\frac{(s-a)(s-b)}{a b}}, \cos \frac{1}{2} C = \sqrt{\frac{s(s-c)}{a b}}, \tan \frac{1}{2} C = \sqrt{\frac{(s-a)(s-b)}{s(s-c)}}$
	Area	$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$

Continued on next page

Trigonometrical Solution of Triangles

Continued

Given	Sought	Formulae
OBLIQUE-ANGLED TRIANGLES		
a, A, b	b, c	$b = \frac{a \sin B}{\sin A} \quad c = \frac{a \sin C}{\sin A} = \frac{a \sin (A+B)}{\sin A}$
	Area	$\text{Area} = \frac{1}{2} a b \sin C = \frac{a^2 \sin B \sin C}{2 \sin A}$
a, b, A	B	$\sin B = \frac{b \sin A}{a}$
	c	$c = \frac{a \sin C}{\sin A} = \frac{b \sin C}{\sin B} = \sqrt{a^2 + b^2 - 2ab \cos C}$
	Area	$\text{Area} = \frac{1}{2} a b \sin C$
a, b, C	A	$\tan A = \frac{a \sin C}{b - a \cos C} \quad \tan \frac{1}{2}(A-B) = \frac{a-b}{a+b} \cot \frac{1}{2} C$
	c	$c = \sqrt{a^2 + b^2 - 2ab \cos C} = \frac{a \sin C}{\sin A}$
	Area	$\text{Area} = \frac{1}{2} ab \sin C$

$$a^2 = b^2 + c^2 - 2bc \cos A, \quad b^2 = a^2 + c^2 - 2ac \cos B, \quad c^2 = a^2 + b^2 - 2ab \cos C$$

Comparison of Standard Linear Units
Approximate Values in Common Fractions, Decimal Equivalents or Both

A	One Millim. Equals	One Centim. Equals	One Inch Equals	One Decim. Equals	One Foot Equals	One Yard Equals	One Meter Equals	One Rod Equals	One Chain Equals	One Hect'm. Equals	One Furlong Equals	One Kilom. Equals	One Mile Equals	One Knot Equals
Millimeters	1	10	25.4	100	304.8	914.4	1000	5029.2	20116.8	100,000	201,168	1,000,000	1,609,344	1,853,256
Centimeters	1/10 0.1	1	2.54	10	30.48	91.44	100	502.9	2011.68	10,000	20,116.8	100,000	160,934	185,325
Inches	1/25 0.03937	0.3937	1	3.937	12	36	39.37	198	792	3937	7920	39,370	63,360	72,903
Decimeters	1/100 0.01	0.1	1/4 0.254	1	3.048	9.144	10	50.29	201.17	1000	2011.7	10,000	16,093	18,532.5
Feet	1/30 0.0328	0.0328	1/12 0.08333	1/3 0.32808	1	3	3.2808	16.5	66	328.08	660	3280.8	5280	6080.2
Yards	1/900 0.00109	0.00109	1/36 0.0278	1/9 0.10936	1/3	1	1.0936	5.5	22	109.36	220	1093.6	1760	2026.7
Meters	1/1000 0.001	0.001	1/40 0.0254	1/10 0.1	3/10 0.3048	9/10 0.9144	1	5.0292	20.116	100	201.17	1000	1609.3	1853.3
Rods	1/5000 0.0002	0.0002	1/2000 0.0005	1/50 0.01988	2/33 0.06061	2/11 0.18182	1/5 0.19884	1	4	19.884	40	198.84	320	368.5
Chains	1/20,000 0.00005	0.00005	1/800 0.00126	1/200 0.005	1/66 0.01515	1/22 0.04545	1/20 0.04971	1/4 0.25	1	4.971	10	49.71	80	92.12
Hectometers	1/100,000 0.00001	0.00001	1/4000 0.000254	1/1000 0.001	3/1000 0.00305	1/110 0.009114	1/20 0.01	1/20 0.05029	1/5 0.20117	1	2.0117	10	16.093	18.53
Furlongs	1/200,000 0.000005	0.000005	1/7700 0.00013	1/2000 0.0005	1/650 0.00152	1/220 0.00455	1/200 0.00497	1/40 0.025	1/10 0.1	1/2 0.4971	1	4.971	8	9.212
Kilometers	1/1,000,000 0.000001	0.000001	1/40,000 0.000025	1/10,000 0.0001	3/10,000 0.00031	1/1100 0.00091	1/1000 0.001	1/200 0.00503	1/50 0.02012	1/10 0.1	1/5 0.20117	1	1.6093	1.853
Statute Miles			1/63,000		1/5280	1/1760 0.00057	1/1600 0.000625	1/320 0.00313	1/80 0.0125	1/16 0.0625	1/8 0.125	5/8 0.62137	1	1.152
Sea Miles			1/73,000		3/20,000	1/2000 0.0005	1/1850 0.00054	1/370 0.00271	1/92 0.01085	1/19 0.05396	1/11 0.09091	7/13 0.53959	7/8 0.875	1

NOTE:—At the point where any vertical column crosses any horizontal column will be found the value of the unit named at head of the vertical column expressed in terms of the unit named under A opposite the horizontal column.
 Thus, 1 Meter = 1.0936 Yards; 1 Foot = 0.3048 Meter.

Natural Tangents and Cotangents

DEGREES	TANGENTS							COTANGENTS
	0'	10'	20'	30'	40'	50'	60'	
0	0.00000	0.00291	0.00582	0.00873	0.01164	0.01455	0.01746	89
1	0.01746	0.02036	0.02328	0.02619	0.02910	0.03201	0.03492	88
2	0.03492	0.03783	0.04075	0.04366	0.04658	0.04949	0.05241	87
3	0.05241	0.05533	0.05824	0.06116	0.06408	0.06700	0.06993	86
4	0.06993	0.07285	0.07578	0.07870	0.08163	0.08456	0.08749	85
5	0.08749	0.09042	0.09335	0.09629	0.09923	0.10216	0.10510	84
6	0.10510	0.10805	0.11099	0.11394	0.11688	0.11983	0.12278	83
7	0.12278	0.12574	0.12869	0.13165	0.13461	0.13758	0.14054	82
8	0.14054	0.14351	0.14648	0.14945	0.15243	0.15540	0.15838	81
9	0.15838	0.16137	0.16435	0.16734	0.17033	0.17333	0.17633	80
10	0.17633	0.17933	0.18233	0.18534	0.18835	0.19136	0.19438	79
11	0.19438	0.19740	0.20042	0.20345	0.20648	0.20952	0.21256	78
12	0.21256	0.21560	0.21864	0.22169	0.22475	0.22781	0.23087	77
13	0.23087	0.23393	0.23700	0.24008	0.24316	0.24624	0.24933	76
14	0.24933	0.25242	0.25552	0.25862	0.26172	0.26483	0.26795	75
15	0.26795	0.27107	0.27419	0.27732	0.28046	0.28360	0.28675	74
16	0.28675	0.28990	0.29305	0.29621	0.29938	0.30255	0.30573	73
17	0.30573	0.30891	0.31210	0.31530	0.31850	0.32171	0.32492	72
18	0.32492	0.32814	0.33136	0.33460	0.33783	0.34108	0.34433	71
19	0.34433	0.34758	0.35085	0.35412	0.35740	0.36068	0.36397	70
20	0.36397	0.36727	0.37057	0.37388	0.37720	0.38053	0.38386	69
21	0.38386	0.38721	0.39055	0.39391	0.39727	0.40065	0.40403	68
22	0.40403	0.40741	0.41081	0.41421	0.41763	0.42105	0.42447	67
23	0.42447	0.42791	0.43136	0.43481	0.43828	0.44175	0.44523	66
24	0.44523	0.44872	0.45222	0.45573	0.45924	0.46277	0.46631	65
25	0.46631	0.46985	0.47341	0.47698	0.48055	0.48414	0.48773	64
26	0.48773	0.49134	0.49495	0.49858	0.50222	0.50587	0.50953	63
27	0.50953	0.51320	0.51688	0.52057	0.52427	0.52798	0.53171	62
28	0.53171	0.53545	0.53920	0.54296	0.54674	0.55051	0.55431	61
29	0.55431	0.55812	0.56194	0.56577	0.56962	0.57348	0.57735	60
30	0.57735	0.58124	0.58513	0.58905	0.59297	0.59691	0.60086	59
31	0.60086	0.60483	0.60881	0.61280	0.61681	0.62083	0.62487	58
32	0.62487	0.62892	0.63299	0.63707	0.64117	0.64528	0.64941	57
33	0.64941	0.65355	0.65771	0.66189	0.66608	0.67028	0.67451	56
34	0.67451	0.67875	0.68301	0.68728	0.69157	0.69588	0.70021	55
35	0.70021	0.70455	0.70891	0.71329	0.71769	0.72211	0.72654	54
36	0.72654	0.73100	0.73547	0.73996	0.74447	0.74900	0.75355	53
37	0.75355	0.75812	0.76272	0.76733	0.77196	0.77661	0.78129	52
38	0.78129	0.78598	0.79070	0.79544	0.80020	0.80498	0.80978	51
39	0.80978	0.81461	0.81946	0.82434	0.82923	0.83415	0.83910	50
40	0.83910	0.84407	0.84906	0.85408	0.85912	0.86419	0.86929	49
41	0.86929	0.87441	0.87955	0.88473	0.88992	0.89515	0.90040	48
42	0.90040	0.90569	0.91099	0.91633	0.92170	0.92709	0.93252	47
43	0.93252	0.93797	0.94345	0.94896	0.95451	0.96008	0.96569	46
44	0.96569	0.97133	0.97700	0.98270	0.98843	0.99420	1.00000	45
TANGENTS	60'	50'	40'	30'	20'	10'	0'	DEGREES

COTANGENTS

JONES & LAUGHLIN STEEL COMPANY

Natural Tangents and Cotangents

Degrees	COTANGENTS							TANGENTS
	0'	10'	20'	30'	40'	50'	60'	
0	∞	343.77371	171.88540	114.58865	85.93979	68.75009	57.28996	89
1	57.28996	49.10388	42.96408	38.18846	34.36777	31.24158	28.63625	88
2	28.63625	26.43160	24.54176	22.90377	21.47040	20.20555	19.08114	87
3	19.08114	18.07498	17.16934	16.34986	15.60478	14.92442	14.30067	86
4	14.30067	13.72674	13.19688	12.70621	12.25051	11.82617	11.43005	85
5	11.43005	11.05943	10.71191	10.38540	10.07803	9.78817	9.51436	84
6	9.51436	9.25530	9.00983	8.77689	8.55555	8.34496	8.14435	83
7	8.14435	7.95302	7.77035	7.59575	7.42871	7.26873	7.11537	82
8	7.11537	6.96823	6.82694	6.69116	6.56055	6.43484	6.31375	81
9	6.31375	6.19703	6.08444	5.97576	5.87080	5.76937	5.67128	80
10	5.67128	5.57638	5.48451	5.39552	5.30928	5.22566	5.14455	79
11	5.14455	5.06584	4.98940	4.91516	4.84300	4.77286	4.70463	78
12	4.70463	4.63825	4.57363	4.51071	4.44942	4.38969	4.33148	77
13	4.33148	4.27471	4.21933	4.16530	4.11256	4.06107	4.01078	76
14	4.01078	3.96165	3.91364	3.86671	3.82083	3.77595	3.73205	75
15	3.73205	3.68909	3.64705	3.60588	3.56557	3.52609	3.48741	74
16	3.48741	3.44951	3.41236	3.37594	3.34023	3.30521	3.27085	73
17	3.27085	3.23714	3.20406	3.17159	3.13972	3.10842	3.07768	72
18	3.07768	3.04749	3.01783	2.98869	2.96004	2.93189	2.90421	71
19	2.90421	2.87700	2.85023	2.82391	2.79802	2.77254	2.74748	70
20	2.74748	2.72281	2.69853	2.67462	2.65109	2.62791	2.60509	69
21	2.60509	2.58261	2.56046	2.53865	2.51715	2.49597	2.47509	68
22	2.47509	2.45451	2.43422	2.41421	2.39449	2.37504	2.35585	67
23	2.35585	2.33693	2.31826	2.29984	2.28167	2.26374	2.24604	66
24	2.24604	2.22857	2.21132	2.19430	2.17749	2.16090	2.14451	65
25	2.14451	2.12832	2.11233	2.09654	2.08094	2.06553	2.05030	64
26	2.05030	2.03526	2.02039	2.00569	1.99116	1.97680	1.96261	63
27	1.96261	1.94858	1.93470	1.92098	1.90741	1.89400	1.88073	62
28	1.88073	1.86760	1.85462	1.84177	1.82907	1.81649	1.80405	61
29	1.80405	1.79174	1.77955	1.76749	1.75556	1.74375	1.73205	60
30	1.73205	1.72047	1.70901	1.69766	1.68643	1.67530	1.66428	59
31	1.66428	1.65337	1.64256	1.63185	1.62125	1.61074	1.60033	58
32	1.60033	1.59002	1.57981	1.56969	1.55966	1.54972	1.53987	57
33	1.53987	1.53010	1.52043	1.51084	1.50133	1.49190	1.48256	56
34	1.48256	1.47330	1.46411	1.45501	1.44598	1.43703	1.42815	55
35	1.42815	1.41934	1.41061	1.40195	1.39336	1.38484	1.37638	54
36	1.37638	1.36800	1.35968	1.35142	1.34323	1.33511	1.32704	53
37	1.32704	1.31904	1.31110	1.30323	1.29541	1.28764	1.27994	52
38	1.27994	1.27230	1.26471	1.25717	1.24969	1.24227	1.23490	51
39	1.23490	1.22758	1.22031	1.21310	1.20593	1.19882	1.19175	50
40	1.19175	1.18474	1.17777	1.17085	1.16398	1.15715	1.15037	49
41	1.15037	1.14363	1.13694	1.13029	1.12369	1.11713	1.11061	48
42	1.11061	1.10414	1.09770	1.09131	1.08496	1.07864	1.07237	47
43	1.07237	1.06613	1.05994	1.05378	1.04766	1.04158	1.03553	46
44	1.03553	1.02952	1.02355	1.01761	1.01170	1.00583	1.00000	45
COTAN- GENTS	TANGENTS							DEGREES
	60'	50'	40'	30'	20'	10'	0'	

JONES & LAUGHLIN STEEL COMPANY

Natural Sines and Cosines

Degrees	SINES							Cosines
	0'	10'	20'	30'	40'	50'	60'	
0	0.00000	0.00291	0.00582	0.00873	0.01164	0.01454	0.01745	89
1	0.01745	0.02036	0.02327	0.02618	0.02908	0.03199	0.03490	88
2	0.03490	0.03781	0.04071	0.04362	0.04653	0.04943	0.05234	87
3	0.05234	0.05524	0.05814	0.06105	0.06395	0.06685	0.06976	86
4	0.06976	0.07266	0.07556	0.07846	0.08136	0.08426	0.08716	85
5	0.08716	0.09005	0.09295	0.09585	0.09874	0.10164	0.10453	84
6	0.10453	0.10742	0.11031	0.11320	0.11609	0.11898	0.12187	83
7	0.12187	0.12476	0.12764	0.13053	0.13341	0.13629	0.13917	82
8	0.13917	0.14205	0.14493	0.14781	0.15069	0.15356	0.15643	81
9	0.15643	0.15931	0.16218	0.16505	0.16792	0.17078	0.17365	80
10	0.17365	0.17651	0.17937	0.18224	0.18509	0.18795	0.19081	79
11	0.19081	0.19366	0.19652	0.19937	0.20222	0.20507	0.20791	78
12	0.20791	0.21076	0.21360	0.21644	0.21928	0.22212	0.22495	77
13	0.22495	0.22778	0.23062	0.23345	0.23627	0.23910	0.24192	76
14	0.24192	0.24474	0.24756	0.25038	0.25320	0.25601	0.25882	75
15	0.25882	0.26163	0.26443	0.26724	0.27004	0.27284	0.27564	74
16	0.27564	0.27843	0.28123	0.28402	0.28680	0.28959	0.29237	73
17	0.29237	0.29515	0.29793	0.30071	0.30348	0.30625	0.30902	72
18	0.30902	0.31178	0.31454	0.31730	0.32006	0.32282	0.32557	71
19	0.32557	0.32832	0.33106	0.33381	0.33655	0.33929	0.34202	70
20	0.34202	0.34475	0.34748	0.35021	0.35293	0.35565	0.35837	69
21	0.35837	0.36108	0.36379	0.36650	0.36921	0.37191	0.37461	68
22	0.37461	0.37730	0.37999	0.38268	0.38537	0.38805	0.39073	67
23	0.39073	0.39341	0.39608	0.39875	0.40142	0.40408	0.40674	66
24	0.40674	0.40939	0.41204	0.41469	0.41734	0.41998	0.42262	65
25	0.42262	0.42525	0.42788	0.43051	0.43313	0.43575	0.43837	64
26	0.43837	0.44098	0.44359	0.44620	0.44880	0.45140	0.45399	63
27	0.45399	0.45658	0.45917	0.46175	0.46433	0.46690	0.46947	62
28	0.46947	0.47204	0.47460	0.47716	0.47971	0.48226	0.48481	61
29	0.48481	0.48735	0.48989	0.49242	0.49495	0.49748	0.50000	60
30	0.50000	0.50252	0.50503	0.50754	0.51004	0.51254	0.51504	59
31	0.51504	0.51753	0.52002	0.52250	0.52498	0.52745	0.52992	58
32	0.52992	0.53238	0.53484	0.53730	0.53975	0.54220	0.54464	57
33	0.54464	0.54708	0.54951	0.55194	0.55436	0.55678	0.55919	56
34	0.55919	0.56160	0.56401	0.56641	0.56880	0.57119	0.57358	55
35	0.57358	0.57596	0.57833	0.58070	0.58307	0.58543	0.58779	54
36	0.58779	0.59014	0.59248	0.59482	0.59716	0.59949	0.60182	53
37	0.60182	0.60414	0.60645	0.60876	0.61107	0.61337	0.61566	52
38	0.61566	0.61795	0.62024	0.62251	0.62479	0.62706	0.62932	51
39	0.62932	0.63158	0.63383	0.63608	0.63832	0.64056	0.64279	50
40	0.64279	0.64501	0.64723	0.64945	0.65166	0.65386	0.65606	49
41	0.65606	0.65825	0.66044	0.66262	0.66480	0.66697	0.66913	48
42	0.66913	0.67129	0.67344	0.67559	0.67773	0.67987	0.68200	47
43	0.68200	0.68412	0.68624	0.68835	0.69046	0.69256	0.69466	46
44	0.69466	0.69675	0.69883	0.70091	0.70298	0.70505	0.70711	45
Sines	60'	50'	40'	30'	20'	10'	0'	Degrees
	COSINES							

JONES & LAUGHLIN STEEL COMPANY

Natural Sines and Cosines

Degrees	COSINES							SINES
	0'	10'	20'	30'	40'	50'	60'	
0	1.00000	1.00000	0.99998	0.99996	0.99993	0.99989	0.99985	89
1	0.99985	0.99979	0.99973	0.99966	0.99958	0.99949	0.99939	88
2	0.99939	0.99929	0.99917	0.99905	0.99892	0.99878	0.99863	87
3	0.99863	0.99847	0.99831	0.99813	0.99795	0.99776	0.99756	86
4	0.99756	0.99736	0.99714	0.99692	0.99668	0.99644	0.99619	85
5	0.99619	0.99594	0.99567	0.99540	0.99511	0.99482	0.99452	84
6	0.99452	0.99421	0.99390	0.99357	0.99324	0.99290	0.99255	83
7	0.99255	0.99219	0.99182	0.99144	0.99106	0.99067	0.99027	82
8	0.99027	0.98986	0.98944	0.98902	0.98858	0.98814	0.98769	81
9	0.98769	0.98723	0.98676	0.98629	0.98580	0.98531	0.98481	80
10	0.98481	0.98430	0.98378	0.98325	0.98272	0.98218	0.98163	79
11	0.98163	0.98107	0.98050	0.97992	0.97934	0.97875	0.97815	78
12	0.97815	0.97754	0.97692	0.97630	0.97566	0.97502	0.97437	77
13	0.97437	0.97371	0.97304	0.97237	0.97169	0.97100	0.97030	76
14	0.97030	0.96959	0.96887	0.96815	0.96742	0.96667	0.96593	75
15	0.96593	0.96517	0.96440	0.96363	0.96285	0.96206	0.96126	74
16	0.96126	0.96046	0.95964	0.95882	0.95799	0.95715	0.95630	73
17	0.95630	0.95545	0.95459	0.95372	0.95284	0.95195	0.95106	72
18	0.95106	0.95015	0.94924	0.94832	0.94740	0.94646	0.94552	71
19	0.94552	0.94457	0.94361	0.94264	0.94167	0.94068	0.93969	70
20	0.93969	0.93869	0.93769	0.93667	0.93565	0.93462	0.93358	69
21	0.93358	0.93253	0.93148	0.93042	0.92935	0.92827	0.92718	68
22	0.92718	0.92609	0.92499	0.92388	0.92276	0.92164	0.92050	67
23	0.92050	0.91936	0.91822	0.91706	0.91590	0.91472	0.91355	66
24	0.91355	0.91236	0.91116	0.90996	0.90875	0.90753	0.90631	65
25	0.90631	0.90507	0.90383	0.90259	0.90133	0.90007	0.89879	64
26	0.89879	0.89752	0.89623	0.89493	0.89363	0.89232	0.89101	63
27	0.89101	0.88968	0.88835	0.88701	0.88566	0.88431	0.88295	62
28	0.88295	0.88158	0.88020	0.87882	0.87743	0.87603	0.87462	61
29	0.87462	0.87321	0.87178	0.87036	0.86892	0.86748	0.86603	60
30	0.86603	0.86457	0.86310	0.86163	0.86015	0.85866	0.85717	59
31	0.85717	0.85567	0.85416	0.85264	0.85112	0.84959	0.84805	58
32	0.84805	0.84650	0.84495	0.84339	0.84182	0.84025	0.83867	57
33	0.83867	0.83708	0.83549	0.83389	0.83228	0.83066	0.82904	56
34	0.82904	0.82741	0.82577	0.82413	0.82248	0.82082	0.81915	55
35	0.81915	0.81748	0.81580	0.81412	0.81242	0.81072	0.80902	54
36	0.80902	0.80730	0.80558	0.80386	0.80212	0.80038	0.79864	53
37	0.79864	0.79688	0.79512	0.79335	0.79158	0.78980	0.78801	52
38	0.78801	0.78622	0.78442	0.78261	0.78079	0.77897	0.77715	51
39	0.77715	0.77531	0.77347	0.77162	0.76977	0.76791	0.76604	50
40	0.76604	0.76417	0.76229	0.76041	0.75851	0.75661	0.75471	49
41	0.75471	0.75280	0.75088	0.74896	0.74703	0.74509	0.74314	48
42	0.74314	0.74120	0.73924	0.73728	0.73531	0.73333	0.73135	47
43	0.73135	0.72937	0.72737	0.72537	0.72337	0.72136	0.71934	46
44	0.71934	0.71732	0.71529	0.71325	0.71121	0.70916	0.70711	45
COSINES	60'	50'	40'	30'	20'	10'	0'	DEGREES

JONES & LAUGHLIN STEEL COMPANY

Natural Secants and Cosecants

Degrees	Secants							Co-secants
	0'	10'	20'	30'	40'	50'	60'	
0	1.00000	1.00000	1.00002	1.00004	1.00007	1.00011	1.00015	89
1	1.00015	1.00021	1.00027	1.00034	1.00042	1.00051	1.00061	88
2	1.00061	1.00072	1.00083	1.00095	1.00108	1.00122	1.00137	87
3	1.00137	1.00153	1.00169	1.00187	1.00205	1.00224	1.00244	86
4	1.00244	1.00265	1.00287	1.00309	1.00333	1.00357	1.00382	85
5	1.00382	1.00408	1.00435	1.00463	1.00491	1.00521	1.00551	84
6	1.00551	1.00582	1.00614	1.00647	1.00681	1.00715	1.00751	83
7	1.00751	1.00787	1.00825	1.00863	1.00902	1.00942	1.00983	82
8	1.00983	1.01024	1.01067	1.01111	1.01155	1.01200	1.01247	81
9	1.01247	1.01294	1.01342	1.01391	1.01440	1.01491	1.01543	80
10	1.01543	1.01595	1.01649	1.01703	1.01758	1.01815	1.01872	79
11	1.01872	1.01930	1.01989	1.02049	1.02110	1.02171	1.02234	78
12	1.02234	1.02298	1.02362	1.02428	1.02494	1.02562	1.02630	77
13	1.02630	1.02700	1.02770	1.02842	1.02914	1.02987	1.03061	76
14	1.03061	1.03137	1.03213	1.03290	1.03368	1.03447	1.03528	75
15	1.03528	1.03609	1.03691	1.03774	1.03858	1.03944	1.04030	74
16	1.04030	1.04117	1.04206	1.04295	1.04385	1.04477	1.04569	73
17	1.04569	1.04663	1.04757	1.04853	1.04950	1.05047	1.05146	72
18	1.05146	1.05246	1.05347	1.05449	1.05552	1.05657	1.05762	71
19	1.05762	1.05869	1.05976	1.06085	1.06195	1.06306	1.06418	70
20	1.06418	1.06531	1.06645	1.06761	1.06878	1.06995	1.07115	69
21	1.07115	1.07235	1.07356	1.07479	1.07602	1.07727	1.07853	68
22	1.07853	1.07981	1.08109	1.08239	1.08370	1.08503	1.08636	67
23	1.08636	1.08771	1.08907	1.09044	1.09183	1.09323	1.09464	66
24	1.09464	1.09606	1.09750	1.09895	1.10041	1.10189	1.10338	65
25	1.10338	1.10488	1.10640	1.10793	1.10947	1.11103	1.11260	64
26	1.11260	1.11419	1.11579	1.11740	1.11903	1.12067	1.12233	63
27	1.12233	1.12400	1.12568	1.12738	1.12910	1.13083	1.13257	62
28	1.13257	1.13433	1.13610	1.13789	1.13970	1.14152	1.14335	61
29	1.14335	1.14521	1.14707	1.14896	1.15085	1.15277	1.15470	60
30	1.15470	1.15665	1.15861	1.16059	1.16259	1.16460	1.16663	59
31	1.16663	1.16868	1.17075	1.17283	1.17493	1.17704	1.17918	58
32	1.17918	1.18133	1.18350	1.18569	1.18790	1.19012	1.19236	57
33	1.19236	1.19463	1.19691	1.19920	1.20152	1.20386	1.20622	56
34	1.20622	1.20859	1.21099	1.21341	1.21584	1.21830	1.22077	55
35	1.22077	1.22327	1.22579	1.22833	1.23089	1.23347	1.23607	54
36	1.23607	1.23869	1.24134	1.24400	1.24669	1.24940	1.25214	53
37	1.25214	1.25489	1.25767	1.26047	1.26330	1.26615	1.26902	52
38	1.26902	1.27191	1.27483	1.27778	1.28075	1.28374	1.28676	51
39	1.28676	1.28980	1.29287	1.29597	1.29909	1.30223	1.30541	50
40	1.30541	1.30861	1.31183	1.31509	1.31837	1.32168	1.32501	49
41	1.32501	1.32838	1.33177	1.33519	1.33864	1.34212	1.34563	48
42	1.34563	1.34917	1.35274	1.35634	1.35997	1.36363	1.36733	47
43	1.36733	1.37105	1.37481	1.37860	1.38242	1.38628	1.39016	46
44	1.39016	1.39409	1.39804	1.40203	1.40606	1.41012	1.41421	45
Secants	Cosecants							Degrees
	60'	50'	40'	30'	20'	10'	0'	

Natural Secants and Cosecants

DEGREES	COSECANTS							SECANTS
	0'	10'	20'	30'	40'	50'	60'	
0	∞	343.77516	171.88831	114.59301	85.94561	68.75736	57.29869	89
1	57.29869	49.11406	42.97571	38.20155	34.38232	31.25758	28.65371	88
2	28.65371	26.45051	24.56212	22.92559	21.49368	20.23028	19.10732	87
3	19.10732	18.10262	17.19843	16.38041	15.63679	14.95788	14.33559	86
4	14.33559	13.76312	13.23472	12.74550	12.29125	11.86837	11.47371	85
5	11.47371	11.10455	10.75849	10.43343	10.12752	9.83912	9.56677	84
6	9.56677	9.30917	9.06515	8.83367	8.61379	8.40466	8.20551	83
7	8.20551	8.01565	7.83443	7.66130	7.49571	7.33719	7.18530	82
8	7.18530	7.03962	6.89979	6.76547	6.63633	6.51208	6.39245	81
9	6.39245	6.27719	6.16607	6.05886	5.95536	5.85539	5.75877	80
10	5.75877	5.66533	5.57493	5.48740	5.40263	5.32049	5.24084	79
11	5.24084	5.16359	5.08863	5.01585	4.94517	4.87649	4.80973	78
12	4.80973	4.74482	4.68167	4.62023	4.56041	4.50216	4.44541	77
13	4.44541	4.39012	4.33622	4.28366	4.23239	4.18238	4.13357	76
14	4.13357	4.08591	4.03938	3.99393	3.94952	3.90613	3.86370	75
15	3.86370	3.82223	3.78166	3.74198	3.70315	3.66515	3.62796	74
16	3.62796	3.59154	3.55587	3.52094	3.48671	3.45317	3.42030	73
17	3.42030	3.38808	3.35649	3.32551	3.29512	3.26531	3.23607	72
18	3.23607	3.20737	3.17920	3.15155	3.12440	3.09774	3.07155	71
19	3.07155	3.04584	3.02057	2.99574	2.97135	2.94737	2.92380	70
20	2.92380	2.90063	2.87785	2.85545	2.83342	2.81175	2.79043	69
21	2.79043	2.76945	2.74881	2.72850	2.70851	2.68884	2.66947	68
22	2.66947	2.65040	2.63162	2.61313	2.59491	2.57698	2.55930	67
23	2.55930	2.54190	2.52474	2.50784	2.49119	2.47477	2.45859	66
24	2.45859	2.44264	2.42692	2.41142	2.39614	2.38107	2.36620	65
25	2.36620	2.35154	2.33708	2.32282	2.30875	2.29487	2.28117	64
26	2.28117	2.26766	2.25432	2.24116	2.22817	2.21535	2.20269	63
27	2.20269	2.19019	2.17786	2.16568	2.15366	2.14178	2.13005	62
28	2.13005	2.11847	2.10704	2.09574	2.08458	2.07356	2.06267	61
29	2.06267	2.05191	2.04128	2.03077	2.02039	2.01014	2.00000	60
30	2.00000	1.98998	1.98008	1.97029	1.96062	1.95106	1.94160	59
31	1.94160	1.93226	1.92302	1.91388	1.90485	1.89591	1.88709	58
32	1.88708	1.87834	1.86970	1.86116	1.85271	1.84435	1.83608	57
33	1.83608	1.82790	1.81981	1.81180	1.80388	1.79604	1.78829	56
34	1.78829	1.78062	1.77303	1.76552	1.75808	1.75073	1.74345	55
35	1.74345	1.73624	1.72911	1.72205	1.71506	1.70815	1.70130	54
36	1.70130	1.69452	1.68782	1.68117	1.67460	1.66809	1.66164	53
37	1.66164	1.65526	1.64894	1.64268	1.63648	1.63035	1.62427	52
38	1.62427	1.61825	1.61229	1.60639	1.60054	1.59475	1.58902	51
39	1.58902	1.58333	1.57771	1.57213	1.56661	1.56114	1.55572	50
40	1.55572	1.55036	1.54504	1.53977	1.53455	1.52938	1.52425	49
41	1.52425	1.51918	1.51415	1.50916	1.50422	1.49933	1.49448	48
42	1.49448	1.48967	1.48491	1.48019	1.47551	1.47087	1.46628	47
43	1.46628	1.46173	1.45721	1.45274	1.44831	1.44391	1.43956	46
44	1.43956	1.43524	1.43096	1.42672	1.42251	1.41835	1.41421	45
Co- SECANTS	60'	50'	40'	30'	20'	10'	0'	DEGREES

SECANTS

Functions of Numbers, 1 to 49

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
1	1	1	1.0000	1.0000	0.00000	1000.000	3.142	0.7854
2	4	8	1.4142	1.2599	0.30103	500.000	6.283	3.1416
3	9	27	1.7321	1.4422	0.47712	333.333	9.425	7.0686
4	16	64	2.0000	1.5874	0.60206	250.000	12.566	12.5664
5	25	125	2.2361	1.7100	0.69897	200.000	15.708	19.6350
6	36	216	2.4495	1.8171	0.77815	166.667	18.850	28.2743
7	49	343	2.6458	1.9129	0.84510	142.857	21.991	38.4845
8	64	512	2.8284	2.0000	0.90309	125.000	25.133	50.2655
9	81	729	3.0000	2.0801	0.95424	111.111	28.274	63.6173
10	100	1000	3.1623	2.1544	1.00000	100.000	31.416	78.5398
11	121	1331	3.3166	2.2240	1.04139	90.9091	34.558	95.0332
12	144	1728	3.4641	2.2894	1.07918	83.3333	37.699	113.097
13	169	2197	3.6056	2.3513	1.11394	76.9231	40.841	132.732
14	196	2744	3.7417	2.4101	1.14613	71.4286	43.982	153.938
15	225	3375	3.8730	2.4662	1.17609	66.6667	47.124	176.715
16	256	4096	4.0000	2.5198	1.20412	62.5000	50.265	201.062
17	289	4913	4.1231	2.5713	1.23045	58.8235	53.407	226.980
18	324	5832	4.2426	2.6207	1.25527	55.5556	56.549	254.469
19	361	6859	4.3589	2.6684	1.27875	52.6316	59.690	283.529
20	400	8000	4.4721	2.7144	1.30103	50.0000	62.832	314.159
21	441	9261	4.5826	2.7589	1.32222	47.6190	65.973	346.361
22	484	10648	4.6904	2.8020	1.34242	45.4545	69.115	380.133
23	529	12167	4.7958	2.8439	1.36173	43.4783	72.257	415.476
24	576	13824	4.8990	2.8845	1.38021	41.6667	75.398	452.389
25	625	15625	5.0000	2.9240	1.39794	40.0000	78.540	490.874
26	676	17576	5.0990	2.9625	1.41497	38.4615	81.681	530.929
27	729	19683	5.1962	3.0000	1.43136	37.0370	84.823	572.555
28	784	21952	5.2915	3.0366	1.44716	35.7143	87.965	615.752
29	841	24389	5.3852	3.0723	1.46240	34.4828	91.106	660.520
30	900	27000	5.4772	3.1072	1.47712	33.3333	94.248	706.858
31	961	29791	5.5678	3.1414	1.49136	32.2581	97.389	754.768
32	1024	32768	5.6569	3.1748	1.50515	31.2500	100.531	804.248
33	1089	35937	5.7446	3.2075	1.51851	30.3030	103.673	855.299
34	1156	39304	5.8310	3.2396	1.53148	29.4118	106.814	907.920
35	1225	42875	5.9161	3.2711	1.54407	28.5714	109.956	962.113
36	1296	46656	6.0000	3.3019	1.55630	27.7778	113.097	1017.88
37	1369	50653	6.0828	3.3322	1.56820	27.0270	116.239	1075.21
38	1444	54872	6.1644	3.3620	1.57978	26.3158	119.381	1134.11
39	1521	59319	6.2450	3.3912	1.59106	25.6410	122.522	1194.59
40	1600	64000	6.3246	3.4200	1.60206	25.0000	125.66	1256.64
41	1681	68921	6.4031	3.4482	1.61278	24.3902	128.81	1320.25
42	1764	74088	6.4807	3.4760	1.62325	23.8095	131.95	1385.44
43	1849	79507	6.5574	3.5034	1.63347	23.2558	135.09	1452.20
44	1936	85184	6.6332	3.5303	1.64345	22.7273	138.23	1520.53
45	2025	91125	6.7082	3.5569	1.65321	22.2222	141.37	1590.43
46	2116	97336	6.7823	3.5830	1.66276	21.7391	144.51	1661.90
47	2209	103823	6.8557	3.6088	1.67210	21.2766	147.65	1734.94
48	2304	110592	6.9282	3.6342	1.68124	20.8333	150.80	1809.56
49	2401	117649	7.0000	3.6593	1.69020	20.4082	153.94	1885.74

Functions of Numbers, 50 to 99

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
50	2500	125000	7.0711	3.6840	1.69897	20.0000	157.08	1963.50
51	2601	132651	7.1414	3.7084	1.70757	19.6078	160.22	2042.82
52	2704	140608	7.2111	3.7325	1.71600	19.2308	163.36	2123.72
53	2809	148877	7.2801	3.7563	1.72428	18.8679	166.50	2206.18
54	2916	157464	7.3485	3.7798	1.73239	18.5185	169.65	2290.22
55	3025	166375	7.4162	3.8030	1.74036	18.1818	172.79	2375.83
56	3136	175616	7.4833	3.8259	1.74819	17.8571	175.93	2463.01
57	3249	185193	7.5498	3.8485	1.75587	17.5439	179.07	2551.76
58	3364	195112	7.6158	3.8709	1.76343	17.2414	182.21	2642.08
59	3481	205379	7.6811	3.8930	1.77085	16.9492	185.35	2733.97
60	3600	216000	7.7460	3.9149	1.77815	16.6667	188.50	2827.43
61	3721	226981	7.8102	3.9365	1.78533	16.3934	191.64	2922.47
62	3844	238328	7.8740	3.9579	1.79239	16.1290	194.78	3019.07
63	3969	250047	7.9373	3.9791	1.79934	15.8730	197.92	3117.25
64	4096	262144	8.0000	4.0000	1.80618	15.6250	201.06	3216.99
65	4225	274625	8.0623	4.0207	1.81291	15.3846	204.20	3318.31
66	4356	287496	8.1240	4.0412	1.81954	15.1515	207.35	3421.19
67	4489	300763	8.1854	4.0615	1.82607	14.9254	210.49	3525.65
68	4624	314432	8.2462	4.0817	1.83251	14.7059	213.63	3631.68
69	4761	328509	8.3066	4.1016	1.83885	14.4925	216.77	3739.28
70	4900	343000	8.3666	4.1213	1.84510	14.2857	219.91	3848.45
71	5041	357911	8.4261	4.1408	1.85126	14.0845	223.05	3959.19
72	5184	373248	8.4853	4.1602	1.85733	13.8889	226.19	4071.50
73	5329	389017	8.5440	4.1793	1.86332	13.6986	229.34	4185.39
74	5476	405224	8.6023	4.1983	1.86923	13.5135	232.48	4300.84
75	5625	421875	8.6603	4.2172	1.87506	13.3333	235.62	4417.86
76	5776	438976	8.7178	4.2358	1.88081	13.1579	238.76	4536.46
77	5929	456533	8.7750	4.2543	1.88649	12.9870	241.90	4656.63
78	6084	474552	8.8318	4.2727	1.89209	12.8205	245.04	4778.36
79	6241	493039	8.8882	4.2908	1.89763	12.6582	248.19	4901.67
80	6400	512000	8.9443	4.3089	1.90309	12.5000	251.33	5026.55
81	6561	531441	9.0000	4.3267	1.90849	12.3457	254.47	5153.00
82	6724	551368	9.0554	4.3445	1.91381	12.1951	257.61	5281.02
83	6889	571787	9.1104	4.3621	1.91908	12.0482	260.75	5410.61
84	7056	592704	9.1652	4.3795	1.92428	11.9048	263.89	5541.77
85	7225	614125	9.2195	4.3968	1.92942	11.7647	267.04	5674.50
86	7396	636056	9.2736	4.4140	1.93450	11.6279	270.18	5808.80
87	7569	658503	9.3274	4.4310	1.93952	11.4943	273.32	5944.68
88	7744	681472	9.3808	4.4480	1.94448	11.3636	276.46	6082.12
89	7921	704969	9.4340	4.4647	1.94939	11.2360	279.60	6221.14
90	8100	729000	9.4868	4.4814	1.95424	11.1111	282.74	6361.73
91	8281	753571	9.5394	4.4979	1.95904	10.9890	285.88	6503.88
92	8464	778688	9.5917	4.5144	1.96379	10.8696	289.03	6647.61
93	8649	804357	9.6437	4.5307	1.96848	10.7527	292.17	6792.91
94	8836	830584	9.6954	4.5468	1.97313	10.6383	295.31	6939.78
95	9025	857375	9.7468	4.5629	1.97772	10.5263	298.45	7088.22
96	9216	884736	9.7980	4.5789	1.98227	10.4167	301.59	7238.23
97	9409	912673	9.8489	4.5947	1.98677	10.3093	304.73	7389.81
98	9604	941192	9.8995	4.6104	1.99123	10.2041	307.88	7542.96
99	9801	970299	9.9499	4.6261	1.99564	10.1010	311.02	7697.69

Functions of Numbers, 100 to 149

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
100	10000	1000000	10.0000	4.6416	2.00000	10.0000	314.16	7853.98
101	10201	1030301	10.0499	4.6570	2.00432	9.90099	317.30	8011.85
102	10404	1061208	10.0995	4.6723	2.00860	9.80392	320.44	8171.28
103	10609	1092727	10.1489	4.6875	2.01284	9.70874	323.58	8332.29
104	10816	1124864	10.1980	4.7027	2.01703	9.61538	326.73	8494.87
105	11025	1157625	10.2470	4.7177	2.02119	9.52381	329.87	8659.01
106	11236	1191016	10.2956	4.7326	2.02531	9.43396	333.01	8824.73
107	11449	1225043	10.3441	4.7475	2.02938	9.34579	336.15	8992.02
108	11664	1259712	10.3923	4.7622	2.03342	9.25926	339.29	9160.88
109	11881	1295029	10.4403	4.7769	2.03743	9.17431	342.43	9331.32
110	12100	1331000	10.4881	4.7914	2.04139	9.09091	345.58	9503.32
111	12321	1367631	10.5357	4.8059	2.04532	9.00901	348.72	9676.89
112	12544	1404928	10.5830	4.8203	2.04922	8.92857	351.86	9852.03
113	12769	1442897	10.6301	4.8346	2.05308	8.84956	355.00	10028.7
114	12996	1481544	10.6771	4.8488	2.05690	8.77193	358.14	10207.0
115	13225	1520875	10.7238	4.8629	2.06070	8.69565	361.28	10386.9
116	13456	1560896	10.7703	4.8770	2.06446	8.62069	364.42	10568.3
117	13689	1601613	10.8167	4.8910	2.06819	8.54701	367.57	10751.3
118	13924	1643032	10.8628	4.9049	2.07188	8.47458	370.71	10935.9
119	14161	1685159	10.9087	4.9187	2.07555	8.40336	373.85	11122.0
120	14400	1728000	10.9545	4.9324	2.07918	8.33333	376.99	11309.7
121	14641	1771561	11.0000	4.9461	2.08279	8.26446	380.13	11499.0
122	14884	1815848	11.0454	4.9597	2.08636	8.19672	383.27	11689.9
123	15129	1860867	11.0905	4.9732	2.08991	8.13008	386.42	11882.3
124	15376	1906624	11.1355	4.9866	2.09342	8.06452	389.56	12076.3
125	15625	1953125	11.1803	5.0000	2.09691	8.00000	392.70	12271.8
126	15876	2000376	11.2250	5.0133	2.10037	7.93651	395.84	12469.0
127	16129	2048383	11.2694	5.0265	2.10380	7.87402	398.98	12667.7
128	16384	2097152	11.3137	5.0397	2.10721	7.81250	402.12	12868.0
129	16641	2146689	11.3578	5.0528	2.11059	7.75194	405.27	13069.8
130	16900	2197000	11.4018	5.0658	2.11394	7.69231	408.41	13273.2
131	17161	2248091	11.4455	5.0788	2.11727	7.63359	411.55	13478.2
132	17424	2299968	11.4891	5.0916	2.12057	7.57576	414.69	13684.8
133	17689	2352637	11.5326	5.1045	2.12385	7.51880	417.83	13892.9
134	17956	2406104	11.5758	5.1172	2.12710	7.46269	420.97	14102.6
135	18225	2460375	11.6190	5.1299	2.13033	7.40741	424.12	14313.9
136	18496	2515456	11.6619	5.1426	2.13354	7.35294	427.26	14526.7
137	18769	2571353	11.7047	5.1551	2.13672	7.29927	430.40	14741.1
138	19044	2628072	11.7473	5.1676	2.13988	7.24638	433.54	14957.1
139	19321	2685619	11.7898	5.1801	2.14301	7.19424	436.68	15174.7
140	19600	2744000	11.8322	5.1925	2.14613	7.14286	439.82	15393.8
141	19881	2803221	11.8743	5.2048	2.14922	7.09220	442.96	15614.5
142	20164	2863288	11.9164	5.2171	2.15229	7.04225	446.11	15836.8
143	20449	2924207	11.9583	5.2293	2.15534	6.99301	449.25	16060.6
144	20736	2985984	12.0000	5.2415	2.15836	6.94444	452.39	16286.0
145	21025	3048625	12.0416	5.2536	2.16137	6.89655	455.53	16513.0
146	21316	3112136	12.0830	5.2656	2.16435	6.84932	458.67	16741.5
147	21609	3176623	12.1244	5.2776	2.16732	6.80272	461.81	16971.7
148	21904	3241792	12.1655	5.2896	2.17026	6.75676	464.96	17203.4
149	22201	3307949	12.2066	5.3015	2.17319	6.71141	468.10	17436.6

Functions of Numbers, 150 to 199

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
150	22500	3375000	12.2474	5.3133	2.17609	6.66667	471.24	17671.5
151	22801	3442951	12.2882	5.3251	2.17898	6.62252	474.38	17907.9
152	23104	3511808	12.3288	5.3368	2.18184	6.57895	477.52	18145.8
153	23409	3581677	12.3693	5.3485	2.18469	6.53595	480.66	18385.4
154	23716	3652264	12.4097	5.3601	2.18752	6.49351	483.81	18626.5
155	24025	3723875	12.4499	5.3717	2.19033	6.45161	486.95	18869.2
156	24336	3796416	12.4900	5.3832	2.19312	6.41026	490.09	19113.4
157	24649	3869893	12.5300	5.3947	2.19590	6.36943	493.23	19359.3
158	24964	3944312	12.5698	5.4061	2.19866	6.32911	496.37	19606.7
159	25281	4019679	12.6095	5.4175	2.20140	6.28931	499.51	19855.7
160	25600	4096000	12.6491	5.4288	2.20412	6.25000	502.65	20106.2
161	25921	4173281	12.6886	5.4401	2.20683	6.21118	505.80	20358.3
162	26244	4251528	12.7279	5.4514	2.20952	6.17284	508.94	20612.0
163	26569	4330747	12.7671	5.4626	2.21219	6.13497	512.08	20867.2
164	26896	4410944	12.8062	5.4737	2.21484	6.09756	515.22	21124.1
165	27225	4492125	12.8452	5.4848	2.21748	6.06061	518.36	21382.5
166	27556	4574296	12.8841	5.4959	2.22011	6.02410	521.50	21642.4
167	27889	4657463	12.9228	5.5069	2.22272	5.98802	524.65	21904.0
168	28224	4741632	12.9615	5.5178	2.22531	5.95238	527.79	22167.1
169	28561	4826809	13.0000	5.5288	2.22789	5.91716	530.93	22431.8
170	28900	4913000	13.0384	5.5397	2.23045	5.88235	534.07	22698.0
171	29241	5000211	13.0767	5.5505	2.23300	5.84795	537.21	22965.8
172	29584	5088448	13.1149	5.5613	2.23553	5.81395	540.35	23235.2
173	29929	5177717	13.1529	5.5721	2.23805	5.78035	543.50	23506.2
174	30276	5268024	13.1909	5.5828	2.24055	5.74713	546.64	23778.7
175	30625	5359375	13.2288	5.5934	2.24304	5.71429	549.78	24052.8
176	30976	5451776	13.2665	5.6041	2.24551	5.68182	552.92	24328.5
177	31329	5545233	13.3041	5.6147	2.24797	5.64972	556.06	24605.7
178	31684	5639752	13.3417	5.6252	2.25042	5.61798	559.20	24884.6
179	32041	5735339	13.3791	5.6357	2.25285	5.58659	562.35	25164.9
180	32400	5832000	13.4164	5.6462	2.25527	5.55556	565.49	25446.9
181	32761	5929741	13.4536	5.6567	2.25768	5.52486	568.63	25730.4
182	33124	6028568	13.4907	5.6671	2.26007	5.49451	571.77	26015.5
183	33489	6128487	13.5277	5.6774	2.26245	5.46448	574.91	26302.2
184	33856	6229504	13.5647	5.6877	2.26482	5.43478	578.05	26590.4
185	34225	6331625	13.6015	5.6980	2.26717	5.40541	581.19	26880.3
186	34596	6434856	13.6382	5.7083	2.26951	5.37634	584.34	27171.6
187	34969	6539203	13.6748	5.7185	2.27184	5.34759	587.48	27464.6
188	35344	6644672	13.7113	5.7287	2.27416	5.31915	590.62	27759.1
189	35721	6751269	13.7477	5.7388	2.27646	5.29101	593.76	28055.2
190	36100	6859000	13.7840	5.7489	2.27875	5.26316	596.90	28352.9
191	36481	6967871	13.8203	5.7590	2.28103	5.23560	600.04	28652.1
192	36864	7077888	13.8564	5.7690	2.28330	5.20833	603.19	28952.9
193	37249	7189057	13.8924	5.7790	2.28556	5.18135	606.33	29255.3
194	37636	7301384	13.9284	5.7890	2.28780	5.15464	609.47	29559.2
195	38025	7414875	13.9642	5.7989	2.29003	5.12821	612.61	29864.8
196	38416	7529536	14.0000	5.8088	2.29226	5.10204	615.75	30171.9
197	38809	7645373	14.0357	5.8186	2.29447	5.07614	618.89	30480.5
198	39204	7762392	14.0712	5.8285	2.29667	5.05051	622.04	30790.7
199	39601	7880509	14.1067	5.8383	2.29885	5.02513	625.18	31102.6

Functions of Numbers, 250 to 299

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
250	62500	15625000	15.8114	6.2996	2.39794	4.00000	785.40	49087.4
251	63001	15813251	15.8430	6.3080	2.39967	3.98406	788.54	49480.9
252	63504	16003008	15.8745	6.3164	2.40140	3.96825	791.68	49875.9
253	64009	16194277	15.9060	6.3247	2.40312	3.95257	794.82	50272.6
254	64516	16387064	15.9374	6.3330	2.40483	3.93701	797.96	50670.7
255	65025	16581375	15.9687	6.3413	2.40654	3.92157	801.11	51070.5
256	65536	16777216	16.0000	6.3496	2.40824	3.90625	804.25	51471.9
257	66049	16974593	16.0312	6.3579	2.40993	3.89105	807.39	51874.8
258	66564	17173512	16.0624	6.3661	2.41162	3.87597	810.53	52279.2
259	67081	17373979	16.0935	6.3743	2.41330	3.86100	813.67	52685.3
260	67600	17576000	16.1245	6.3825	2.41497	3.84615	816.81	53092.9
261	68121	17779581	16.1555	6.3907	2.41664	3.83142	819.96	53502.1
262	68644	17984728	16.1864	6.3988	2.41830	3.81679	823.10	53912.9
263	69169	18191447	16.2173	6.4070	2.41996	3.80228	826.24	54325.2
264	69696	18399744	16.2481	6.4151	2.42160	3.78788	829.38	54739.1
265	70225	18609625	16.2788	6.4232	2.42325	3.77358	832.52	55154.6
266	70756	18821096	16.3095	6.4312	2.42488	3.75940	835.66	55571.6
267	71289	19034163	16.3401	6.4393	2.42651	3.74532	838.81	55990.2
268	71824	19248832	16.3707	6.4473	2.42813	3.73134	841.95	56410.4
269	72361	19465109	16.4012	6.4553	2.42975	3.71747	845.09	56832.2
270	72900	19683000	16.4317	6.4633	2.43136	3.70370	848.23	57255.5
271	73441	19902511	16.4621	6.4713	2.43297	3.69004	851.37	57680.4
272	73984	20123648	16.4924	6.4792	2.43457	3.67647	854.51	58106.9
273	74529	20346417	16.5227	6.4872	2.43616	3.66300	857.65	58534.9
274	75076	20570824	16.5529	6.4951	2.43775	3.64964	860.80	58964.6
275	75625	20796875	16.5831	6.5030	2.43933	3.63636	863.94	59395.7
276	76176	21024576	16.6132	6.5108	2.44091	3.62319	867.08	59828.5
277	76729	21253933	16.6433	6.5187	2.44248	3.61011	870.22	60262.8
278	77284	21484952	16.6733	6.5265	2.44404	3.59712	873.36	60698.7
279	77841	21717639	16.7033	6.5343	2.44560	3.58423	876.50	61136.2
280	78400	21952000	16.7332	6.5421	2.44716	3.57143	879.65	61575.2
281	78961	22188041	16.7631	6.5499	2.44871	3.55872	882.79	62015.8
282	79524	22425768	16.7929	6.5577	2.45025	3.54610	885.93	62458.0
283	80089	22665187	16.8226	6.5654	2.45179	3.53357	889.07	62901.8
284	80656	22906304	16.8523	6.5731	2.45332	3.52113	892.21	63347.1
285	81225	23149125	16.8819	6.5808	2.45484	3.50877	895.35	63794.0
286	81796	23393656	16.9115	6.5885	2.45637	3.49650	898.50	64242.4
287	82369	23639903	16.9411	6.5962	2.45788	3.48432	901.64	64692.5
288	82944	23887872	16.9706	6.6039	2.45939	3.47222	904.78	65144.1
289	83521	24137569	17.0000	6.6115	2.46090	3.46021	907.92	65597.2
290	84100	24389000	17.0294	6.6191	2.46240	3.44828	911.06	66052.0
291	84681	24642171	17.0587	6.6267	2.46389	3.43643	914.20	66508.3
292	85264	24897088	17.0880	6.6343	2.46538	3.42466	917.35	66966.2
293	85849	25153757	17.1172	6.6419	2.46687	3.41297	920.49	67425.6
294	86436	25412184	17.1464	6.6494	2.46835	3.40136	923.63	67886.7
295	87025	25672375	17.1756	6.6569	2.46982	3.38983	926.77	68349.3
296	87616	25934336	17.2047	6.6644	2.47129	3.37838	929.91	68813.4
297	88209	26198073	17.2337	6.6719	2.47276	3.36700	933.05	69279.2
298	88804	26463592	17.2627	6.6794	2.47422	3.35570	936.19	69746.5
299	89401	26730899	17.2916	6.6869	2.47567	3.34448	939.34	70215.4

Functions of Numbers, 200 to 249

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
200	40000	8000000	14.1421	5.8480	2.30103	5.00000	628.32	31415.9
201	40401	8120601	14.1774	5.8578	2.30320	4.97512	631.46	31730.9
202	40804	8242408	14.2127	5.8675	2.30535	4.95050	634.60	32047.4
203	41209	8365427	14.2478	5.8771	2.30750	4.92611	637.74	32365.5
204	41616	8489664	14.2829	5.8868	2.30963	4.90196	640.88	32685.1
205	42025	8615125	14.3178	5.8964	2.31175	4.87805	644.03	33006.4
206	42436	8741816	14.3527	5.9059	2.31387	4.85437	647.17	33329.2
207	42849	8869743	14.3875	5.9155	2.31597	4.83092	650.31	33653.5
208	43264	8998912	14.4222	5.9250	2.31806	4.80769	653.45	33979.5
209	43681	9129329	14.4568	5.9345	2.32015	4.78469	656.59	34307.0
210	44100	9261000	14.4914	5.9439	2.32222	4.76190	659.73	34636.1
211	44521	9393931	14.5258	5.9533	2.32428	4.73934	662.88	34966.7
212	44944	9528128	14.5602	5.9627	2.32634	4.71698	666.02	35298.9
213	45369	9663597	14.5945	5.9721	2.32838	4.69484	669.16	35632.7
214	45796	9800344	14.6287	5.9814	2.33041	4.67290	672.30	35968.1
215	46225	9938375	14.6629	5.9907	2.33244	4.65116	675.44	36305.0
216	46656	10077696	14.6969	6.0000	2.33445	4.62963	678.58	36643.5
217	47089	10218313	14.7309	6.0092	2.33646	4.60829	681.73	36983.6
218	47524	10360232	14.7648	6.0185	2.33846	4.58716	684.87	37325.3
219	47961	10503459	14.7986	6.0277	2.34044	4.56621	688.01	37668.5
220	48400	10648000	14.8324	6.0368	2.34242	4.54545	691.15	38013.3
221	48841	10793861	14.8661	6.0459	2.34439	4.52489	694.29	38359.6
222	49284	10941048	14.8997	6.0550	2.34635	4.50450	697.43	38707.6
223	49729	11089567	14.9332	6.0641	2.34830	4.48430	700.58	39057.1
224	50176	11239424	14.9666	6.0732	2.35025	4.46429	703.72	39408.1
225	50625	11390625	15.0000	6.0822	2.35218	4.44444	706.86	39760.8
226	51076	11543176	15.0333	6.0912	2.35411	4.42478	710.00	40115.0
227	51529	11697083	15.0665	6.1002	2.35603	4.40529	713.14	40470.8
228	51984	11852352	15.0997	6.1091	2.35793	4.38596	716.28	40828.1
229	52441	12008989	15.1327	6.1180	2.35984	4.36681	719.42	41187.1
230	52900	12167000	15.1658	6.1269	2.36173	4.34783	722.57	41547.6
231	53361	12326391	15.1987	6.1358	2.36361	4.32900	725.71	41909.6
232	53824	12487168	15.2315	6.1446	2.36549	4.31034	728.85	42273.3
233	54289	12649337	15.2643	6.1534	2.36736	4.29185	731.99	42638.5
234	54756	12812904	15.2971	6.1622	2.36922	4.27350	735.13	43005.3
235	55225	12977875	15.3297	6.1710	2.37107	4.25532	738.27	43373.6
236	55696	13144256	15.3623	6.1797	2.37291	4.23729	741.42	43743.5
237	56169	13312053	15.3948	6.1885	2.37475	4.21941	744.56	44115.0
238	56644	13481272	15.4272	6.1972	2.37658	4.20168	747.70	44488.1
239	57121	13651919	15.4596	6.2058	2.37840	4.18410	750.84	44862.7
240	57600	13824000	15.4919	6.2145	2.38021	4.16667	753.98	45238.9
241	58081	13997521	15.5242	6.2231	2.38202	4.14938	757.12	45616.7
242	58564	14172488	15.5563	6.2317	2.38382	4.13223	760.27	45996.1
243	59049	14348907	15.5885	6.2403	2.38561	4.11523	763.41	46377.0
244	59536	14526784	15.6205	6.2488	2.38739	4.09836	766.55	46759.5
245	60025	14706125	15.6525	6.2573	2.38917	4.08163	769.69	47143.5
246	60516	14886936	15.6844	6.2658	2.39094	4.06504	772.83	47529.2
247	61009	15069223	15.7162	6.2743	2.39270	4.04858	775.97	47916.4
248	61504	15252992	15.7480	6.2828	2.39445	4.03226	779.12	48305.1
249	62001	15438249	15.7797	6.2912	2.39620	4.01606	782.26	48695.5

Functions of Numbers, 250 to 299

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
250	62500	15625000	15.8114	6.2996	2.39794	4.00000	785.40	49087.4
251	63001	15813251	15.8430	6.3080	2.39967	3.98406	788.54	49480.9
252	63504	16003008	15.8745	6.3164	2.40140	3.96825	791.68	49875.9
253	64009	16194277	15.9060	6.3247	2.40312	3.95257	794.82	50272.6
254	64516	16387064	15.9374	6.3330	2.40483	3.93701	797.96	50670.7
255	65025	16581375	15.9687	6.3413	2.40654	3.92157	801.11	51070.5
256	65536	16777216	16.0000	6.3496	2.40824	3.90625	804.25	51471.9
257	66049	16974593	16.0312	6.3579	2.40993	3.89105	807.39	51874.8
258	66564	17173512	16.0624	6.3661	2.41162	3.87597	810.53	52279.2
259	67081	17373979	16.0935	6.3743	2.41330	3.86100	813.67	52685.3
260	67600	17576900	16.1245	6.3825	2.41497	3.84615	816.81	53092.9
261	68121	17779581	16.1555	6.3907	2.41664	3.83142	819.96	53502.1
262	68644	17984728	16.1864	6.3988	2.41830	3.81679	823.10	53912.9
263	69169	18191447	16.2173	6.4070	2.41996	3.80228	826.24	54325.2
264	69696	18399744	16.2481	6.4151	2.42160	3.78788	829.38	54739.1
265	70225	18609625	16.2788	6.4232	2.42325	3.77358	832.52	55154.6
266	70756	18821096	16.3095	6.4312	2.42488	3.75940	835.66	55571.6
267	71289	19034163	16.3401	6.4393	2.42651	3.74532	838.81	55990.2
268	71824	19248832	16.3707	6.4473	2.42813	3.73134	841.95	56410.4
269	72361	19465109	16.4012	6.4553	2.42975	3.71747	845.09	56832.2
270	72900	19683000	16.4317	6.4633	2.43136	3.70370	848.23	57255.5
271	73441	19902511	16.4621	6.4713	2.43297	3.69004	851.37	57680.4
272	73984	20123648	16.4924	6.4792	2.43457	3.67647	854.51	58106.9
273	74529	20346417	16.5227	6.4872	2.43616	3.66300	857.65	58534.9
274	75076	20570824	16.5529	6.4951	2.43775	3.64964	860.80	58964.6
275	75625	20796875	16.5831	6.5030	2.43933	3.63636	863.94	59395.7
276	76176	21024576	16.6132	6.5108	2.44091	3.62319	867.08	59828.5
277	76729	21253933	16.6433	6.5187	2.44248	3.61011	870.22	60262.8
278	77284	21484952	16.6733	6.5265	2.44404	3.59712	873.36	60698.7
279	77841	21717639	16.7033	6.5343	2.44560	3.58423	876.50	61136.2
280	78400	21952000	16.7332	6.5421	2.44716	3.57143	879.65	61575.2
281	78961	22188041	16.7631	6.5499	2.44871	3.55872	882.79	62015.8
282	79524	22425768	16.7929	6.5577	2.45025	3.54610	885.93	62458.0
283	80089	22665187	16.8226	6.5654	2.45179	3.53357	889.07	62901.8
284	80656	22906304	16.8523	6.5731	2.45332	3.52113	892.21	63347.1
285	81225	23149125	16.8819	6.5808	2.45484	3.50877	895.35	63794.0
286	81796	23393656	16.9115	6.5885	2.45637	3.49650	898.50	64242.4
287	82369	23639903	16.9411	6.5962	2.45788	3.48432	901.64	64692.5
288	82944	23887872	16.9706	6.6039	2.45939	3.47222	904.78	65144.1
289	83521	24137569	17.0000	6.6115	2.46090	3.46021	907.92	65597.2
290	84100	24389000	17.0294	6.6191	2.46240	3.44828	911.06	66052.0
291	84681	24642171	17.0587	6.6267	2.46389	3.43643	914.20	66508.3
292	85264	24897088	17.0880	6.6343	2.46538	3.42466	917.35	66966.2
293	85849	25153757	17.1172	6.6419	2.46687	3.41297	920.49	67425.6
294	86436	25412184	17.1464	6.6494	2.46835	3.40136	923.63	67886.7
295	87025	25672375	17.1756	6.6569	2.46982	3.38983	926.77	68349.3
296	87616	25934336	17.2047	6.6644	2.47129	3.37838	929.91	68813.4
297	88209	26198073	17.2337	6.6719	2.47276	3.36700	933.05	69279.2
298	88804	26463592	17.2627	6.6794	2.47422	3.35570	936.19	69746.5
299	89401	26730899	17.2916	6.6869	2.47567	3.34448	939.34	70215.4

Functions of Numbers, 300 to 349

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
300	90000	27000000	17.3205	6.6943	2.47712	3.33333	942.48	70685.8
301	90601	27270901	17.3494	6.7018	2.47857	3.32226	945.62	71157.9
302	91204	27543608	17.3781	6.7092	2.48001	3.31126	948.76	71631.5
303	91809	27818127	17.4069	6.7166	2.48144	3.30033	951.90	72106.6
304	92416	28094464	17.4356	6.7240	2.48287	3.28947	955.04	72583.4
305	93025	28372625	17.4642	6.7313	2.48430	3.27869	958.19	73061.7
306	93636	28652616	17.4929	6.7387	2.48572	3.26797	961.33	73541.5
307	94249	28934443	17.5214	6.7460	2.48714	3.25733	964.47	74023.0
308	94864	29218112	17.5499	6.7533	2.48855	3.24675	967.61	74506.0
309	95481	29503629	17.5784	6.7606	2.48996	3.23621	970.75	74990.6
310	96100	29791000	17.6068	6.7679	2.49136	3.22581	973.89	75476.8
311	96721	30080231	17.6352	6.7752	2.49276	3.21543	977.04	75964.5
312	97344	30371328	17.6635	6.7824	2.49415	3.20513	980.18	76453.8
313	97969	30664297	17.6918	6.7897	2.49554	3.19489	983.32	76944.7
314	98596	30959144	17.7200	6.7969	2.49693	3.18471	986.46	77437.1
315	99225	31255875	17.7482	6.8041	2.49831	3.17460	989.60	77931.1
316	99856	31554496	17.7764	6.8113	2.49969	3.16456	992.74	78426.7
317	100489	31855013	17.8045	6.8185	2.50106	3.15457	995.88	78923.9
318	101124	32157432	17.8326	6.8256	2.50243	3.14465	999.03	79422.6
319	101761	32461759	17.8606	6.8328	2.50379	3.13480	1002.2	79922.9
320	102400	32768000	17.8885	6.8399	2.50515	3.12500	1005.3	80424.8
321	103041	33076161	17.9165	6.8470	2.50651	3.11526	1008.5	80928.2
322	103684	33386248	17.9444	6.8541	2.50786	3.10559	1011.6	81433.2
323	104329	33698267	17.9722	6.8612	2.50920	3.09598	1014.7	81939.8
324	104976	34012224	18.0000	6.8683	2.51055	3.08642	1017.9	82448.0
325	105625	34328125	18.0278	6.8753	2.51188	3.07692	1021.0	82957.7
326	106276	34645976	18.0555	6.8824	2.51322	3.06749	1024.2	83469.0
327	106929	34965783	18.0831	6.8894	2.51455	3.05810	1027.3	83981.8
328	107584	35287552	18.1108	6.8964	2.51587	3.04878	1030.4	84496.3
329	108241	35611289	18.1384	6.9034	2.51720	3.03951	1033.6	85012.3
330	108900	35937000	18.1659	6.9104	2.51851	3.03030	1036.7	85529.9
331	109561	36264691	18.1934	6.9174	2.51983	3.02115	1039.9	86049.0
332	110224	36594368	18.2209	6.9244	2.52114	3.01205	1043.0	86569.7
333	110889	36926037	18.2483	6.9313	2.52244	3.00300	1046.2	87092.0
334	111556	37259704	18.2757	6.9382	2.52375	2.99401	1049.3	87615.9
335	112225	37595375	18.3030	6.9451	2.52504	2.98507	1052.4	88141.3
336	112896	37933056	18.3303	6.9521	2.52634	2.97619	1055.6	88668.3
337	113569	38272753	18.3576	6.9589	2.52763	2.96736	1058.7	89196.9
338	114244	38614472	18.3848	6.9658	2.52892	2.95858	1061.9	89727.0
339	114921	38958219	18.4120	6.9727	2.53020	2.94985	1065.0	90258.7
340	115600	39304000	18.4391	6.9795	2.53148	2.94118	1068.1	90792.0
341	116281	39651821	18.4662	6.9864	2.53275	2.93255	1071.3	91326.9
342	116964	40001688	18.4932	6.9932	2.53403	2.92398	1074.4	91863.3
343	117649	40353607	18.5203	7.0000	2.53529	2.91545	1077.6	92401.3
344	118336	40707584	18.5472	7.0068	2.53656	2.90695	1080.7	92940.9
345	119025	41063625	18.5742	7.0136	2.53782	2.89855	1083.8	93482.0
346	119716	41421736	18.6011	7.0203	2.53908	2.89017	1087.0	94024.7
347	120409	41781923	18.6279	7.0271	2.54033	2.88184	1090.1	94569.0
348	121104	42144192	18.6548	7.0338	2.54158	2.87356	1093.3	95114.9
349	121801	42508549	18.6815	7.0406	2.54283	2.86533	1096.4	95662.3

Functions of Numbers, 350 to 399

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
350	122500	42875000	18.7083	7.0473	2.54407	2.85714	1099.6	96211.3
351	123201	43243551	18.7350	7.0540	2.54531	2.84900	1102.7	96761.8
352	123904	43614208	18.7617	7.0607	2.54654	2.84091	1105.8	97314.0
353	124609	43986977	18.7883	7.0674	2.54777	2.83286	1109.0	97867.7
354	125316	44361864	18.8149	7.0740	2.54900	2.82486	1112.1	98423.0
355	126025	44738875	18.8414	7.0807	2.55023	2.81690	1115.3	98979.8
356	126736	45118016	18.8680	7.0873	2.55145	2.80899	1118.4	99538.2
357	127449	45499293	18.8944	7.0940	2.55267	2.80112	1121.5	100098
358	128164	45882712	18.9209	7.1006	2.55388	2.79330	1124.7	100660
359	128881	46268279	18.9473	7.1072	2.55509	2.78552	1127.8	101223
360	129600	46656000	18.9737	7.1138	2.55630	2.77778	1131.0	101788
361	130321	47045881	19.0000	7.1204	2.55751	2.77008	1134.1	102354
362	131044	47437928	19.0263	7.1269	2.55871	2.76243	1137.3	102922
363	131769	47832147	19.0526	7.1335	2.55991	2.75482	1140.4	103491
364	132496	48228544	19.0788	7.1400	2.56110	2.74725	1143.5	104062
365	133225	48627125	19.1050	7.1466	2.56229	2.73973	1146.7	104635
366	133956	49027896	19.1311	7.1531	2.56348	2.73224	1149.8	105209
367	134689	49430863	19.1572	7.1596	2.56467	2.72480	1153.0	105785
368	135424	49836032	19.1833	7.1661	2.56585	2.71739	1156.1	106362
369	136161	50243409	19.2094	7.1726	2.56703	2.71003	1159.2	106941
370	136900	50653000	19.2354	7.1791	2.56820	2.70270	1162.4	107521
371	137641	51064811	19.2614	7.1855	2.56937	2.69542	1165.5	108103
372	138384	51478848	19.2873	7.1920	2.57054	2.68817	1168.7	108687
373	139129	51895117	19.3132	7.1984	2.57171	2.68097	1171.8	109272
374	139876	52313624	19.3391	7.2048	2.57287	2.67380	1175.0	109858
375	140625	52734375	19.3649	7.2112	2.57403	2.66667	1178.1	110447
376	141376	53157376	19.3907	7.2177	2.57519	2.65957	1181.2	111036
377	142129	53582633	19.4165	7.2240	2.57634	2.65252	1184.4	111628
378	142884	54010152	19.4422	7.2304	2.57749	2.64550	1187.5	112221
379	143641	54439939	19.4679	7.2368	2.57864	2.63852	1190.7	112815
380	144400	54872000	19.4936	7.2432	2.57978	2.63158	1193.8	113411
381	145161	55306341	19.5192	7.2495	2.58093	2.62467	1196.9	114009
382	145924	55742968	19.5448	7.2558	2.58206	2.61780	1200.1	114608
383	146689	56181887	19.5704	7.2622	2.58320	2.61097	1203.2	115209
384	147456	56623104	19.5959	7.2685	2.58433	2.60417	1206.4	115812
385	148225	57066625	19.6214	7.2748	2.58540	2.59740	1209.5	116416
386	148996	57512456	19.6469	7.2811	2.58659	2.59067	1212.7	117021
387	149769	57960603	19.6723	7.2874	2.58771	2.58398	1215.8	117628
388	150544	58411072	19.6977	7.2936	2.58883	2.57732	1218.9	118237
389	151321	58863869	19.7231	7.2999	2.58995	2.57069	1222.1	118847
390	152100	59319000	19.7484	7.3061	2.59106	2.56410	1225.2	119459
391	152881	59776471	19.7737	7.3124	2.59218	2.55754	1228.4	120072
392	153664	60236288	19.7990	7.3186	2.59329	2.55102	1231.5	120687
393	154449	60698457	19.8242	7.3248	2.59439	2.54453	1234.6	121304
394	155236	61162984	19.8494	7.3310	2.59550	2.53807	1237.8	121922
395	156025	61629875	19.8746	7.3372	2.59660	2.53165	1240.9	122542
396	156816	62099136	19.8997	7.3434	2.59770	2.52525	1244.1	123163
397	157609	62570773	19.9249	7.3496	2.59879	2.51889	1247.2	123786
398	158404	63044792	19.9499	7.3558	2.59988	2.51256	1250.4	124410
399	159201	63521199	19.9750	7.3619	2.60097	2.50627	1253.5	125036

Functions of Numbers, 400 to 449

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
400	160000	64000000	20.0000	7.3681	2.60206	2.50000	1256.6	125664
401	160801	64481201	20.0250	7.3742	2.60314	2.49377	1259.8	126293
402	161604	64964808	20.0499	7.3803	2.60423	2.48756	1262.9	126923
403	162409	65450827	20.0749	7.3864	2.60531	2.48139	1266.1	127556
404	163216	65939264	20.0998	7.3925	2.60638	2.47525	1269.2	128190
405	164025	66430125	20.1246	7.3986	2.60746	2.46914	1272.3	128825
406	164836	66923416	20.1494	7.4047	2.60853	2.46305	1275.5	129462
407	165649	67419143	20.1742	7.4108	2.60959	2.45700	1278.6	130100
408	166464	67917312	20.1990	7.4169	2.61066	2.45098	1281.8	130741
409	167281	68417929	20.2237	7.4229	2.61172	2.44499	1284.9	131382
410	168100	68921000	20.2485	7.4290	2.61278	2.43902	1288.1	132025
411	168921	69426531	20.2731	7.4350	2.61384	2.43309	1291.2	132670
412	169744	69934528	20.2978	7.4410	2.61490	2.42718	1294.3	133317
413	170569	70444997	20.3224	7.4470	2.61595	2.42131	1297.5	133965
414	171396	70957944	20.3470	7.4530	2.61700	2.41546	1300.6	134614
415	172225	71473375	20.3715	7.4590	2.61805	2.40964	1303.8	135265
416	173056	71991296	20.3961	7.4650	2.61909	2.40385	1306.9	135918
417	173889	72511713	20.4206	7.4710	2.62014	2.39808	1310.0	136572
418	174724	73034632	20.4450	7.4770	2.62118	2.39234	1313.2	137228
419	175561	73560059	20.4695	7.4829	2.62221	2.38663	1316.3	137885
420	176400	74088000	20.4939	7.4889	2.62325	2.38095	1319.5	138544
421	177241	74618461	20.5183	7.4948	2.62428	2.37530	1322.6	139205
422	178084	75151448	20.5426	7.5007	2.62531	2.36967	1325.8	139867
423	178929	75686967	20.5670	7.5067	2.62634	2.36407	1328.9	140531
424	179776	76225024	20.5913	7.5126	2.62737	2.35849	1332.0	141196
425	180625	76765625	20.6155	7.5185	2.62839	2.35294	1335.2	141863
426	181476	77308776	20.6398	7.5244	2.62941	2.34742	1338.3	142531
427	182329	77854483	20.6640	7.5302	2.63043	2.34192	1341.5	143201
428	183184	78402752	20.6882	7.5361	2.63144	2.33645	1344.6	143872
429	184041	78953589	20.7123	7.5420	2.63246	2.33100	1347.7	144545
430	184900	79507000	20.7364	7.5478	2.63347	2.32558	1350.9	145220
431	185761	80062991	20.7605	7.5537	2.63448	2.32019	1354.0	145896
432	186624	80621568	20.7846	7.5595	2.63548	2.31481	1357.2	146574
433	187489	81182737	20.8087	7.5654	2.63649	2.30947	1360.3	147254
434	188356	81746504	20.8327	7.5712	2.63749	2.30415	1363.5	147934
435	189225	82312875	20.8567	7.5770	2.63849	2.29885	1366.6	148617
436	190096	82881856	20.8806	7.5828	2.63949	2.29358	1369.7	149301
437	190969	83453453	20.9045	7.5886	2.64048	2.28833	1372.9	149987
438	191844	84027672	20.9284	7.5944	2.64147	2.28311	1376.0	150674
439	192721	84604519	20.9523	7.6001	2.64246	2.27790	1379.2	151363
440	193600	85184000	20.9762	7.6059	2.64345	2.27273	1382.3	152053
441	194481	85766121	21.0000	7.6117	2.64444	2.26757	1385.4	152745
442	195364	86350888	21.0238	7.6174	2.64542	2.26244	1388.6	153439
443	196249	86938307	21.0476	7.6232	2.64640	2.25734	1391.7	154134
444	197136	87528384	21.0713	7.6289	2.64738	2.25225	1394.9	154830
445	198025	88121125	21.0950	7.6346	2.64836	2.24719	1398.0	155528
446	198916	88716536	21.1187	7.6403	2.64933	2.24215	1401.2	156228
447	199809	89314623	21.1424	7.6460	2.65031	2.23714	1404.3	156930
448	200704	89915392	21.1660	7.6517	2.65128	2.23214	1407.4	157633
449	201601	90518849	21.1896	7.6574	2.65225	2.22717	1410.6	158337

Functions of Numbers, 450 to 499

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
450	202500	91125000	21.2132	7.6631	2.65321	2.22222	1413.7	159043
451	203401	91733851	21.2368	7.6688	2.65418	2.21729	1416.9	159751
452	204304	92345408	21.2603	7.6744	2.65514	2.21239	1420.0	160460
453	205209	92959677	21.2838	7.6801	2.65610	2.20751	1423.1	161171
454	206116	93576664	21.3073	7.6857	2.65706	2.20264	1426.3	161883
455	207025	94196375	21.3307	7.6914	2.65801	2.19780	1429.4	162597
456	207936	94818816	21.3542	7.6970	2.65896	2.19298	1432.6	163313
457	208849	95443993	21.3776	7.7026	2.65992	2.18818	1435.7	164030
458	209764	96071912	21.4009	7.7082	2.66087	2.18341	1438.8	164748
459	210681	96702579	21.4243	7.7138	2.66181	2.17865	1442.0	165468
460	211600	97336000	21.4476	7.7194	2.66276	2.17391	1445.1	166190
461	212521	97972181	21.4709	7.7250	2.66370	2.16920	1448.3	166914
462	213444	98611128	21.4942	7.7306	2.66464	2.16450	1451.4	167639
463	214369	99252847	21.5174	7.7362	2.66558	2.15983	1454.6	168365
464	215296	99897344	21.5407	7.7418	2.66652	2.15517	1457.7	169093
465	216225	100546325	21.5639	7.7473	2.66745	2.15054	1460.8	169823
466	217156	101194696	21.5870	7.7529	2.66839	2.14592	1464.0	170554
467	218089	101847563	21.6102	7.7584	2.66932	2.14133	1467.1	171287
468	219024	102503232	21.6333	7.7639	2.67025	2.13675	1470.3	172021
469	219961	103161709	21.6564	7.7695	2.67117	2.13220	1473.4	172757
470	220900	103823000	21.6795	7.7750	2.67210	2.12766	1476.5	173494
471	221841	104487111	21.7025	7.7805	2.67302	2.12314	1479.7	174234
472	222784	105154048	21.7256	7.7860	2.67394	2.11864	1482.8	174974
473	223729	105823817	21.7486	7.7915	2.67486	2.11416	1486.0	175716
474	224676	106496424	21.7715	7.7970	2.67578	2.10970	1489.1	176460
475	225625	107171875	21.7945	7.8025	2.67669	2.10526	1492.3	177205
476	226576	107850176	21.8174	7.8079	2.67761	2.10084	1495.4	177952
477	227529	108531333	21.8403	7.8134	2.67852	2.09644	1498.5	178701
478	228484	109215352	21.8632	7.8188	2.67943	2.09205	1501.7	179451
479	229441	109902239	21.8861	7.8243	2.68034	2.08768	1504.8	180203
480	230400	110592000	21.9089	7.8297	2.68124	2.08333	1508.0	180956
481	231361	111284641	21.9317	7.8352	2.68215	2.07900	1511.1	181711
482	232324	111980168	21.9545	7.8406	2.68305	2.07469	1514.2	182467
483	233289	112678587	21.9773	7.8460	2.68395	2.07039	1517.4	183225
484	234256	113379904	22.0000	7.8514	2.68485	2.06612	1520.5	183984
485	235225	114084125	22.0227	7.8568	2.68574	2.06186	1523.7	184745
486	236196	114791256	22.0454	7.8622	2.68664	2.05761	1526.8	185508
487	237169	115501303	22.0681	7.8676	2.68753	2.05339	1530.0	186272
488	238144	116214272	22.0907	7.8730	2.68842	2.04918	1533.1	187038
489	239121	116930169	22.1133	7.8784	2.68931	2.04499	1536.2	187805
490	240100	117649000	22.1359	7.8837	2.69020	2.04082	1539.4	188574
491	241081	118370771	22.1585	7.8891	2.69108	2.03666	1542.5	189345
492	242064	119095488	22.1811	7.8944	2.69197	2.03252	1545.7	190117
493	243049	119823157	22.2036	7.8998	2.69285	2.02840	1548.8	190890
494	244036	120553784	22.2261	7.9051	2.69373	2.02429	1551.9	191665
495	245025	121287375	22.2486	7.9105	2.69461	2.02020	1555.1	192442
496	246016	122023936	22.2711	7.9158	2.69548	2.01613	1558.2	193221
497	247009	122763473	22.2935	7.9211	2.69636	2.01207	1561.4	194000
498	248004	123505992	22.3159	7.9264	2.69723	2.00803	1564.5	194782
499	249001	124251499	22.3383	7.9317	2.69810	2.00401	1567.7	195565

JONES & LAUGHLIN STEEL COMPANY

Functions of Numbers, 500 to 549

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
500	250000	125000000	22.3607	7.9370	2.69897	2.00000	1570.8	196350
501	251001	125751501	22.3830	7.9423	2.69984	1.99601	1573.9	197136
502	252004	126506008	22.4054	7.9476	2.70070	1.99203	1577.1	197923
503	253009	127263527	22.4277	7.9528	2.70157	1.98807	1580.2	198713
504	254016	128024064	22.4499	7.9581	2.70243	1.98413	1583.4	199504
505	255025	128787625	22.4722	7.9634	2.70329	1.98020	1586.5	200296
506	256036	129554216	22.4944	7.9686	2.70415	1.97628	1589.6	201090
507	257049	130323843	22.5167	7.9739	2.70501	1.97239	1592.8	201886
508	258064	131096512	22.5389	7.9791	2.70586	1.96850	1595.9	202683
509	259081	131872229	22.5610	7.9843	2.70672	1.96464	1599.1	203482
510	260100	132651000	22.5832	7.9896	2.70757	1.96078	1602.2	204282
511	261121	133432831	22.6053	7.9948	2.70842	1.95695	1605.4	205084
512	262144	134217728	22.6274	8.0000	2.70927	1.95312	1608.5	205887
513	263169	135005697	22.6495	8.0052	2.71012	1.94932	1611.6	206692
514	264196	135796744	22.6716	8.0104	2.71096	1.94553	1614.8	207499
515	265225	136590875	22.6936	8.0156	2.71181	1.94175	1617.9	208307
516	266256	137388096	22.7156	8.0208	2.71265	1.93798	1621.1	209117
517	267289	138188413	22.7376	8.0260	2.71349	1.93424	1624.2	209928
518	268324	138991832	22.7596	8.0311	2.71433	1.93050	1627.3	210741
519	269361	139798359	22.7816	8.0363	2.71517	1.92678	1630.5	211556
520	270400	140608000	22.8035	8.0415	2.71600	1.92308	1633.6	212372
521	271441	141420761	22.8254	8.0466	2.71684	1.91939	1636.8	213189
522	272484	142236648	22.8473	8.0517	2.71767	1.91571	1639.9	214008
523	273529	143055667	22.8692	8.0569	2.71850	1.91205	1643.1	214829
524	274576	143877824	22.8910	8.0620	2.71933	1.90840	1646.2	215651
525	275625	144703125	22.9129	8.0671	2.72016	1.90476	1649.3	216475
526	276676	145531576	22.9347	8.0723	2.72099	1.90114	1652.5	217301
527	277729	146363183	22.9565	8.0774	2.72181	1.89753	1655.6	218128
528	278784	147197952	22.9783	8.0825	2.72263	1.89394	1658.8	218956
529	279841	148035889	23.0000	8.0876	2.72346	1.89036	1661.9	219787
530	280900	148877000	23.0217	8.0927	2.72428	1.88679	1665.0	220618
531	281961	149721291	23.0434	8.0978	2.72509	1.88324	1668.2	221452
532	283024	150568768	23.0651	8.1028	2.72591	1.87970	1671.3	222287
533	284089	151419437	23.0868	8.1079	2.72673	1.87617	1674.5	223123
534	285156	152273304	23.1084	8.1130	2.72754	1.87266	1677.6	223961
535	286225	153130375	23.1301	8.1180	2.72835	1.86916	1680.8	224801
536	287296	153990656	23.1517	8.1231	2.72916	1.86567	1683.9	225642
537	288369	154854153	23.1733	8.1281	2.72997	1.86220	1687.0	226484
538	289444	155720872	23.1948	8.1332	2.73078	1.85874	1690.2	227329
539	290521	156590819	23.2164	8.1382	2.73159	1.85529	1693.3	228175
540	291600	157464000	23.2379	8.1433	2.73239	1.85185	1696.5	229022
541	292681	158340421	23.2594	8.1483	2.73320	1.84843	1699.6	229871
542	293764	159220088	23.2809	8.1533	2.73400	1.84502	1702.7	230722
543	294849	160103007	23.3024	8.1583	2.73480	1.84162	1705.9	231574
544	295936	160989184	23.3238	8.1633	2.73560	1.83824	1709.0	232428
545	297025	161878625	23.3452	8.1683	2.73640	1.83486	1712.2	233283
546	298116	162771336	23.3666	8.1733	2.73719	1.83150	1715.3	234140
547	299209	163666723	23.3880	8.1783	2.73799	1.82815	1718.5	234998
548	300304	164565692	23.4094	8.1833	2.73878	1.82482	1721.6	235858
549	301401	165469149	23.4307	8.1882	2.73957	1.82149	1724.7	236720

Functions of Numbers, 550 to 599

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
550	302500	166375000	23.4521	8.1932	2.74036	1.81818	1727.9	237583
551	303601	167284151	23.4734	8.1982	2.74115	1.81488	1731.0	238448
552	304704	168196608	23.4947	8.2031	2.74194	1.81159	1734.2	239314
553	305809	169112377	23.5160	8.2081	2.74273	1.80832	1737.3	240182
554	306916	170031464	23.5372	8.2130	2.74351	1.80505	1740.4	241051
555	308025	170953875	23.5584	8.2180	2.74429	1.80180	1743.6	241922
556	309136	171879616	23.5797	8.2229	2.74507	1.79856	1746.7	242795
557	310249	172808693	23.6008	8.2278	2.74586	1.79533	1749.9	243669
558	311364	173741112	23.6220	8.2327	2.74663	1.79211	1753.0	244545
559	312481	174676879	23.6432	8.2377	2.74741	1.78891	1756.2	245422
560	313600	175616000	23.6643	8.2426	2.74819	1.78571	1759.3	246301
561	314721	176558481	23.6854	8.2475	2.74896	1.78253	1762.4	247181
562	315844	177504328	23.7065	8.2524	2.74974	1.77936	1765.6	248063
563	316969	178453547	23.7276	8.2573	2.75051	1.77620	1768.7	248947
564	318096	179406144	23.7487	8.2621	2.75128	1.77305	1771.9	249832
565	319225	180362125	23.7697	8.2670	2.75205	1.76991	1775.0	250719
566	320356	181321496	23.7908	8.2719	2.75282	1.76678	1778.1	251607
567	321489	182284263	23.8118	8.2768	2.75358	1.76367	1781.3	252497
568	322624	183250432	23.8328	8.2816	2.75435	1.76056	1784.4	253388
569	323761	184220009	23.8537	8.2865	2.75511	1.75747	1787.6	254281
570	324900	185193000	23.8747	8.2913	2.75587	1.75439	1790.7	255176
571	326041	186169411	23.8956	8.2962	2.75664	1.75131	1793.8	256072
572	327184	187149248	23.9165	8.3010	2.75740	1.74825	1797.0	256970
573	328329	188132517	23.9374	8.3059	2.75815	1.74520	1800.1	257869
574	329476	189119224	23.9583	8.3107	2.75891	1.74216	1803.3	258770
575	330625	190109375	23.9792	8.3155	2.75967	1.73913	1806.4	259672
576	331776	191102976	24.0000	8.3203	2.76042	1.73611	1809.6	260576
577	332929	192100033	24.0208	8.3251	2.76118	1.73310	1812.7	261482
578	334084	193100552	24.0416	8.3300	2.76193	1.73010	1815.8	262389
579	335241	194104539	24.0624	8.3348	2.76268	1.72712	1819.0	263298
580	336400	195112000	24.0832	8.3396	2.76343	1.72414	1822.1	264208
581	337561	196122941	24.1039	8.3443	2.76418	1.72117	1825.3	265120
582	338724	197137368	24.1247	8.3491	2.76492	1.71821	1828.4	266033
583	339889	198155287	24.1454	8.3539	2.76567	1.71527	1831.6	266948
584	341056	199176704	24.1661	8.3587	2.76641	1.71233	1834.7	267865
585	342225	200201625	24.1868	8.3634	2.76716	1.70940	1837.8	268783
586	343396	201230056	24.2074	8.3682	2.76790	1.70648	1841.0	269703
587	344569	202262003	24.2281	8.3730	2.76864	1.70358	1844.1	270624
588	345744	203297472	24.2487	8.3777	2.76938	1.70068	1847.3	271547
589	346921	204336469	24.2693	8.3825	2.77012	1.69779	1850.4	272471
590	348100	205379000	24.2899	8.3872	2.77085	1.69492	1853.5	273397
591	349281	206425071	24.3105	8.3919	2.77159	1.69205	1856.7	274325
592	350464	207474688	24.3311	8.3967	2.77232	1.68919	1859.8	275254
593	351649	208527857	24.3516	8.4014	2.77305	1.68634	1863.0	276184
594	352836	209584584	24.3721	8.4061	2.77379	1.68350	1866.1	277117
595	354025	210644875	24.3926	8.4108	2.77452	1.68067	1869.2	278051
596	355216	211708736	24.4131	8.4155	2.77525	1.67785	1872.4	278986
597	356409	212776173	24.4336	8.4202	2.77597	1.67504	1875.5	279923
598	357604	213847192	24.4540	8.4249	2.77670	1.67224	1878.7	280862
599	358801	214921799	24.4745	8.4296	2.77743	1.66945	1881.8	281802

Functions of Numbers, 600 to 649

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = I Circum.
600	360000	216000000	24.4949	8.4343	2.77815	1.66667	1885.0
601	361201	217081801	24.5153	8.4390	2.77887	1.66389	1888.1
602	362404	218167208	24.5357	8.4437	2.77960	1.66113	1891.2
603	363609	219256227	24.5561	8.4484	2.78032	1.65837	1894.4
604	364816	220348864	24.5764	8.4530	2.78104	1.65563	1897.5
605	366025	221445125	24.5967	8.4577	2.78176	1.65289	1900.7
606	367236	222545016	24.6171	8.4623	2.78247	1.65017	1903.8
607	368449	223648543	24.6374	8.4670	2.78319	1.64745	1906.9
608	369664	224755712	24.6577	8.4716	2.78390	1.64474	1910.1
609	370881	225866529	24.6779	8.4763	2.78462	1.64204	1913.2
610	372100	226981000	24.6982	8.4809	2.78533	1.63934	1916.4
611	373321	228099131	24.7184	8.4856	2.78604	1.63666	1919.5
612	374544	229220928	24.7386	8.4902	2.78675	1.63399	1922.7
613	375769	230346397	24.7588	8.4948	2.78746	1.63132	1925.8
614	376996	231475544	24.7790	8.4994	2.78817	1.62866	1928.9
615	378225	232608375	24.7992	8.5040	2.78888	1.62602	1932.1
616	379456	233744896	24.8193	8.5086	2.78958	1.62338	1935.2
617	380689	234885113	24.8395	8.5132	2.79029	1.62075	1938.4
618	381924	236029032	24.8596	8.5178	2.79099	1.61812	1941.5
619	383161	237176659	24.8797	8.5224	2.79169	1.61551	1944.6
620	384400	238328000	24.8998	8.5270	2.79239	1.61290	1947.8
621	385641	239483061	24.9199	8.5316	2.79309	1.61031	1950.9
622	386884	240641848	24.9399	8.5362	2.79379	1.60772	1954.1
623	388129	241804367	24.9600	8.5408	2.79449	1.60514	1957.2
624	389376	242970624	24.9800	8.5453	2.79518	1.60256	1960.4
625	390625	244140625	25.0000	8.5499	2.79588	1.60000	1963.5
626	391876	245314376	25.0200	8.5544	2.79657	1.59744	1966.6
627	393129	246491883	25.0400	8.5590	2.79727	1.59490	1969.8
628	394384	247673152	25.0599	8.5635	2.79796	1.59236	1972.9
629	395641	248858189	25.0799	8.5681	2.79865	1.58983	1976.1
630	396900	250047000	25.0998	8.5726	2.79934	1.58730	1979.2
631	398161	251239591	25.1197	8.5772	2.80003	1.58479	1982.3
632	399424	252435968	25.1396	8.5817	2.80072	1.58228	1985.5
633	400689	253636137	25.1595	8.5862	2.80140	1.57978	1988.6
634	401956	254840104	25.1794	8.5907	2.80209	1.57729	1991.8
635	403225	256047875	25.1992	8.5952	2.80277	1.57480	1994.9
636	404496	257259456	25.2190	8.5997	2.80346	1.57233	1998.1
637	405769	258474853	25.2389	8.6043	2.80414	1.56986	2001.2
638	407044	259694072	25.2587	8.6088	2.80482	1.56740	2004.3
639	408321	260917119	25.2784	8.6132	2.80550	1.56495	2007.5
640	409600	262144000	25.2982	8.6177	2.80618	1.56250	2010.6
641	410881	263374721	25.3180	8.6222	2.80686	1.56006	2013.8
642	412164	264609288	25.3377	8.6267	2.80754	1.55763	2016.9
643	413449	265847707	25.3574	8.6312	2.80821	1.55521	2020.0
644	414736	267089984	25.3772	8.6357	2.80889	1.55280	2023.2
645	416025	268336125	25.3969	8.6401	2.80956	1.55039	2026.3
646	417316	269586136	25.4165	8.6446	2.81023	1.54799	2029.5
647	418609	270840023	25.4362	8.6490	2.81090	1.54560	2032.6
648	419904	272097792	25.4558	8.6535	2.81158	1.54321	2035.8
649	421201	273359449	25.4755	8.6579	2.81224	1.54083	2038.9

Functions of Numbers, 650 to 699

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
650	422500	274625000	25.4951	8.6624	2.81291	1.53846	2042.0	331831
651	423801	275894451	25.5147	8.6668	2.81358	1.53610	2045.2	332853
652	425104	277167808	25.5343	8.6713	2.81425	1.53374	2048.3	333876
653	426409	278445077	25.5539	8.6757	2.81491	1.53139	2051.5	334901
654	427716	279726264	25.5734	8.6801	2.81558	1.52905	2054.6	335927
655	429025	281011375	25.5930	8.6845	2.81624	1.52672	2057.7	336955
656	430336	282300416	25.6125	8.6890	2.81690	1.52439	2060.9	337985
657	431649	283593393	25.6320	8.6934	2.81757	1.52207	2064.0	339016
658	432964	284890312	25.6515	8.6978	2.81823	1.51976	2067.2	340049
659	434281	286191179	25.6710	8.7022	2.81889	1.51745	2070.3	341084
660	435600	287496000	25.6905	8.7066	2.81954	1.51515	2073.5	342119
661	436921	288804781	25.7099	8.7110	2.82020	1.51286	2076.6	343157
662	438244	290117528	25.7294	8.7154	2.82086	1.51057	2079.7	344196
663	439569	291434247	25.7488	8.7198	2.82151	1.50830	2082.9	345237
664	440896	292754944	25.7682	8.7241	2.82217	1.50602	2086.0	346279
665	442225	294079625	25.7876	8.7285	2.82282	1.50376	2089.2	347323
666	443556	295408296	25.8070	8.7329	2.82347	1.50150	2092.3	348368
667	444889	296740963	25.8263	8.7373	2.82413	1.49925	2095.4	349415
668	446224	298077632	25.8457	8.7416	2.82478	1.49701	2098.6	350464
669	447561	299418309	25.8650	8.7460	2.82543	1.49477	2101.7	351514
670	448900	300763000	25.8844	8.7503	2.82607	1.49254	2104.9	352565
671	450241	302111711	25.9037	8.7547	2.82672	1.49031	2108.0	353618
672	451584	303464448	25.9230	8.7590	2.82737	1.48810	2111.2	354673
673	452929	304821217	25.9422	8.7634	2.82802	1.48588	2114.3	355730
674	454276	306182024	25.9615	8.7677	2.82866	1.48368	2117.4	356788
675	455625	307546875	25.9808	8.7721	2.82930	1.48148	2120.6	357847
676	456976	308915776	26.0000	8.7764	2.82995	1.47929	2123.7	358908
677	458329	310288733	26.0192	8.7807	2.83059	1.47710	2126.9	359971
678	459684	311665752	26.0384	8.7850	2.83123	1.47493	2130.0	361035
679	461041	313046839	26.0576	8.7893	2.83187	1.47275	2133.1	362101
680	462400	314432000	26.0768	8.7937	2.83251	1.47059	2136.3	363168
681	463761	315821241	26.0960	8.7980	2.83315	1.46843	2139.4	364237
682	465124	317214568	26.1151	8.8023	2.83378	1.46628	2142.6	365308
683	466489	318611987	26.1342	8.8066	2.83442	1.46413	2145.7	366380
684	467856	320013504	26.1534	8.8109	2.83506	1.46199	2148.8	367453
685	469225	321419125	26.1725	8.8152	2.83569	1.45985	2152.0	368528
686	470596	322828856	26.1916	8.8194	2.83632	1.45773	2155.1	369605
687	471969	324242703	26.2107	8.8237	2.83696	1.45560	2158.3	370684
688	473344	325660672	26.2298	8.8280	2.83759	1.45349	2161.4	371764
689	474721	327082769	26.2488	8.8323	2.83822	1.45138	2164.6	372845
690	476100	328509000	26.2679	8.8366	2.83885	1.44928	2167.7	373928
691	477481	329939371	26.2869	8.8408	2.83948	1.44718	2170.8	375013
692	478864	331373888	26.3059	8.8451	2.84011	1.44509	2174.0	376099
693	480249	332812557	26.3249	8.8493	2.84073	1.44300	2177.1	377187
694	481636	334255384	26.3439	8.8536	2.84136	1.44092	2180.3	378276
695	483025	335702375	26.3629	8.8578	2.84198	1.43885	2183.4	379367
696	484416	337153536	26.3818	8.8621	2.84261	1.43678	2186.5	380459
697	485809	338608873	26.4008	8.8663	2.84323	1.43472	2189.7	381553
698	487204	340068392	26.4197	8.8706	2.84386	1.43266	2192.8	382649
699	488601	341532099	26.4386	8.8748	2.84448	1.43062	2196.0	383746

JONES & LAUGHLIN STEEL COMPANY

Functions of Numbers, 700 to 749

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
700	490000	343000000	26.4575	8.8790	2.84510	1.42857	2199.1	384845
701	491401	344472101	26.4764	8.8833	2.84572	1.42653	2202.3	385945
702	492804	345948408	26.4953	8.8875	2.84634	1.42450	2205.4	387047
703	494209	347428927	26.5141	8.8917	2.84696	1.42248	2208.5	388151
704	495616	348913664	26.5330	8.8959	2.84757	1.42045	2211.7	389256
705	497025	350402625	26.5518	8.9001	2.84819	1.41844	2214.8	390363
706	498436	351895816	26.5707	8.9043	2.84880	1.41643	2218.0	391471
707	499849	353393243	26.5895	8.9085	2.84942	1.41443	2221.1	392580
708	501264	354894912	26.6083	8.9127	2.85003	1.41243	2224.2	393692
709	502681	356400829	26.6271	8.9169	2.85065	1.41044	2227.4	394805
710	504100	357911000	26.6458	8.9211	2.85126	1.40845	2230.5	395919
711	505521	359425431	26.6646	8.9253	2.85187	1.40647	2233.7	397035
712	506944	360944128	26.6833	8.9295	2.85248	1.40449	2236.8	398153
713	508369	362467097	26.7021	8.9337	2.85309	1.40252	2240.0	399273
714	509796	363994344	26.7208	8.9378	2.85370	1.40056	2243.1	400393
715	511225	365525875	26.7395	8.9420	2.85431	1.39860	2246.2	401515
716	512656	367061696	26.7582	8.9462	2.85491	1.39665	2249.4	402639
717	514089	368601813	26.7769	8.9503	2.85552	1.39470	2252.5	403765
718	515524	370146232	26.7955	8.9545	2.85612	1.39276	2255.7	404892
719	516961	371694959	26.8142	8.9587	2.85673	1.39082	2258.8	406020
720	518400	373248000	26.8328	8.9628	2.85733	1.38889	2261.9	407150
721	519841	374805361	26.8514	8.9670	2.85794	1.38696	2265.1	408282
722	521284	376367048	26.8701	8.9711	2.85854	1.38504	2268.2	409415
723	522729	377933067	26.8887	8.9752	2.85914	1.38313	2271.4	410550
724	524176	379503424	26.9072	8.9794	2.85974	1.38122	2274.5	411687
725	525625	381078125	26.9258	8.9835	2.86034	1.37931	2277.7	412825
726	527076	382657176	26.9444	8.9876	2.86094	1.37741	2280.8	413965
727	528529	384240583	26.9629	8.9918	2.86153	1.37552	2283.9	415106
728	529984	385828352	26.9815	8.9959	2.86213	1.37363	2287.1	416248
729	531441	387420489	27.0000	9.0000	2.86273	1.37174	2290.2	417393
730	532900	389017000	27.0185	9.0041	2.86332	1.36986	2293.4	418539
731	534361	390617891	27.0370	9.0082	2.86392	1.36799	2296.5	419686
732	535824	392223168	27.0555	9.0123	2.86451	1.36612	2299.6	420835
733	537289	393833837	27.0740	9.0164	2.86510	1.36426	2302.8	421986
734	538756	395446904	27.0924	9.0205	2.86570	1.36240	2305.9	423138
735	540225	397063375	27.1109	9.0246	2.86629	1.36054	2309.1	424293
736	541696	398688256	27.1293	9.0287	2.86688	1.35870	2312.2	425447
737	543169	400315553	27.1477	9.0328	2.86747	1.35685	2315.4	426604
738	544644	401947272	27.1662	9.0369	2.86806	1.35501	2318.5	427762
739	546121	403583419	27.1846	9.0410	2.86864	1.35318	2321.6	428922
740	547600	405224000	27.2029	9.0450	2.86923	1.35135	2324.8	430084
741	549081	406869021	27.2213	9.0491	2.86982	1.34953	2327.9	431247
742	550564	408518488	27.2397	9.0532	2.87040	1.34771	2331.1	432412
743	552049	410172407	27.2580	9.0572	2.87099	1.34590	2334.2	433578
744	553536	411830784	27.2764	9.0613	2.87157	1.34409	2337.3	434746
745	555025	413493625	27.2947	9.0654	2.87216	1.34228	2340.5	435916
746	556516	415160936	27.3130	9.0694	2.87274	1.34048	2343.6	437087
747	558009	416832723	27.3313	9.0735	2.87332	1.33869	2346.8	438259
748	559504	418508992	27.3496	9.0775	2.87390	1.33690	2349.9	439433
749	561001	420189749	27.3679	9.0816	2.87448	1.33511	2353.1	440609

JONES & LAUGHLIN STEEL COMPANY

Functions of Numbers, 750 to 799

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
750	562500	421875000	27.3861	9.0856	2.87506	1.33333	2356.2	441786
751	564001	423564751	27.4044	9.0896	2.87564	1.33156	2359.3	442965
752	565504	425259008	27.4226	9.0937	2.87622	1.32979	2362.5	444146
753	567009	426957777	27.4408	9.0977	2.87680	1.32802	2365.6	445328
754	568516	428661064	27.4591	9.1017	2.87737	1.32626	2368.8	446511
755	570025	430368875	27.4773	9.1057	2.87795	1.32450	2371.9	447697
756	571536	432081216	27.4955	9.1098	2.87852	1.32275	2375.0	448883
757	573049	433798093	27.5136	9.1138	2.87910	1.32100	2378.2	450072
758	574564	435519512	27.5318	9.1178	2.87967	1.31926	2381.3	451262
759	576081	437245479	27.5500	9.1218	2.88024	1.31752	2384.5	452453
760	577600	438976000	27.5681	9.1258	2.88081	1.31579	2387.6	453646
761	579121	440711081	27.5862	9.1298	2.88138	1.31406	2390.8	454841
762	580644	442456072	27.6043	9.1338	2.88196	1.31234	2393.9	456037
763	582169	444194947	27.6225	9.1378	2.88252	1.31062	2397.0	457234
764	583696	445943744	27.6405	9.1418	2.88309	1.30890	2400.2	458434
765	585225	447697125	27.6586	9.1458	2.88366	1.30719	2403.3	459635
766	586756	449455096	27.6767	9.1498	2.88423	1.30548	2406.5	460837
767	588289	451217663	27.6948	9.1537	2.88480	1.30378	2409.6	462041
768	589824	452984832	27.7128	9.1577	2.88536	1.30208	2412.7	463247
769	591361	454756609	27.7308	9.1617	2.88593	1.30039	2415.9	464454
770	592900	456533000	27.7489	9.1657	2.88649	1.29870	2419.0	465663
771	594441	458314011	27.7669	9.1696	2.88705	1.29702	2422.2	466873
772	595984	460099648	27.7849	9.1736	2.88762	1.29534	2425.3	468085
773	597529	461889917	27.8029	9.1775	2.88818	1.29366	2428.5	469298
774	599076	463684824	27.8209	9.1815	2.88874	1.29199	2431.6	470513
775	600625	465484375	27.8388	9.1855	2.88930	1.29032	2434.7	471730
776	602176	467288576	27.8568	9.1894	2.88986	1.28866	2437.9	472948
777	603729	469097433	27.8747	9.1933	2.89042	1.28700	2441.0	474168
778	605284	470910952	27.8927	9.1973	2.89098	1.28535	2444.2	475389
779	606841	472729139	27.9106	9.2012	2.89154	1.28370	2447.3	476612
780	608400	474552000	27.9285	9.2052	2.89209	1.28205	2450.4	477836
781	609961	476379541	27.9464	9.2091	2.89265	1.28041	2453.6	479062
782	611524	478211768	27.9643	9.2130	2.89321	1.27877	2456.7	480290
783	613089	480048687	27.9821	9.2170	2.89376	1.27714	2459.9	481519
784	614656	481890304	28.0000	9.2209	2.89432	1.27551	2463.0	482750
785	616225	483736625	28.0179	9.2248	2.89487	1.27389	2466.2	483982
786	617796	485587656	28.0357	9.2287	2.89542	1.27226	2469.3	485216
787	619369	487443403	28.0535	9.2326	2.89597	1.27065	2472.4	486451
788	620944	489303872	28.0713	9.2365	2.89653	1.26904	2475.6	487688
789	622521	491169069	28.0891	9.2404	2.89708	1.26743	2478.7	488927
790	624100	493039000	28.1069	9.2443	2.89763	1.26582	2481.9	490167
791	625681	494913671	28.1247	9.2482	2.89818	1.26422	2485.0	491409
792	627264	496793088	28.1425	9.2521	2.89873	1.26263	2488.1	492652
793	628849	498677257	28.1603	9.2560	2.89927	1.26103	2491.3	493897
794	630436	500566184	28.1780	9.2599	2.89982	1.25944	2494.4	495143
795	632025	502459875	28.1957	9.2638	2.90037	1.25786	2497.6	496391
796	633616	504358336	28.2135	9.2677	2.90091	1.25628	2500.7	497641
797	635209	506261573	28.2312	9.2716	2.90146	1.25471	2503.8	498892
798	636804	508169592	28.2489	9.2754	2.90200	1.25313	2507.0	500145
799	638401	510082399	28.2666	9.2793	2.90255	1.25156	2510.1	501399

JONES & LAUGHLIN STEEL COMPANY

Functions of Numbers, 800 to 849

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
800	640000	512000000	28.2843	9.2832	2.90309	1.25000	2513.3	5026
801	641601	513922401	28.3019	9.2870	2.90363	1.24844	2516.4	5039
802	643204	515849608	28.3196	9.2909	2.90417	1.24688	2519.6	5051
803	644809	517781627	28.3373	9.2948	2.90472	1.24533	2522.7	5064
804	646416	519718464	28.3549	9.2986	2.90526	1.24378	2525.8	5076
805	648205	521660125	28.3725	9.3025	2.90580	1.24224	2529.0	5089
806	649636	523606616	28.3901	9.3063	2.90634	1.24069	2532.1	5102
807	651249	525557943	28.4077	9.3102	2.90687	1.23916	2535.3	5114
808	652864	527514112	28.4253	9.3140	2.90741	1.23762	2538.4	5127
809	654481	529475129	28.4429	9.3179	2.90795	1.23609	2541.5	5140
810	656100	531441000	28.4605	9.3217	2.90849	1.23457	2544.7	5153
811	657721	533411731	28.4781	9.3255	2.90902	1.23305	2547.8	5165
812	659344	535387328	28.4956	9.3294	2.90956	1.23153	2551.0	5178
813	660969	537367797	28.5132	9.3332	2.91009	1.23001	2554.1	5191
814	662596	539353144	28.5307	9.3370	2.91062	1.22850	2557.3	5204
815	664225	541343375	28.5482	9.3408	2.91116	1.22699	2560.4	5216
816	665856	543338496	28.5657	9.3447	2.91169	1.22549	2563.5	5229
817	667489	545338513	28.5832	9.3485	2.91222	1.22399	2566.7	5242
818	669124	547343432	28.6007	9.3523	2.91275	1.22249	2569.8	5255
819	670761	549353259	28.6182	9.3561	2.91328	1.22100	2573.0	5268
820	672400	551368000	28.6356	9.3599	2.91381	1.21951	2576.1	5281
821	674041	553387661	28.6531	9.3637	2.91434	1.21803	2579.2	5293
822	675684	555412248	28.6705	9.3675	2.91487	1.21655	2582.4	5306
823	677329	557441767	28.6880	9.3713	2.91540	1.21507	2585.5	5319
824	678976	559476224	28.7054	9.3751	2.91593	1.21359	2588.7	5332
825	680625	561515625	28.7228	9.3789	2.91645	1.21212	2591.8	5345
826	682276	563559976	28.7402	9.3827	2.91698	1.21065	2595.0	5358
827	683929	565609283	28.7576	9.3865	2.91751	1.20919	2598.1	5371
828	685584	567663552	28.7750	9.3902	2.91803	1.20773	2601.2	5384
829	687241	569722789	28.7924	9.3940	2.91855	1.20627	2604.4	5397
830	688900	571787000	28.8097	9.3978	2.91908	1.20482	2607.5	5410
831	690561	573856191	28.8271	9.4016	2.91960	1.20337	2610.7	5423
832	692224	575930368	28.8444	9.4053	2.92012	1.20192	2613.8	5436
833	693889	578009537	28.8617	9.4091	2.92065	1.20048	2616.9	5449
834	695556	580093704	28.8791	9.4129	2.92117	1.19904	2620.1	5462
835	697225	582182875	28.8964	9.4166	2.92169	1.19760	2623.2	5475
836	698896	584277056	28.9137	9.4204	2.92221	1.19617	2626.4	5488
837	700569	586376253	28.9310	9.4241	2.92273	1.19474	2629.5	5502
838	702244	588480472	28.9482	9.4279	2.92324	1.19332	2632.7	5515
839	703921	590589719	28.9655	9.4316	2.92376	1.19190	2635.8	5528
840	705600	592704000	28.9828	9.4354	2.92428	1.19048	2638.9	5541
841	707281	594823321	29.0000	9.4391	2.92480	1.18906	2642.1	5554
842	708964	596947688	29.0172	9.4429	2.92531	1.18765	2645.2	5568
843	710649	599077107	29.0345	9.4466	2.92583	1.18624	2648.4	5581
844	712336	601211584	29.0517	9.4503	2.92634	1.18483	2651.5	5594
845	714025	603351125	29.0689	9.4541	2.92686	1.18343	2654.6	5607
846	715716	605495736	29.0861	9.4578	2.92737	1.18203	2657.8	5621
847	717409	607645423	29.1033	9.4615	2.92788	1.18064	2660.9	5634
848	719104	609800192	29.1204	9.4652	2.92840	1.17925	2664.1	5647
849	720801	611960049	29.1376	9.4690	2.92891	1.17786	2667.2	5661

Functions of Numbers, 850 to 899

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No.—Diameter	
							Circum.	Area
850	722500	614125000	29.1548	9.4727	2.92942	1.17647	2670.4	567450
851	724201	616295051	29.1719	9.4764	2.92993	1.17509	2673.5	568786
852	725904	618470208	29.1890	9.4801	2.93044	1.17371	2676.6	570124
853	727609	620650477	29.2062	9.4838	2.93095	1.17233	2679.8	571463
854	729316	622835864	29.2233	9.4875	2.93146	1.17096	2682.9	572803
855	731025	625026375	29.2404	9.4912	2.93197	1.16959	2686.1	574146
856	732736	627222016	29.2575	9.4949	2.93247	1.16822	2689.2	575490
857	734449	629422793	29.2746	9.4986	2.93298	1.16686	2692.3	576835
858	736164	631628712	29.2916	9.5023	2.93349	1.16550	2695.5	578182
859	737881	633839779	29.3087	9.5060	2.93399	1.16414	2698.6	579530
860	739600	636056000	29.3258	9.5097	2.93450	1.16279	2701.8	580880
861	741321	638277381	29.3428	9.5134	2.93500	1.16144	2704.9	582232
862	743044	640503928	29.3598	9.5171	2.93551	1.16009	2708.1	583585
863	744769	642735647	29.3769	9.5207	2.93601	1.15875	2711.2	584940
864	746496	644972544	29.3939	9.5244	2.93651	1.15741	2714.3	586297
865	748225	647214625	29.4109	9.5281	2.93702	1.15607	2717.5	587655
866	749956	649461896	29.4279	9.5317	2.93752	1.15473	2720.6	589014
867	751689	651714363	29.4449	9.5354	2.93802	1.15340	2723.8	590375
868	753424	653972032	29.4618	9.5391	2.93852	1.15207	2726.9	591738
869	755161	656234909	29.4788	9.5427	2.93902	1.15075	2730.0	593102
870	756900	658503000	29.4958	9.5464	2.93952	1.14943	2733.2	594468
871	758641	660776311	29.5127	9.5501	2.94002	1.14811	2736.3	595835
872	760384	663054848	29.5296	9.5537	2.94052	1.14679	2739.5	597204
873	762129	665338617	29.5466	9.5574	2.94101	1.14548	2742.6	598575
874	763876	667627624	29.5635	9.5610	2.94151	1.14416	2745.8	599947
875	765625	669921875	29.5804	9.5647	2.94201	1.14286	2748.9	601320
876	767376	672221376	29.5973	9.5683	2.94250	1.14155	2752.0	602696
877	769129	674526133	29.6142	9.5719	2.94300	1.14025	2755.2	604073
878	770884	676836152	29.6311	9.5756	2.94349	1.13895	2758.3	605451
879	772641	679151439	29.6479	9.5792	2.94399	1.13766	2761.5	606831
880	774400	681472000	29.6648	9.5828	2.94448	1.13636	2764.6	608212
881	776161	683797841	29.6816	9.5865	2.94498	1.13507	2767.7	609595
882	777924	686128968	29.6985	9.5901	2.94547	1.13379	2770.9	610980
883	779689	688465387	29.7153	9.5937	2.94596	1.13250	2774.0	612366
884	781456	690807104	29.7321	9.5973	2.94645	1.13122	2777.2	613754
885	783225	693154125	29.7489	9.6010	2.94694	1.12994	2780.3	615143
886	784996	695506456	29.7658	9.6046	2.94743	1.12867	2783.5	616534
887	786769	697864103	29.7825	9.6082	2.94792	1.12740	2786.6	617927
888	788544	700227072	29.7993	9.6118	2.94841	1.12613	2789.7	619321
889	790321	702595369	29.8161	9.6154	2.94890	1.12486	2792.9	620717
890	792100	704969000	29.8329	9.6190	2.94939	1.12360	2796.0	622114
891	793881	707347971	29.8496	9.6226	2.94988	1.12233	2799.2	623513
892	795664	709732288	29.8664	9.6262	2.95036	1.12108	2802.3	624913
893	797449	712121957	29.8831	9.6298	2.95085	1.11982	2805.4	626315
894	799236	714516984	29.8998	9.6334	2.95134	1.11857	2808.6	627718
895	801025	716917375	29.9166	9.6370	2.95182	1.11732	2811.7	629124
896	802816	719323136	29.9333	9.6406	2.95231	1.11607	2814.9	630530
897	804609	721734273	29.9500	9.6442	2.95279	1.11483	2818.0	631938
898	806404	724150792	29.9666	9.6477	2.95328	1.11359	2821.2	633348
899	808201	726572699	29.9833	9.6513	2.95376	1.11235	2824.3	634760

JONES & LAUGHLIN STEEL COMPANY

Functions of Numbers, 900 to 949

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
900	810000	729000000	30.0000	9.6549	2.95424	1.11111	2827.4	636173
901	811801	731432701	30.0167	9.6585	2.95472	1.10988	2830.6	637587
902	813604	733870808	30.0333	9.6620	2.95521	1.10865	2833.7	639003
903	815409	736314327	30.0500	9.6656	2.95569	1.10742	2836.9	640421
904	817216	738763264	30.0666	9.6692	2.95617	1.10619	2840.0	641840
905	819025	741217625	30.0832	9.6727	2.95665	1.10497	2843.1	643261
906	820836	743677416	30.0998	9.6763	2.95713	1.10375	2846.3	644683
907	822649	746142649	30.1164	9.6799	2.95761	1.10254	2849.4	646107
908	824464	748613312	30.1330	9.6834	2.95809	1.10132	2852.6	647533
909	826281	751089429	30.1496	9.6870	2.95856	1.10011	2855.7	648960
910	828100	753571000	30.1662	9.6905	2.95904	1.09890	2858.8	650388
911	829921	756058031	30.1828	9.6941	2.95952	1.09769	2862.0	651818
912	831744	758550528	30.1993	9.6976	2.95999	1.09649	2865.1	653250
913	833569	761048497	30.2159	9.7012	2.96047	1.09529	2868.3	654684
914	835396	763551944	30.2324	9.7047	2.96095	1.09409	2871.4	656118
915	837225	766060875	30.2490	9.7082	2.96142	1.09290	2874.6	657555
916	839056	768575296	30.2655	9.7118	2.96190	1.09170	2877.7	658993
917	840889	771095313	30.2820	9.7153	2.96237	1.09051	2880.8	660433
918	842724	773620632	30.2985	9.7188	2.96284	1.08932	2884.0	661874
919	844561	776151559	30.3150	9.7224	2.96332	1.08814	2887.1	663317
920	846400	778688000	30.3315	9.7259	2.96379	1.08696	2890.3	664761
921	848241	781229961	30.3480	9.7294	2.96426	1.08578	2893.4	666207
922	850084	783777448	30.3645	9.7329	2.96473	1.08460	2896.5	667654
923	851929	786330467	30.3809	9.7364	2.96520	1.08342	2899.7	669103
924	853776	788889024	30.3974	9.7400	2.96567	1.08225	2902.8	670554
925	855625	791453125	30.4138	9.7435	2.96614	1.08108	2906.0	672006
926	857476	794022776	30.4302	9.7470	2.96661	1.07991	2909.1	673460
927	859329	796597983	30.4467	9.7505	2.96708	1.07875	2912.3	674915
928	861184	799178752	30.4631	9.7540	2.96755	1.07759	2915.4	676372
929	863041	801765089	30.4795	9.7575	2.96802	1.07643	2918.5	677831
930	864900	804357000	30.4959	9.7610	2.96848	1.07527	2921.7	679291
931	866761	806954491	30.5123	9.7645	2.96895	1.07411	2924.8	680752
932	868624	809557568	30.5287	9.7680	2.96942	1.07296	2928.0	682216
933	870489	812166237	30.5450	9.7715	2.96988	1.07181	2931.1	683680
934	872356	814780504	30.5614	9.7750	2.97035	1.07066	2934.2	685147
935	874225	817400375	30.5778	9.7785	2.97081	1.06952	2937.4	686615
936	876096	820025856	30.5941	9.7819	2.97128	1.06838	2940.5	688084
937	877969	822656953	30.6105	9.7854	2.97174	1.06724	2943.7	689555
938	879844	825293672	30.6268	9.7889	2.97220	1.06610	2946.8	691028
939	881721	827936019	30.6431	9.7924	2.97267	1.06496	2950.0	692502
940	883600	830584000	30.6594	9.7959	2.97313	1.06383	2953.1	693978
941	885481	833237621	30.6757	9.7993	2.97359	1.06270	2956.2	695455
942	887364	835896888	30.6920	9.8028	2.97405	1.06157	2959.4	696934
943	889249	838561807	30.7083	9.8063	2.97451	1.06045	2962.5	698415
944	891136	841232384	30.7246	9.8097	2.97497	1.05932	2965.7	699897
945	893025	843908625	30.7409	9.8132	2.97543	1.05820	2968.8	701380
946	894916	846590536	30.7571	9.8167	2.97589	1.05708	2971.9	702865
947	896809	849278123	30.7734	9.8201	2.97635	1.05597	2975.1	704352
948	898704	851971392	30.7896	9.8236	2.97681	1.05485	2978.2	705840
949	900601	854670349	30.8058	9.8270	2.97727	1.05374	2981.4	707330

Functions of Numbers, 950 to 999

No.	Square	Cube	Square Root	Cube Root	Logarithm	1000 x Reciprocal	No. = Diameter	
							Circum.	Area
950	902500	857375000	30.8221	9.8305	2.97772	1.05263	2984.5	708822
951	904401	860085351	30.8383	9.8339	2.97818	1.05152	2987.7	710315
952	906304	862801408	30.8545	9.8374	2.97864	1.05042	2990.8	711809
953	908209	865523177	30.8707	9.8408	2.97909	1.04932	2993.9	713306
954	910116	868250664	30.8869	9.8443	2.97955	1.04822	2997.1	714803
955	912025	870983875	30.9031	9.8477	2.98000	1.04712	3000.2	716303
956	913936	873722816	30.9192	9.8511	2.98046	1.04603	3003.4	717804
957	915849	876467493	30.9354	9.8546	2.98091	1.04493	3006.5	719306
958	917764	879217912	30.9516	9.8580	2.98137	1.04384	3009.6	720810
959	919681	881974079	30.9677	9.8614	2.98182	1.04275	3012.8	722316
960	921600	884736000	30.9839	9.8648	2.98227	1.04167	3015.9	723823
961	923521	887503681	31.0000	9.8683	2.98272	1.04058	3019.1	725332
962	925444	890277128	31.0161	9.8717	2.98318	1.03950	3022.2	726842
963	927369	893056347	31.0322	9.8751	2.98363	1.03842	3025.4	728354
964	929296	895841344	31.0483	9.8785	2.98408	1.03734	3028.5	729867
965	931225	898632125	31.0644	9.8819	2.98453	1.03627	3031.6	731382
966	933156	901428696	31.0805	9.8854	2.98498	1.03520	3034.8	732899
967	935089	904231063	31.0966	9.8888	2.98543	1.03413	3037.9	734417
968	937024	907039232	31.1127	9.8922	2.98588	1.03306	3041.1	735937
969	938961	909853209	31.1288	9.8956	2.98632	1.03199	3044.2	737458
970	940900	912673000	31.1448	9.8990	2.98677	1.03093	3047.3	738981
971	942841	915498611	31.1609	9.9024	2.98722	1.02987	3050.5	740506
972	944784	918330048	31.1769	9.9058	2.98767	1.02881	3053.6	742032
973	946729	921167317	31.1929	9.9092	2.98811	1.02775	3056.8	743559
974	948676	924010424	31.2090	9.9126	2.98856	1.02669	3059.9	745088
975	950625	926859375	31.2250	9.9160	2.98900	1.02564	3063.1	746619
976	952576	929714176	31.2410	9.9194	2.98945	1.02459	3066.2	748151
977	954529	932574833	31.2570	9.9227	2.98989	1.02354	3069.3	749685
978	956484	935441352	31.2730	9.9261	2.99034	1.02249	3072.5	751221
979	958441	938313739	31.2890	9.9295	2.99078	1.02145	3075.6	752758
980	960400	941192000	31.3050	9.9329	2.99123	1.02041	3078.8	754296
981	962361	944076141	31.3209	9.9363	2.99167	1.01937	3081.9	755837
982	964324	946966168	31.3369	9.9396	2.99211	1.01833	3085.0	757378
983	966289	949862087	31.3528	9.9430	2.99255	1.01729	3088.2	758922
984	968256	952763904	31.3688	9.9464	2.99300	1.01626	3091.3	760466
985	970225	955671625	31.3847	9.9497	2.99344	1.01523	3094.5	762013
986	972196	958585256	31.4006	9.9531	2.99388	1.01420	3097.6	763561
987	974169	961504803	31.4166	9.9565	2.99432	1.01317	3100.8	765111
988	976144	964430272	31.4325	9.9598	2.99476	1.01215	3103.9	766662
989	978121	967361669	31.4484	9.9632	2.99520	1.01112	3107.0	768214
990	980100	970299000	31.4643	9.9666	2.99564	1.01010	3110.2	769769
991	982081	973242271	31.4802	9.9699	2.99607	1.00908	3113.3	771325
992	984064	976191488	31.4960	9.9733	2.99651	1.00806	3116.5	772882
993	986049	979146657	31.5119	9.9766	2.99695	1.00705	3119.6	774441
994	988036	982107784	31.5278	9.9800	2.99739	1.00604	3122.7	776002
995	990025	985074875	31.5436	9.9833	2.99782	1.00503	3125.9	777564
996	992016	988047936	31.5595	9.9866	2.99826	1.00402	3129.0	779128
997	994009	991026973	31.5753	9.9900	2.99870	1.00301	3132.2	780693
998	996004	994011992	31.5911	9.9933	2.99913	1.00200	3135.3	782260
999	998001	997002999	31.6070	9.9967	2.99957	1.00100	3138.5	783828

AMERICAN SOCIETY FOR TESTING MATERIALS
PHILADELPHIA, PA., U. S. A.

AFFILIATED WITH THE
INTERNATIONAL ASSOCIATION FOR TESTING MATERIALS

Standard Specifications for
Structural Steel for Buildings
Serial Designation: A9-14

Adopted, 1901; Revised, 1909, 1913, 1914

I. MANUFACTURE

1. PROCESS—(a) Structural steel, except as noted in Paragraph (b), may be made by the Bessemer or the open-hearth process.

(b) Rivet steel, and steel for plates or angles over $\frac{3}{4}$ inch in thickness which are to be punched, shall be made by the open-hearth process.

II. CHEMICAL PROPERTIES AND TESTS

2. CHEMICAL COMPOSITION—The steel shall conform to the following requirements as to chemical composition:

	STRUCTURAL STEEL	RIVET STEEL
Phosphorus	(Bessemer.....not over 0.10 per cent.
	(Open-hearth.....not over 0.06 per cent.	not over 0.06 per cent.
Sulphur.....	not over 0.045 per cent.	

3. LADLE ANALYSES—An analysis to determine the percentages of carbon, manganese, phosphorus and sulphur shall be made by the manufacturer from a test ingot taken during the pouring of each melt, a copy of which shall be given to the purchaser or his representative. This analysis shall conform to the requirements specified in Section 2.

4. CHECK ANALYSES—Analyses may be made by the purchaser from finished material representing each melt, in which case an excess of 25 per cent above the requirements specified in Section 2 shall be allowed.

Specifications for Steel for Buildings

Continued

III. PHYSICAL PROPERTIES AND TESTS

5. TENSION TESTS—(a) The material shall conform to the following requirements as to tensile properties:

Properties Considered	Structural Steel	Rivet Steel
Tensile strength, lbs. per sq. in....	55,000-65,000	46,000-56,000
Yield point, min., lbs. per sq. in....	0.5 tens. str.	0.5 tens. str.
Elongation in 8 in., min., per cent...	<u>1,400,000^a</u>	<u>1,400,000</u>
	Tens. str.	Tens. str.
Elongation in 2 in., min., per cent...	22

^a See Section 6

(b) The yield point shall be determined by the drop of the beam of the testing machine.

6. MODIFICATIONS IN ELONGATION—(a) For structural steel over $\frac{3}{4}$ inch in thickness, a deduction of 1 from the percentage of elongation in 8 inches specified in Section 5(a) shall be made for each increase of $\frac{1}{8}$ inch in thickness above $\frac{3}{4}$ inch, to a minimum of 18 per cent.

(b) For structural steel under $\frac{5}{16}$ inch in thickness, a deduction of 2.5 from the percentage of elongation in 8 inches specified in Section 5 (a) shall be made for each decrease of $\frac{1}{16}$ inch in thickness below $\frac{5}{16}$ inch.

7. BEND TESTS—(a) The test specimen for plates, shapes and bars, except as specified in Paragraphs (b) and (c), shall bend cold through 180 degrees without cracking on the outside of the bent portion, as follows: For material $\frac{3}{4}$ inch or under in thickness, flat on itself; for material over $\frac{3}{4}$ inch to and including $1\frac{1}{4}$ inches in thickness, around a pin the diameter of which is equal to the thickness of the specimen; and for material over $1\frac{1}{4}$ inches in thickness, around a pin the diameter of which is equal to twice the thickness of the specimen.

(b) The test specimen for pins, rollers and other bars, when prepared as specified in Section 8 (e), shall bend cold through 180 degrees around a 1-inch pin without cracking on the outside of the bent portion.

Specifications for Steel for Buildings

Continued

(c) The test specimen for rivet steel shall bend cold through 180 degrees flat on itself without cracking on the outside of the bent portion.

8. TEST SPECIMENS—(a) Tension and bend test specimens shall be taken from rolled steel in the condition in which it comes from the rolls, except as specified in Paragraph (b).

(b) Tension and bend test specimens for pins and rollers shall be taken from the finished bars, after annealing when annealing is specified.

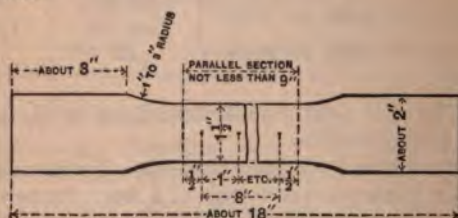


FIG. 1

(c) Tension and bend test specimens for plates, shapes and bars, except as specified in Paragraphs (d), (e) and (f), shall be of the full thickness of material as rolled; and may be machined to the form and dimensions shown in Fig. 1, or with both edges parallel.

(d) Tension and bend test specimens for plates over 1 inch in thickness or diameter may be machined to a thickness or diameter of at least $\frac{3}{4}$ inch for a length of at least 9 inches.

(e) Tension test specimens for pins, rollers and bars over $1\frac{1}{2}$ inches in thickness or diameter may be of the form and dimensions shown in Fig. 2. Bend test specimens may be 1 by $\frac{1}{2}$ inch in section. The axis of the specimens shall be located at a point midway between the center and surface and shall be parallel to the axis of the bar.

(f) Tension and bend test specimens for rivet steel shall be of the full-size section of bars as rolled.

9. NUMBER OF TESTS—(a) One tension and one bend test shall be made from each melt; except that if material from one melt

Specifications for Steel for Buildings

Continued

differs $\frac{3}{8}$ inch or more in thickness, one tension and one bend test shall be made from both the thickest and the thinnest material rolled.

(b) If any test specimen shows defective machining or develops flaws, it may be discarded and another specimen substituted.

(c) If the percentage of elongation of any tension test specimen is less than that specified in Section 5 (a) and any part of the fracture is more than $\frac{3}{4}$ inch from the center of the gauge length of a 2-inch specimen or is outside the middle third of the gauge

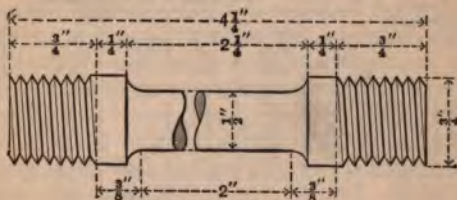


FIG. 2

length of an 8-inch specimen, as indicated by scribe scratches marked on the specimen before testing, a retest shall be allowed.

IV. PERMISSIBLE VARIATIONS IN WEIGHT AND GAUGE

10. PERMISSIBLE VARIATIONS—The cross-section or weight of each piece of steel shall not vary more than 2.5 per cent. from that specified; except in the case of sheared plates, which shall be covered by the following permissible variations to apply to single plates:

(a) *When Ordered to Weight*—For plates $12\frac{1}{2}$ pounds per square foot or over:

Under 100 inches in width, 2.5 per cent. above or below the specified weight;

100 inches in width or over, 5 per cent. above or below the specified weight.

For plates under $12\frac{1}{2}$ pounds per square foot:

Under 75 inches in width, 2.5 per cent. above or below the specified weight;
75 to 100 inches, exclusive, in width, 5 per cent. above or 3 per cent. below the specified weight;

100 inches in width or over, 10 per cent. above or 3 per cent. below the specified weight.

Specifications for Steel for Buildings

Continued

(b) *When Ordered to Gauge*—The thickness of each plate shall not vary more than 0.01 inch under that ordered.

An excess over the nominal weight corresponding to the dimensions on the order shall be allowed for each plate, if not more than that shown in the following table, one cubic inch of rolled steel being assumed to weigh 0.2833 pound.

Thickness Ordered, Inches	Nominal Weight, Pounds per Square Foot	ALLOWABLE EXCESS (EXPRESSED AS PERCENTAGE OF NOMINAL WEIGHT) For Width of Plate as follows:						
		Under 50 in.	50 to 70 in., excl.	70 in. or over.	Under 75 in.	75 to 100 in., excl.	100 to 115 in., excl.	115 in. or over.
$\frac{1}{8}$ to $\frac{5}{32}$	5.10 to 6.37	10	15	20				
$\frac{5}{32}$ to $\frac{3}{16}$	6.37 to 7.65	8.5	12.5	17				
$\frac{3}{16}$ to $\frac{1}{4}$	7.65 to 10.20	7	10	15				
$\frac{1}{4}$	10.20				10	14	18	
$\frac{5}{16}$	12.75				8	12	16	
$\frac{3}{8}$	15.30				7	10	13	17
$\frac{7}{16}$	17.85				6	8	10	13
$\frac{1}{2}$	20.40				5	7	9	12
$\frac{9}{16}$	22.95				4.5	6.5	8.5	11
$\frac{5}{8}$	25.50				4	6	8	10
Over $\frac{5}{8}$					3.5	5	6.5	9

V. FINISH

11. The finished material shall be free from injurious defects and shall have a workmanlike finish.

VI. MARKING

12. The name or brand of the manufacturer and the melt number shall be legibly stamped or rolled on all finished material, except that rivet and lattice bars and other small sections shall, when loaded for shipment, be properly separated and marked for identification. The identification marks shall be legibly stamped on the end of each pin and roller. The melt number shall be legibly marked, by stamping if practicable, on each test specimen.

Specifications for Steel for Buildings

Continued

VII. INSPECTION AND REJECTION

13. **INSPECTION**—The inspector representing the purchaser shall have free entry, at all times while work on the contract of the purchaser is being performed, to all parts of the manufacturer's works which concern the manufacture of the material ordered. The manufacturer shall afford the inspector, free of cost, all reasonable facilities to satisfy him that the material is being furnished in accordance with these specifications. All tests (except check analyses) and inspection shall be made at the place of manufacture prior to shipment, unless otherwise specified, and shall be so conducted as not to interfere unnecessarily with the operation of the works.

14. **REJECTION**—(a) Unless otherwise specified, any rejection based on tests made in accordance with Section 4 shall be reported within five working days from the receipt of samples.

(b) Material which shows injurious defects subsequent to its acceptance at the manufacturer's works will be rejected, and the manufacturer shall be notified.

15. **REHEARING**—Samples tested in accordance with Section 4, which represent rejected material, shall be preserved for two weeks from the date of the test report. In case of dissatisfaction with the results of the tests, the manufacturer may make claim for a rehearing within that time.

AMERICAN SOCIETY FOR TESTING MATERIALS
PHILADELPHIA, PA., U. S. A.

AFFILIATED WITH THE
INTERNATIONAL ASSOCIATION FOR TESTING MATERIALS

Standard Specifications for
Structural Steel for Bridges
Serial Designation: A7-15

Adopted, 1901; Revised, 1905, 1909, 1913, 1914, 1915

1. STEEL CASTINGS—The Standard Specifications for Steel Castings adopted by the American Society for Testing Materials shall govern the purchase of steel castings for bridges. Unless otherwise specified, Class B castings, medium grade, shall be used.

I. MANUFACTURE

2. PROCESS—The steel shall be made by the open-hearth process.

II. CHEMICAL PROPERTIES AND TESTS

3. CHEMICAL COMPOSITION—The steel shall conform to the following requirements as to chemical composition:

	STRUCTURAL STEEL	RIVET STEEL
Phosphorus	Acid.....not over 0.06	not over 0.04 per cent.
	Basic.....not over 0.04	not over 0.04 per cent.
Sulphur.....	not over 0.05	not over 0.045 per cent.

4. LADLE ANALYSES—An analysis to determine the percentages of carbon, manganese, phosphorus and sulphur shall be made by the manufacturer from a test ingot taken during the pouring of each melt, a copy of which shall be given to the purchaser or his representative. This analysis shall conform to the requirements specified in Section 3.

5. CHECK ANALYSES—Analyses may be made by the purchaser from finished material representing each melt, in which case an excess of 25 per cent. above the requirements specified in Section 3 be allowed.

Specifications for Steel for Bridges

Continued

III. PHYSICAL PROPERTIES AND TESTS

6. TENSION TESTS—(a) The material shall conform to the following requirements as to tensile properties:

Properties Considered	Structural Steel	Rivet Steel
Tensile strength, lbs. per sq. in.	55,000-65,000 ^a	46,000-56,000
Yield point, min., lbs. per sq. in.	0.5 tens. str.	0.5 tens. str.
Elongation in 8 in., min., per cent. ...	1,500,000 ^b Tens. str.	1,500,000 Tens. str.
Elongation in 2 in., min., per cent. ...	22

^a See Paragraph (b).

^b See Section 7.

(b) In order to meet the required minimum tensile strength of full-size annealed eye bars, the purchaser may determine the tensile strength to be obtained in specimen tests; the range shall not exceed 14,000 pounds per square inch, and the maximum shall not exceed 74,000 pounds per square inch. The material shall conform to the requirements as to physical properties other than that of tensile strength, specified in Sections 6, 7 and 8 (b).

(c) The yield point shall be determined by the drop of the beam of the testing machine.

7. MODIFICATIONS IN ELONGATION—(a) For structural steel over $\frac{3}{4}$ inch in thickness, a deduction of 1 from the percentage of elongation in 8 inches specified in Section 6 (a) shall be made for each increase of $\frac{1}{8}$ inch in thickness above $\frac{3}{4}$ inch, to a minimum of 18 per cent.

(b) For structural steel under $\frac{5}{16}$ inch in thickness, a deduction of 2.5 from the percentage of elongation in 8 inches specified in Section 6 (a) shall be made for each decrease of $\frac{1}{16}$ inch in thickness below $\frac{5}{16}$ inch.

8. BEND TESTS—(a) The test specimen for plates, shapes and bars, except as specified in paragraphs (b), (c) and (d), shall bend cold through 180 degrees without cracking on the outside of the bent portion, as follows: For material $\frac{3}{4}$ inch or under in thickness, flat on itself; for material over $\frac{3}{4}$ inch to and

Specifications for Steel for Bridges

Continued

including $1\frac{1}{4}$ inches in thickness, around a pin the diameter of which is equal to the thickness of the specimen; and for material over $1\frac{1}{4}$ inches in thickness, around a pin the diameter of which is equal to twice the thickness of the specimen.

(b) The test specimen for eye-bar flats shall bend cold through 180 degrees without cracking on the outside of the bent portion as follows: For material $\frac{3}{4}$ inch or under in thickness, around a pin the diameter of which is equal to the thickness of the

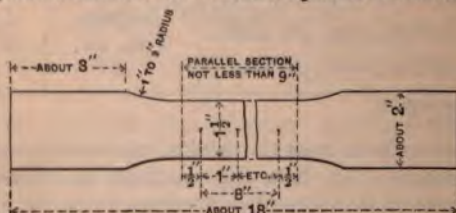


FIG. 1

specimen; for material over $\frac{3}{4}$ inch to and including $1\frac{1}{4}$ inches in thickness, around a pin the diameter of which is equal to twice the thickness of the specimen; and for material over $1\frac{1}{4}$ inches in thickness, around a pin the diameter of which is equal to three times the thickness of the specimen.

(c) The test specimen for pins, rollers and other bars, when prepared as specified in Section 9 (e), shall bend cold through 180 degrees around a 1-inch pin without cracking on the outside of the bent portion.

(d) The test specimen for rivet steel shall bend cold through 180 degrees flat on itself without cracking on the outside of the bent portion.

9. TEST SPECIMENS—(a) Tension and bend test specimens shall be taken from rolled steel in the condition in which it comes from the rolls, except as specified in Paragraph (b).

(b) Tension and bend test specimens for pins and rollers shall be taken from the finished bars, after annealing when annealing is specified.

(c) Tension and bend test specimens for plates, shapes and bars except as specified in Paragraphs (d), (e) and (f), shall be of

Specifications for Steel for Bridges

Continued

the full thickness of material as rolled. They may be machined to the form and dimensions shown in Fig. 1, or with both edges parallel; except that bend test specimens for eye-bar flats may have three rolled sides.

(d) Tension and bend test specimens for plates, and tension test specimens for eye-bar flats, over $1\frac{1}{2}$ inches in thickness may be machined to a thickness or diameter of at least $\frac{3}{4}$ inch for a length of at least 9 inches.

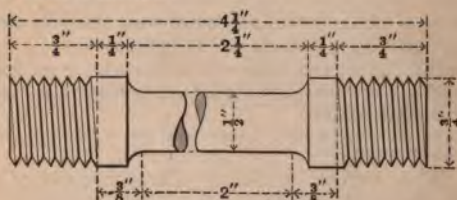


FIG. 2

(e) Tension test specimens for pins, rollers and bars (except eye-bar flats) over $1\frac{1}{2}$ inches in thickness or diameter may be of the form and dimensions shown in Fig. 2. Bend test specimens may be 1 by $\frac{1}{2}$ inch in section. The axis of the specimen shall be located at any point midway between the center and surface and shall be parallel to the axis of the bar.

(f) Tension and bend test specimens for rivet steel shall be of the full-size section of bars as rolled.

10. NUMBER OF TESTS—(a) One tension and one bend test shall be made from each melt; except that if material from one melt differs $\frac{3}{8}$ inch or more in thickness, one tension and one bend test shall be made from both the thickest and the thinnest material rolled.

(b) If any test specimen shows defective machining or develops flaws, it may be discarded and another specimen substituted.

(c) If the percentage of elongation of any tension test specimen is less than that specified in Section 6 (a) and any part of the fracture is more than $\frac{3}{4}$ inch from the center of the gauge length of a 2-inch specimen or is outside the middle third of the gauge length of an 8-inch specimen, as indicated by scribe scratches marked on the specimen before testing, a retest shall be allowed.

Specifications for Steel for Bridges

Continued

IV. PERMISSIBLE VARIATIONS IN WEIGHT AND GAUGE

11. PERMISSIBLE VARIATIONS—The cross-section or weight of each piece of steel shall not vary more than 2.5 per cent. from that specified; except in the case of sheared plates, which shall be covered by the following permissible variations to apply to single plates:

(a) *When Ordered to Weight*—For plates $12\frac{1}{2}$ pounds per square foot or over:

Under 100 inches in width, 2.5 per cent. above or below the specified weight;

100 inches in width or over, 5 per cent. above or below the specified weight.

For plates under $12\frac{1}{2}$ pounds per square foot:

Under 75 inches in width, 2.5 per cent. above or below the specified weight;

75 to 100 inches, exclusive, in width, 5 per cent. above or 3 per cent. below the specified weight;

100 inches in width or over, 10 per cent. above or 3 per cent. below the specified weight.

(b) *When Ordered to Gauge*—The thickness of each plate shall not vary more than 0.01 inch under that ordered.

An excess over the nominal weight corresponding to the dimensions on the order shall be allowed for each plate, if not more than that shown in the following table, one cubic inch of rolled steel being assumed to weigh 0.2833 pound.

Thickness Ordered, Inches	Nominal Weight, Pounds per Square Foot	ALLOWABLE EXCESS (EXPRESSED AS PERCENTAGE OF NOMINAL WEIGHT) For Width of Plate as follows:						
		Under 50 in.	50 to 70 in., excl.	70 in. or over.	Under 75 in.	75 to 100 in., excl.	100 to 115 in., excl.	115 in. or over.
$\frac{1}{8}$ to $\frac{5}{32}$	5.10 to 6.37	10	15	20
$\frac{3}{16}$ to $\frac{1}{4}$	6.37 to 7.65	8.5	12.5	17
$\frac{1}{4}$ to $\frac{5}{16}$	7.65 to 10.20	7	10	15
$\frac{5}{16}$	10.20	10	14	18
$\frac{3}{8}$	12.75	8	12	16
$\frac{7}{16}$	15.30	7	10	13	17
$\frac{1}{2}$	17.85	6	8	10	13
$\frac{5}{8}$	20.40	5	7	9	12
$\frac{3}{4}$	22.95	4.5	6.5	8.5	11
$\frac{7}{8}$	25.50	4	6	8	10
1	3.5	5	6.5	9

Specifications for Steel for Bridges

Continued

V. FINISH

12. FINISH—The finished material shall be free from injurious defects and shall have a workmanlike finish.

VI. MARKING

13. MARKING—The name or brand of the manufacturer and the melt number shall be legibly stamped or rolled on all finished material, except that rivet and lattice bars and other small sections shall, when loaded for shipment, be properly separated and marked for identification. The identification marks shall be legibly stamped on the end of each pin and roller. The melt number shall be legibly marked, by stamping if practicable, on each test specimen.

VII. INSPECTION AND REJECTION

14. INSPECTION—The inspector representing the purchaser shall have free entry, at all times while work on the contract of the purchaser is being performed, to all parts of the manufacturer's works which concern the manufacture of the material ordered. The manufacturer shall afford the inspector, free of cost, all reasonable facilities to satisfy him that the material is being furnished in accordance with these specifications. All tests (except check analyses) and inspection shall be made at the place of manufacture prior to shipment, unless otherwise specified, and shall be so conducted as not to interfere unnecessarily with the operation of the works.

15. REJECTION—(a) Unless otherwise specified, any rejection based on tests made in accordance with Section 5 shall be reported within five working days from the receipt of samples.

(b) Material which shows injurious defects subsequent to its acceptance at the manufacturer's works will be rejected, and the manufacturer shall be notified.

16. REHEARING—Samples tested in accordance with Section 5, which represent rejected material, shall be preserved for two weeks from the date of the test report. In case of dissatisfaction with the results of the tests, the manufacturer may make claim for a rehearing within that time.

AMERICAN SOCIETY FOR TESTING MATERIALS
PHILADELPHIA, PA., U. S. A.

AFFILIATED WITH THE
INTERNATIONAL ASSOCIATION FOR TESTING MATERIALS

Standard Specifications for
Steel Castings

Serial Designation: A27-14

Adopted, 1901; Revised, 1905, 1912, 1913, 1914

1. CLASSES—These specifications cover two classes of castings, namely:

Class A, ordinary castings for which no physical requirements are specified;

Class B, castings for which physical requirements are specified. These are of three grades: hard, medium and soft.

2. PATTERNS—(a) Patterns shall be made so that sufficient finish is allowed to provide for all variations in shrinkage.

(b) Patterns shall be painted three colors to represent metal, cores and finished surfaces. It is recommended that core prints shall be painted black and finished surfaces red.

3. BASIS OF PURCHASE—The purchaser shall indicate his intention to substitute the test to destruction specified in Section 11 for the tension and bend tests, and shall designate the patterns from which castings for this test shall be made.

I. MANUFACTURE

4. PROCESS—The steel may be made by the open-hearth, crucible, or any other process approved by the purchaser.

5. HEAT TREATMENT—(a) Class A castings need not be annealed unless so specified.

(b) Class B castings shall be allowed to become cold. They shall then be uniformly reheated to the proper temperature to refine the grain (a group thus reheated being known as an "annealing

Specifications for Steel Castings

Continued

charge"), and allowed to cool uniformly and slowly. If, in the opinion of the purchaser or his representative, a casting is not properly annealed, he may at his option require the casting to be re-annealed.

II. CHEMICAL PROPERTIES AND TESTS

6. CHEMICAL COMPOSITION—The castings shall conform to the following requirements as to chemical composition:

	CLASS A	CLASS B
Carbon.....	not over 0.30 per cent.
Phosphorus.....	not over 0.06 per cent.	not over 0.05 per cent.
Sulphur.....	not over 0.05 per cent.

7. LADLE ANALYSES—An analysis to determine the percentages of carbon, manganese, phosphorus and sulphur shall be made by the manufacturer from a test ingot taken during the pouring of each melt, a copy of which shall be given to the purchaser or his representative. This analysis shall conform to the requirements specified in Section 6. Drillings for analysis shall be taken not less than $\frac{1}{4}$ inch beneath the surface of the test ingot.

8. CHECK ANALYSES—(a) Analyses of Class A castings may be made by the purchaser, in which case an excess of 20 per cent. above the requirement as to phosphorus specified in Section 6 shall be allowed. Drillings for analysis shall be taken not less than $\frac{1}{4}$ inch beneath the surface.

(b) Analyses of Class B castings may be made by the purchaser from a broken tension or bend test specimen, in which case an excess of 20 per cent. above the requirements as to phosphorus and sulphur specified in Section 6 shall be allowed. Drillings for analysis shall be taken not less than $\frac{1}{4}$ inch beneath the surface.

III. PHYSICAL PROPERTIES AND TESTS

(FOR CLASS B CASTINGS ONLY)

9. TENSION TESTS—(a) The castings shall conform to the following minimum requirements as to tensile properties:

Specifications for Steel Castings

Continued

	HARD	MEDIUM	SOFT
Tensile strength, lbs. per sq. in.....	80,000	70,000	60,000
Yield point, lbs. per sq. in.	36,000	31,500	27,000
Elongation in 2 in., per cent.....	15	18	22
Reduction of area, per cent.....	20	25	30

(b) The yield point shall be determined by the drop of the beam of the testing machine.

10. BEND TESTS—(a) The test specimen for soft castings shall bend cold through 120 degrees, and for medium castings through 90 degrees, around a 1-inch pin, without cracking on the outside of the bent portion.

(b) Hard castings shall not be subject to bend test requirements.

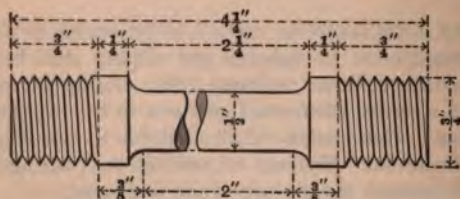


FIG. 2

11. ALTERNATIVE TESTS TO DESTRUCTION—In the case of small or unimportant castings, a test to destruction on three castings from a lot may be substituted for the tension and bend tests. This test shall show the material to be ductile, free from injurious defects, and suitable for the purpose intended. A lot shall consist of all castings from one melt, in the same annealing charge.

12. TEST SPECIMENS—(a) Sufficient test bars, from which the test specimens required in Section 13 (a) may be selected, shall be attached to castings weighing 500 pounds or over, when the design of the castings will permit. If the castings weigh less than 500 pounds, or are of such a design that test bars cannot be attached, two test bars shall be cast to represent each melt; or the quality of the castings shall be determined by tests to destruction as specified in Section 11. All test bars shall be annealed with the castings they represent.

Specifications for Steel Castings

Continued

(b) The manufacturer and purchaser shall agree whether test bars can be attached to castings, on the location of the bars on the castings, on the castings to which bars are to be attached, and on the method of casting unattached bars.

(c) Tension test specimens shall be of the form and dimensions shown in Fig. 1. Bend test specimens shall be machined to 1 by $\frac{1}{2}$ inch in section with corners rounded to a radius not over $\frac{1}{16}$ inch.

13. NUMBER OF TESTS—(a) One tension and one bend test shall be made from each annealing charge. If more than one melt is represented in an annealing charge, one tension and one bend test shall be made from each melt.

(b) If any test specimen shows defective machining or develops flaws, it may be discarded; in which case the manufacturer and the purchaser or his representative shall agree upon the selection of another specimen in its stead.

(c) If the percentage of elongation of any tension test specimen is less than that specified in Section 9 (a) and any part of the fracture is more than $\frac{3}{4}$ inch from the center of the gauge length, as indicated by scribe scratches marked on the specimen before testing, a retest shall be allowed.

IV. WORKMANSHIP AND FINISH

14. WORKMANSHIP—The castings shall substantially conform to the sizes and shapes of the patterns, and shall be made in a workmanlike manner.

15. FINISH—(a) The castings shall be free from injurious defects.

(b) Minor defects which do not impair the strength of the castings may, with the approval of the purchaser or his representative, be welded by an approved process. The defects shall first be cleaned out to solid metal; and after welding, the castings shall be annealed, if specified by the purchaser or his representative.

(c) The castings offered for inspection shall not be painted or covered with any substance that will hide defects, nor rusted to such an extent as to hide defects.

Specifications for Steel Castings

Continued

V. INSPECTION AND REJECTION

16. **INSPECTION**—The inspector representing the purchaser shall have free entry, at all times while work on the contract of the purchaser is being performed, to all parts of the manufacturer's works which concern the manufacture of the castings ordered. The manufacturer shall afford the inspector, free of cost, all reasonable facilities to satisfy him that the castings are being furnished in accordance with these specifications. All tests (except check analyses) and inspection shall be made at the place of manufacture prior to shipment, unless otherwise specified, and shall be so conducted as not to interfere unnecessarily with the operation of the works.

17. **REJECTION**—(a) Unless otherwise specified, any rejection based on tests made in accordance with Section 8 shall be reported within five working days from the receipt of samples.

(b) Castings which show injurious defects subsequent to their acceptance at the manufacturer's works will be rejected, and the manufacturer shall be notified.

18. **REHEARING**—Samples tested in accordance with Section 8, which represent rejected castings, shall be preserved for two weeks from the date of the test report. In case of dissatisfaction with the results of the tests, the manufacturer may make claim for a rehearing within that time.

VI. SPECIAL REQUIREMENTS FOR CASTINGS FOR SHIPS

19. **CASTINGS FOR SHIPS**—In addition to the preceding requirements, castings for ships, when so specified, shall conform to the following requirements:

20. **HEAT TREATMENT**—All castings shall be annealed.

21. **NUMBER OF TESTS**—(a) One tension and one bend test shall be made from each of the following castings: stern frames, stern posts, twin screw spectacle frames, propeller shaft brackets, rudders, steering quadrants, tillers, stems, anchors, and other castings when specified.

(b) When a casting is made from more than one melt, four tension and four bend tests shall be made from each casting.

Specifications for Steel Castings

Continued

22. **PERCUSSION TESTS**—(a) A percussion test shall be made on each of the following castings: stern frames, stern posts, twin screw spectacle frames, propellor shaft brackets, rudders, steering quadrants, tillers, stems, anchors, and other castings when specified.

(b) For this test, the casting shall be suspended by chain and hammered all over with a hammer of a weight approved by the purchaser or his representative. If cracks, flaws, defects, or weakness appear after such treatment, the casting will be rejected.

VII. SPECIAL REQUIREMENTS FOR CASTINGS FOR RAILWAY ROLLING STOCK

23. **CASTINGS FOR RAILWAY ROLLING STOCK**—Castings for railway rolling stock, when so specified, shall conform to the requirements for Class B castings, Sections 1 to 18, inclusive, except that check analyses made in accordance with Section 8 (b) shall conform to the requirements as to phosphorus and sulphur specified in Section 6.

AMERICAN SOCIETY FOR TESTING MATERIALS
PHILADELPHIA, PA., U. S. A.

AFFILIATED WITH THE
INTERNATIONAL ASSOCIATION FOR TESTING MATERIALS

Standard Specifications for
Boiler and Firebox Steel

Serial Designation: A30-14

Adopted, 1901; Revised, 1909, 1912, 1913, 1914

1. GRADES—These specifications cover two grades of steel for boilers, namely: Flange and Firebox.

I. MANUFACTURE

2. PROCESS—The steel shall be made by the open-hearth process.

II. CHEMICAL PROPERTIES AND TESTS

3. CHEMICAL COMPOSITION—The steel shall conform to the following requirements as to chemical composition:

	FLANGE	FIREBOX
Carbon.....		0.12 — 0.25 per cent.
Manganese.....	0.30 — 0.60	0.30 — 0.50 per cent.
Phosphorus (Acid.....)	not over 0.05	not over 0.04 per cent.
Basic.....	not over 0.04	not over 0.035 per cent.
Sulphur.....	not over 0.05	not over 0.04 per cent.
Copper.....		not over 0.05 per cent.

4. LADLE ANALYSES—An analysis shall be made by the manufacturer from a test ingot taken during the pouring of each melt, a copy of which shall be given to the purchaser or his representative. This analysis shall conform to the requirements specified in Section 3.

5. CHECK ANALYSES—Analyses may be made by the purchaser from a broken tension test specimen representing each plate as 1, which shall conform to the requirements specified in Section 3.

Specifications for Boiler and Firebox Steel

Continued

III. PHYSICAL PROPERTIES AND TESTS

6. TENSION TESTS—(a) The material shall conform to the following requirements as to tensile properties:

	FLANGE	FIREBOX
Tensile strength, lbs. per sq. in.....	55,000 — 65,000	52,000 — 62,000
Yield point, min., lbs. per sq. in.....	0.5 tens. str.	0.5 tens. str.
Elongation in 8 in., min., per cent.....	1,500,000	1,500,000
(See Section 7)	Tens. str.	Tens. str.

(b) The yield point shall be determined by the drop of the beam of the testing machine.

7. MODIFICATIONS IN ELONGATION—(a) For material over $\frac{3}{4}$ inch in thickness, a deduction of 0.5 from the percentages of elongation specified in Section 6 (a) shall be made for each increase of $\frac{1}{8}$ inch in thickness above $\frac{3}{4}$ inch.

(b) For material $\frac{1}{4}$ inch or under in thickness, the elongation shall be measured on a gauge length of 24 times the thickness of the specimen.

8. BEND TESTS—(a) *Cold-bend Tests*—The test specimen shall bend cold through 180 degrees without cracking on the outside of the bent portion, as follows: For material 1 inch or under in thickness, flat on itself; and for material over 1 inch in thickness, around a pin the diameter of which is equal to the thickness of the specimen.

(b) *Quench-bend Tests*—The test specimen, when heated to a light cherry red as seen in the dark (not less than 1200 degrees Fahrenheit), and quenched at once in water the temperature of which is between 80 degrees and 90 degrees Fahrenheit, shall bend through 180 degrees without cracking on the outside of the bent portion, as follows: For material 1 inch or under in thickness, flat on itself; and for material over 1 inch in thickness, around a pin the diameter of which is equal to the thickness of the specimen.

9. HOMOGENEITY TESTS—For firebox steel, a sample taken from a broken tension test specimen shall not show any single seam or cavity more than $\frac{1}{4}$ inch long, in either of the three fractures obtained in the test for homogeneity, which shall be made as follows:

The specimen shall be either nicked with a chisel or grooved on a machine, transversely, about $\frac{1}{16}$ inch deep, in three places 2 inches apart. The first groove shall be made 2 inch

Specifications for Boiler and Firebox Steel

Continued

square end; each succeeding groove shall be made on the opposite side from the preceding one. The specimen shall then be firmly held in a vise, with the first groove about $\frac{3}{4}$ inch above the jaws, and the projecting end broken off by light blows of a hammer, the bending being away from the groove. The specimen shall be broken at the other two grooves in the same manner. The object of this test is to open and render visible to the eye any seams due to failure to weld up or to interposed foreign matter, or any cavities

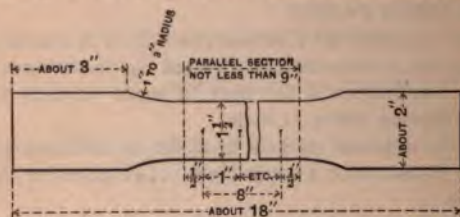


FIG. 1

due to gas bubbles in the ingot. One side of each fracture shall be examined and the lengths of the seams and cavities determined, a pocket lens being used if necessary.

10. TEST SPECIMENS—Tension and bend test specimens shall be taken from the finished rolled material. They shall be of the full thickness of material as rolled, and shall be machined to the form and dimensions shown in Fig. 1; except that bend test specimens may be machined with both edges parallel.

11. NUMBER OF TESTS—(a) One tension, one cold-bend, and one quench-bend test shall be made from each plate as rolled.

(b) If any test specimen shows defective machining or develops flaws, it may be discarded and another specimen substituted.

(c) If the percentage of elongation of any tension test specimen is less than that specified in Section 6 (a) and any part of the fracture is outside the middle third of the gauge length, as indicated by scribe scratches marked on the specimen before testing, test shall be allowed.

Specifications for Boiler and Firebox Steel

Continued

IV. PERMISSIBLE VARIATIONS IN WEIGHT AND GAUGE

12. PERMISSIBLE VARIATIONS—*When Ordered to Gauge*—The thickness of each plate shall not vary more than 0.01 inch under that ordered.

An excess over the nominal weight corresponding to the dimensions on the order shall be allowed for each plate, if not more than that shown in the following table, one cubic inch of rolled steel being assumed to weigh 0.2833 pound:

Thickness Ordered, Inches	Nominal Weight, Pounds per Square Foot	ALLOWABLE EXCESS (EXPRESSED AS PERCENTAGE OF NOMINAL WEIGHT) For Width of Plate as follows:						
		Under 50 in.	50 to 70 in., excl.	70 in. or over.	Under 75 in.	75 to 100 in., excl.	100 to 115 in., excl.	115 in. or over.
$\frac{1}{8}$ to $\frac{5}{32}$	5.10 to 6.37	10	15	20
$\frac{5}{32}$ to $\frac{3}{16}$	6.37 to 7.65	8.5	12.5	17
$\frac{3}{16}$ to $\frac{1}{4}$	7.65 to 10.20	7	10	15
$\frac{1}{4}$	10.20	10	14	18
$\frac{5}{16}$	12.75	8	12	16
$\frac{3}{8}$	15.30	7	10	13	17
$\frac{7}{16}$	17.85	6	8	10	13
$\frac{1}{2}$	20.40	5	7	9	12
$\frac{9}{16}$	22.95	4.5	6.5	8.5	11
$\frac{5}{8}$	25.50	4	6	8	10
Over $\frac{5}{8}$	3.5	5	6.5	9

V. FINISH

13. FINISH—The finished material shall be free from injurious defects and shall have a workmanlike finish.

VI. MARKING

14. MARKING—The name or brand of the manufacturer, melt or slab number, grade, and lowest tensile strength for its grade specified in Section 6 (a), shall be legibly stamped on each melt or slab number shall be legibly stamped on each

Specifications for Boiler and Firebox Steel

Continued

VII. INSPECTION AND REJECTION

15. INSPECTION—The inspector representing the purchaser shall have free entry at all times while work on the contract of the purchaser is being performed, to all parts of the manufacturer's works which concern the manufacture of the material ordered. The manufacturer shall afford the inspector, free of cost, all reasonable facilities to satisfy him that the material is being furnished in accordance with these specifications. All tests (except check analyses) and inspection shall be made at the place of manufacture prior to shipment, unless otherwise specified, and shall be so conducted as not to interfere unnecessarily with the operation of the works.

16. REJECTION—(a) Unless otherwise specified, any rejection based on tests made in accordance with Section 5 shall be reported within five working days from the receipt of samples.

(b) Material which shows injurious defects subsequent to its acceptance at the manufacturer's works will be rejected, and the manufacturer shall be notified.

17. REHEARING—Samples tested in accordance with Section 5, which represent rejected material, shall be preserved for two weeks from the date of the test report. In case of dissatisfaction with the results of the tests, the manufacturer may make claim for a rehearing within that time.

AMERICAN SOCIETY FOR TESTING MATERIALS
PHILADELPHIA, PA., U. S. A.

AFFILIATED WITH THE
INTERNATIONAL ASSOCIATION FOR TESTING MATERIALS

Standard Specifications for
Structural Steel for Ships

Serial Description: A12-14

Adopted, 1901; Revised, 1909, 1913, 1914

I. MANUFACTURE

1. PROCESS—The steel shall be made by the open-hearth process.

II. CHEMICAL PROPERTIES AND TESTS

2. CHEMICAL COMPOSITION—The steel shall conform to the following requirements as to chemical composition:

Phosphorus	Acid.....	not over 0.06 per cent.
	Basic.....	not over 0.04 per cent.
Sulphur.....		not over 0.05 per cent.

3. LADLE ANALYSES—An analysis to determine the percentages of carbon, manganese, phosphorus and sulphur shall be made by the manufacturer from a test ingot taken during the pouring of each melt, a copy of which shall be given to the purchaser or his representative. This analysis shall conform to the requirements specified in Section 2.

4. CHECK ANALYSES—Analyses may be made by the purchaser from finished material representing each melt, in which case an excess of 25 per cent. above the requirements specified in Section 2 shall be allowed.

III. PHYSICAL PROPERTIES AND TESTS

5. TENSION TESTS—(a) The material shall conform to the following requirements as to tensile properties:

NOTE—The requirements for castings for ships have been especially provided for in the Standard Specifications for Steel Castings, adopted by the Society for Testing Materials attached thereto.

Specifications for Structural Steel for Ships

Continued

Tensile strength, lbs. per sq. in.	58,000 — 68,000
Yield point, min., lbs. per sq. in.	0.5 tens. str.
Elongation in 8 in., min., per cent.	1,500,000
(See Section 6.)	Tens. str.

(b) The yield point shall be determined by the drop of the beam of the testing machine.



FIG. 1

6. MODIFICATIONS IN ELONGATION—(a) For material over $\frac{3}{4}$ inch in thickness, a deduction of 1 from the percentage of elongation specified in Section 5 (a) shall be made for each increase of $\frac{1}{8}$ inch in thickness above $\frac{3}{4}$ inch, to a minimum of 18 per cent.

(b) For material $\frac{1}{4}$ inch or under in thickness, the elongation shall be measured on a gauge length of 24 times the thickness of the specimen.

7. BEND TESTS—The test specimen shall bend cold through 180 degrees without cracking on the outside of the bent portion, as follows: For material $\frac{3}{4}$ inch or under in thickness, around a pin the diameter of which is equal to the thickness of the specimen; for material over $\frac{3}{4}$ inch to and including $1\frac{1}{4}$ inches in thickness, around a pin the diameter of which is equal to $1\frac{1}{2}$ times the thickness of the specimen; and for material over $1\frac{1}{4}$ inches in thickness, around a pin the diameter of which is equal to twice the thickness of the specimen.

8. TEST SPECIMENS—(a) Tension and bend test specimens shall be taken from the finished rolled material, and shall not be annealed or otherwise treated, except as specified in Paragraph (b).

(b) Tension and bend test specimens for material which is to be annealed or otherwise treated before use, shall be cut from properly annealed or similarly treated short lengths of the full length of the piece.

Specifications for Structural Steel for Ships

Continued

(c) Tension and bend test specimens, except as specified in Paragraph (d), shall be of the full thickness of material as rolled; and may be machined to the form and dimensions shown in Fig. 1, or with both edges parallel.

(d) Tension and bend test specimens for plates and bars over $1\frac{1}{2}$ inches in thickness or diameter may be machined to a thickness or diameter of at least $\frac{3}{4}$ inch for a length of at least 9 inches.

9. NUMBER OF TESTS—(a) One tension and one bend test shall be made from each melt; except that if material from one melt differs $\frac{3}{8}$ inch or more in thickness, one tension and one bend test shall be made from both the thickest and the thinnest material rolled.

(b) If any test specimen shows defective machining or develops flaws, it may be discarded and another specimen substituted.

(c) If the percentage of elongation of any tension test specimen is less than that specified in Section 5 (a) and any part of the fracture is outside the middle third of the gauge length, as indicated by scribe scratches marked on the specimen before testing, a retest shall be allowed.

IV. PERMISSIBLE VARIATIONS IN WEIGHT AND GAUGE

10. PERMISSIBLE VARIATIONS—The cross-section or weight of each piece of steel shall not vary more than 2.5 per cent. from that specified; except in the case of sheared plates, which shall be covered by the following permissible variations to apply to single plates:

(a) *When Ordered to Weight*—For plates $12\frac{1}{2}$ pounds per square foot or over:

Under 100 inches in width, 2.5 per cent. above or below the specified weight;

100 inches in width or over, 5 per cent. above or below the specified weight.

Specifications for Structural Steel for Ships

Continued

For plates under 12½ pounds per square foot:

Under 75 inches in width, 2.5 per cent. above or below the specified weight;
75 to 100 inches, exclusive, in width, 5 per cent. above or 3 per cent. below
the specified weight;

100 inches in width or over, 10 per cent. above or 3 per cent. below the
specified weight.

(b) *When Ordered to Gauge*—The thickness of each plate shall not vary more than 0.01 inch under that ordered.

An excess over the nominal weight corresponding to the dimensions on the order shall be allowed for each plate, if not more than shown in the following table, one cubic inch of rolled steel being assumed to weigh 0.2833 pound.

Thickness Ordered, Inches	Nominal Weight, Pounds per Square Foot	ALLOWABLE EXCESS (EXPRESSED AS PERCENTAGE OF NOMINAL WEIGHT) For Width of Plate as follows:						
		Under 50 in.	50 to 70 in., excl.	70 in. or over.	Under 75 in.	75 to 100 in., excl.	100 to 115 in., excl.	115 in. or over.
1/8 to 5/32	5.10 to 6.37	10	15	20
5/32 to 3/16	6.37 to 7.65	8.5	12.5	17
3/16 to 1/4	7.65 to 10.20	7	10	15
1/4	10.20	10	14	18
5/16	12.75	8	12	16
3/8	15.30	7	10	13	17
7/16	17.85	6	8	10	13
1/2	20.40	5	7	9	12
5/8	22.95	4.5	6.5	8.5	11
3/4	25.50	4	6	8	10
Over 3/4	3.5	5	6.5	9

V. FINISH

11. *FINISH*—The finished material shall be free from injurious defects and shall have a workmanlike finish.

VI. MARKING

12. *MARKING*—The name or brand of the manufacturer and the melt number shall be legibly rolled or stamped on all finished material. The melt number shall be legibly stamped on each test
imen.

Specifications for Structural Steel for Ships

Continued

VII. INSPECTION AND REJECTION

13. **INSPECTION**—The inspector representing the purchaser shall have free entry, at all times while work on the contract of the purchaser is being performed, to all parts of the manufacturer's works which concern the manufacture of the material ordered. The manufacturer shall afford the inspector, free of cost, all reasonable facilities to satisfy him that the material is being furnished in accordance with these specifications. All tests (except check analyses) and inspection shall be made at the place of manufacture prior to shipment, unless otherwise specified, and shall be so conducted as not to interfere unnecessarily with the operation of the works.

14. **REJECTION**—(a) Unless otherwise specified, any rejection based on tests made in accordance with Section 4 shall be reported within five working days from the receipt of samples.

(b) Material which shows injurious defects subsequent to its acceptance at the manufacturer's works will be rejected, and the manufacturer shall be notified.

15. **REHEARING**—Samples tested in accordance with Section 4, which represent rejected material, shall be preserved for two weeks from the date of the test report. In case of dissatisfaction with the results of the tests, the manufacturer may make claim for a rehearing within that time.

Standard Specifications for Fabricated Steel Building Construction

Adopted 1915

DESIGN

LOADING:

1st—All steel used for building construction shall be so designed as to safely resist all stresses coming from both dead and live loads. The dead load shall consist of the weight of the structure itself, together with all permanent fixtures and attachments, such as walls, roofs, floors, partitions, elevators, vaults and other permanent fixtures. The live load shall consist of the super-imposed loads on floors and roofs, also the exterior loads due to wind pressure, etc.

2nd—Where moving loads are to be provided for, such as cranes or car traffic of any kind, 25% shall be added to the stresses due to such moving loads to care for the impact and vibrations accompanying such loading.

3rd—Unless local conditions indicate other values as being probable, a wind pressure of twenty pounds per square foot on the vertical projection of all structures shall be provided for.

4th—All parts of the structure shall be of such sizes that the dead load or live load or the sum of the dead and live loads, plus impact allowances, if necessary, shall not exceed the following amounts in pounds per square inch:

Tension, net section rolled steel.....	16,000
Direct compression rolled steel.....	16,000
Direct compression, steel castings.....	16,000
Direct compression, iron castings.....	12,000
Stresses in extreme fibers of rolled steel shapes, built sections, girders and steel castings when subject to flexure.....	16,000
Bending in extreme fibers of steel pins and steel slabs under columns.....	24,000
Shear on steel shop rivets and pins.....	12,000
Shear on turned bolts and field rivets.....	10,000
Shear on rough bolts.....	8,000
Shear in webs of steel plate girders and rolled beams.....	10,000
Bearing on steel shop rivets and pins.....	24,000
Bearing on turned bolts and field rivets.....	20,000
Bearing on rough bolts.....	16,000
Compression along longitudinal axis of rolled steel columns, per square inch, $16,000 \times 70 \frac{L}{R}$, with a maximum of 14,000 pounds.....	
Compression along longitudinal axis of cast iron columns per square inch.....	8,000
	$\frac{1 \times L^2}{800d}$

Standard Specifications for Fabricated Steel Building Construction

Continued

In the foregoing formula L equals length of member in inches between points of support; R equals radius of gyration; D equals outside diameter.

The maximum length of any rolled steel section used in compression shall not exceed 150 times the least radius of gyration.

Where expansion rollers are used to provide for the expansion and contraction of a structure, due to changes in temperature, the maximum pressure per linear inch on such rollers shall not exceed 600 times the diameter of the rollers in inches.

For wind bracing, also for members subject to combined stresses due to wind and either dead or live loads or both, the permissible stresses per square inch, as mentioned above, may be increased 25%, provided that the section as determined under this paragraph be not less than that required for dead and live loads alone.

ECCENTRIC LOADING:

In determining sizes for compression members, full consideration shall be given the stresses due to eccentric loading. In determining areas for tension members, net sections only shall be considered, and, in deduction of rivet holes, the hole shall be assumed to be $\frac{1}{8}$ inch greater in diameter than the nominal diameter of the rivets. Such members of the structure as are subject to both direct loading and transverse loading shall be so proportioned that the maximum fiber stress in the member shall not exceed the limits given above.

In members subject to both tension and compression, the greater stress shall be increased by 50% of the lesser, and the member shall then be designed for the stress requiring the larger section.

Connections for such members subject to such reversal of stress shall be proportioned for the sum of the two stresses.

Rolled beams and channels, also built up members used as girders or beams, shall be proportioned by the moment of inertia of their net section.

Webs of plate girders shall have a thickness of not less than $\frac{1}{16}$ of 1% of the unsupported distance of such webs between

Standard Specifications for
Fabricated Steel Building Construction

Continued

flange angles. Webs shall also be provided with stiffeners in pairs over bearings and at points of concentrated loading. Also when web thickness is less than $1\frac{1}{10}\%$ of the unsupported distance between flange angles, stiffeners shall be provided spaced not farther apart than the depth of the web plate. This spacing, however shall not exceed a maximum limit of six feet.

Where beams and girders are without lateral support for a distance exceeding ten times the width of a compression flange, then the stress per square inch in said compression flange shall not be permitted to exceed $19,000 \text{ minus } 300 \frac{L}{B}$, in which L equals unsupported length of the compression flange and B equals width of the compression flange, and providing further that no beam or girder shall be used in which the unsupported length of a compression flange exceeds forty times the width of said flange.

MINIMUM SECTIONS:

Except where used for ornamental purposes, or for fillers, or for smoke stacks, no steel is to be used less than $\frac{1}{4}$ inch thick, nor shall any lateral rods, sag rods or similar ties or braces be used having a less section than $\frac{2}{10}$ of one square inch at the smallest point.

GENERAL:

As a rule all adjustable members in any part of a structure are to be avoided and all built sections shall preferably be made symmetrical. With the exception of lattice bars and the intersections of diagonal bracing, ceiling hangers, etc., no connection shall have less than two rivets. In the construction of trusses, preference is to be given to riveted connections and only under exceptional circumstances shall pin connections be used. All abutting joints and compression members are to be accurately machine finished, so as to secure as uniform a bearing with the abutting member as can be obtained by such means. Further, such joints shall have *splice plates* with sufficient rivets to hold connecting members *curately in place*. Where compression members are not properly

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machine finished, they shall be fully spliced. All tension members shall be fully spliced. Stiff bracing is also to be preferred for all wind bracing, sway bracing and lateral bracing. Adjustable rods for this purpose are not to be used without special sanction.

BEAM GIRDERS:

Where girders are composed of two or more rolled beams or rolled channels, they shall be connected at intervals of not more than five feet by bolts passing through their webs with cast iron or wrought steel separators or distance pieces to maintain them in their proper position. In lieu of such separators and separator bolts, it will be permissible to keep such beams or channels in position by using cover plates on either top flange or bottom flange, or both top and bottom flanges, or by the use of batten plates riveted to the flanges. Should such batten plates be used, they shall contain not less than two rivets in each plate for connection to each flange and shall be spaced at intervals not exceeding five feet. Where flange plates are used on girders, they shall be so limited in width as to not extend a greater distance beyond the outer line of rivets connecting them to the flanges or angles than 6 inches, or sixteen times the thickness of the thinnest flange plate used, unless special provision is made for holding the flanges in their nominal relation to the web of the girder.

STIFFENERS:

Web stiffeners on plate girders shall be used in pairs and shall fit closely against the flange angles. Stiffeners that are used over end bearings, or under points of concentrated load, or for forming connections between columns and girders, shall have a tight bearing against the flange angles. Where web plates of girders are not furnished in one piece, they shall be spliced by a plate on each side of the web with sufficient rivets to properly transmit the maximum shear coming at point of splicing.

RIVETS:

The minimum distance center to center of rivets shall preferably be not less than three inches for $\frac{7}{8}$ inch diameter rivets.

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2½ inches for ¾ inch diameter rivets or two inches for ⅝ inch diameter rivets. In no case, however, shall it be less than three times the diameter of rivets used.

The maximum distance center to center of rivets in the line of stress, where built members composed of plates and shapes are used, shall be six inches or sixteen times the thinnest outside plate. For angles having two gauge lines with rivets staggered, the greatest pitch in each line shall be twice the above allowance.

Where two or more plates are in contact, they shall be held together with stitch rivets spaced not more than 12 inches apart, center to center in both directions.

The minimum distance from the center of any rivet hole to a sheared edge shall be 1½ inches for ⅝ inch diameter rivets, 1¼ inches for ¾ inch diameter rivets, 1⅛ inches for ⅝ inch diameter rivets, and the corresponding distance to a rolled edge shall be 1¼ inches, 1⅛ inches and 1 inch respectively.

The maximum distance from the center of any plate to the center of the nearest rivet shall not exceed eight times the thickness of the plate. For built members subject to compression, the pitch of the rivets at the ends of same shall not exceed four diameters of the rivets used for a length equal to 1½ times the width of said members.

LATTICING:

Where compression members are used that are composed of two or more pieces not connected by web plates or cover plates, they shall have their open sides connected by lattice bars, and be further provided with tie plates at each end, also at such intermediate points as it shall be necessary to interrupt the continuity of the lattice. Such end tie plates shall have a length not less than the distance between rows of rivets connecting them to the flanges of the member, and intermediate tie plates shall have a length of not less than one-half of this distance. The thickness of both end and intermediate tie plates shall not be less than two per cent. of this distance.

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Continued

All latticing used on compression members shall be of such sizes and shall have sufficient rivets to enable the latticing to resist a transverse shearing stress of not less than two per cent. of the total amount of the direct stress. Where a single system of latticing is used, the thickness of the lattice bars shall be not less than $2\frac{1}{2}\%$, or where a double system of latticing is used, not less than $1\frac{1}{10}\%$ of the distance between the end rivets connecting the lattice bars to the main members. Nor shall their width be less than $2\frac{1}{2}$ inches for sections composed of 15-inch channels, or for built sections using $3\frac{1}{2}$ -inch or 4-inch angles; $2\frac{1}{4}$ inches for sections composed of 12, 10 and 9-inch channels or for built sections using 3-inch angles; 2 inches for 8 and 7-inch channels or for built sections using $2\frac{1}{2}$ -inch angles; or $1\frac{3}{4}$ inches for sections composed of 6 and 5-inch channels, or for built sections using 2-inch angles.

Lattice bars in no case shall be used with an inclination to the axis of the main member that is less than 45 degrees where double latticing is used, or 60 degrees where single latticing is used, and double latticing shall be used in all cases where the distance between rivet lines and the flanges of the main member is more than 15 inches. Care shall also be taken that the ratio of length to the radius of gyration of parts of the member that are connected by lattice bars is less than the ratio of total length of the member to the radius of gyration of the member as a whole.

PINS:

All pin holes shall be reinforced by pin plates wherever such reinforcement is necessary to keep the pressure of the pins on the surface of the pin hole within the limits of this specification. Where such pin plates are used, at least one plate shall be as wide as the projecting flanges will allow, and such pin plate shall contain sufficient rivets to properly distribute their proportion of pin pressure to the full cross section of the main member. All pins shall be long enough to insure a full bearing on all parts connecting with the turned body of the pin, and members connecting on the pin shall be properly held against lateral movement.

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All beams, channels and girders that derive their support from walls or piers shall be properly anchored to same, and shall further be provided with wall plates of such thickness and such area as to properly distribute the load coming from said beams, channels or girders on the wall or piers.

Where beams, channels, girders and other members act as skew-backs for floor arches, such beams, channels, girders and other members shall be duly designed to resist the lateral thrust coming from such arches, in addition to all other loads that they may be called upon to sustain.

Tie rods shall be placed as near to the spring of the arches as is practicable and shall be of such size as to enable them to properly resist the stresses coming upon them.

WORKMANSHIP

SHEARING:

The workmanship shall be equal to the best practice in fully equipped structural shops. All shearing must be done accurately and all portions of the work present a neat and workmanlike finish.

PUNCHING:

The diameter of the punch shall not be more than $\frac{1}{16}$ inch larger than the nominal diameter of the rivet, nor shall the diameter of the die be more than $\frac{1}{8}$ inch larger than the nominal diameter of the rivet. All punching must be done accurately. An occasional slight inaccuracy in the matching of holes may be corrected by reaming. Drifting for such purposes will not be allowed under any circumstances.

RIVETING:

Pressure tools shall be used wherever possible for the driving of rivets, and pneumatic hammers shall be used where the use of such pressure tools is not possible. Hand riveting will be allowed only under exceptional circumstances. All rivet heads shall be *flush* on the shank and shall be neat, full and of equal size and *grip* the assembled pieces closely.

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Fabricated Steel Building Construction**

Continued

ASSEMBLING:

All riveted members shall be well pinned up and firmly bolted together before riveting is begun. All surfaces coming in contact shall be painted before assembling. All the abutting joints shall be accurately cut so as to make a snug fit, and when finished all riveted pieces shall be free from twists, bends and open joints. Where steel has been partially heated in the fabrication the entire piece shall be annealed when finished. All steel castings shall also be annealed before using. Welds in steel will not be allowed under any circumstances.

PAINTING:

Except where members are to be embedded in concrete all steel shall be thoroughly cleaned with wire brushes and be given one thorough coat of an approved paint, well worked into all joints and seams before leaving the fabricating shop. No castings of any kind, however, shall be painted until after inspection and acceptance by the inspector.

EYE BARS:

Where eye bars are used they shall be straight and true to size, free from twists, folds or seams in neck or head. Heads shall be made by upsetting or forging as welded heads will not be allowed. Pin holes shall be on the center line of the bar and in the center of the heads. The boring of pin holes shall be done with such accuracy that when bars of same length are placed together a pin $\frac{1}{8}$ inch smaller in diameter than the pin holes can be passed through the holes at both ends of the bars at the same time.

PINS:

Pins and rollers shall be accurately turned to gauge and are to be straight, smooth and free from flaws. Pin holes shall be bored true to gauge, smooth and straight and at right angles to the axis of the member through which they pass. Such boring to be done after the member is riveted up.

INSPECTION:

Full facilities shall be furnished by the manufacturer for inspecting and testing the quality of the material, the workmanship and the weights, including the use of a suitable testing machine. Inspector shall also have free access to all parts of the works where material embraced in this contract is being manufactured.

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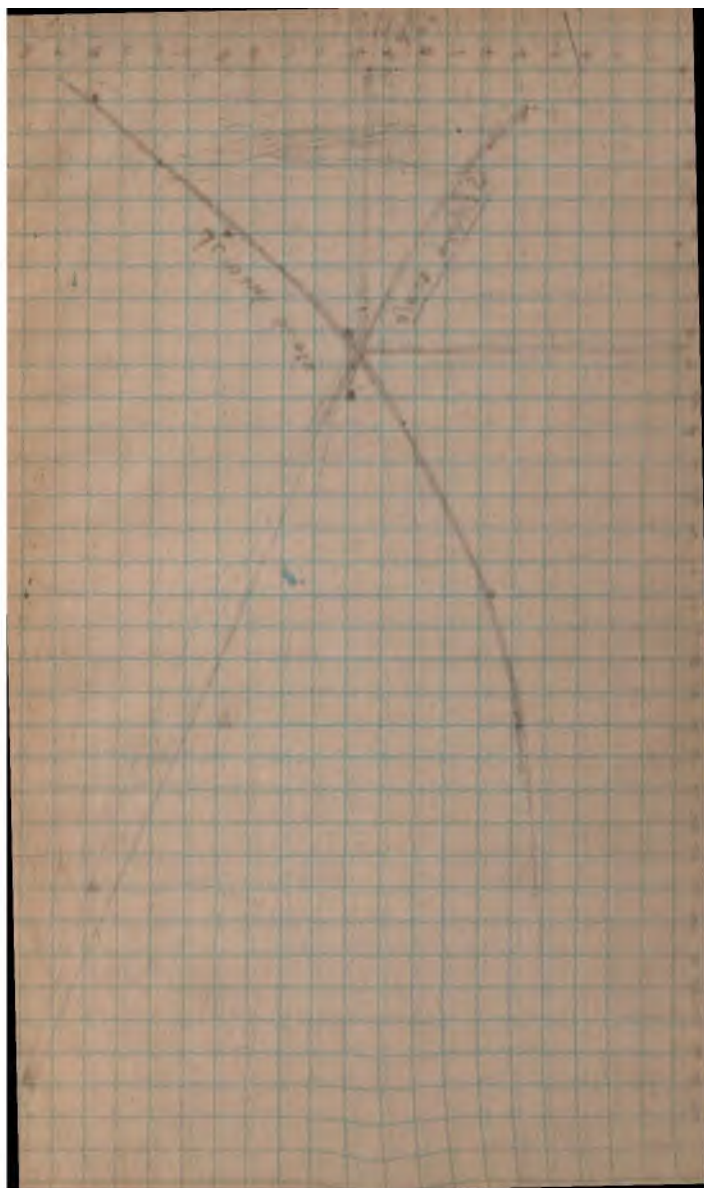
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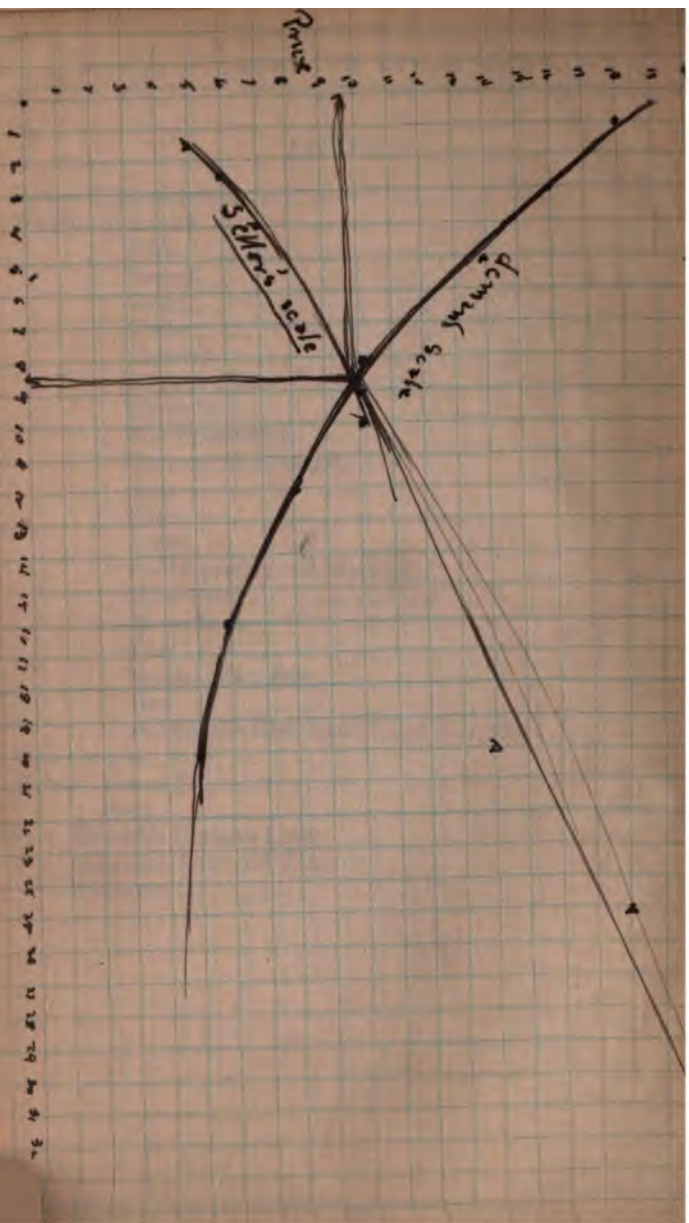
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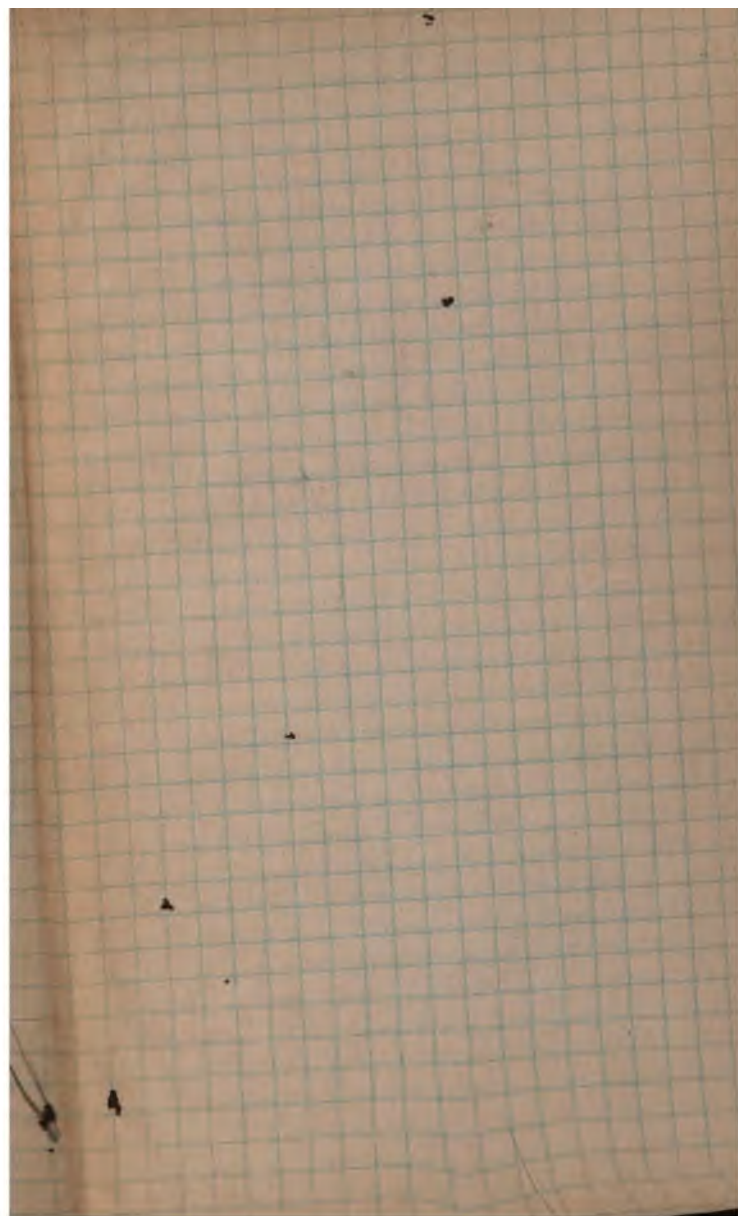
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Temp of coal

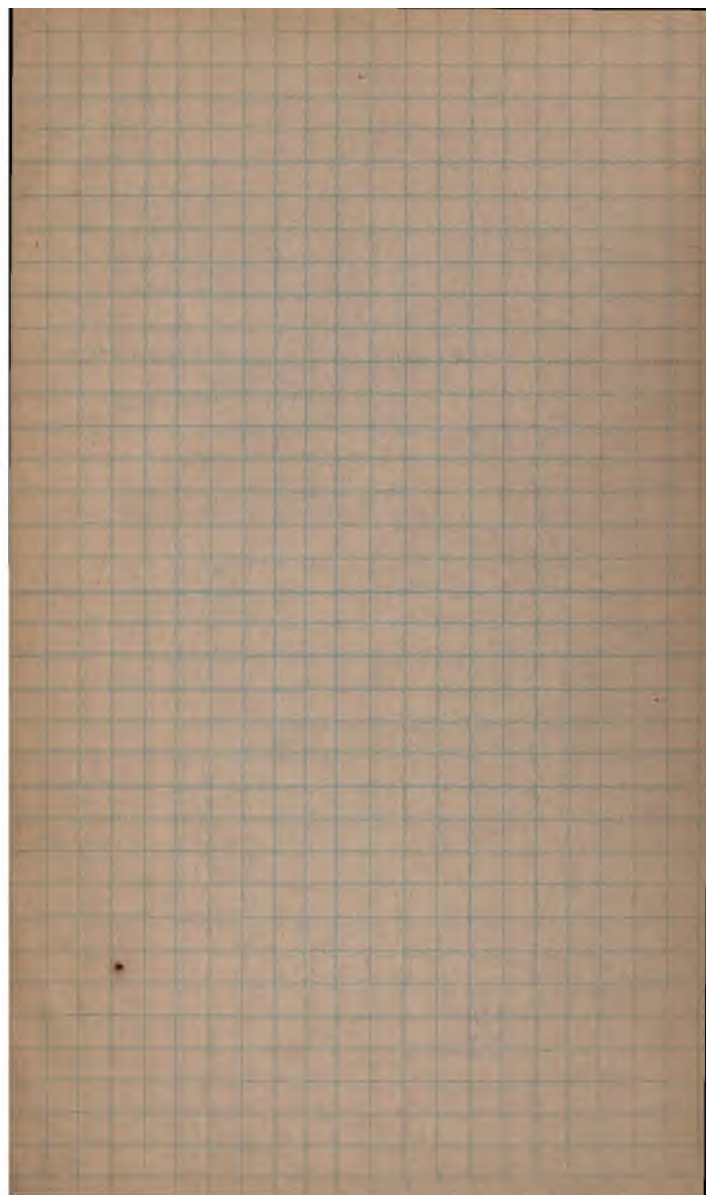


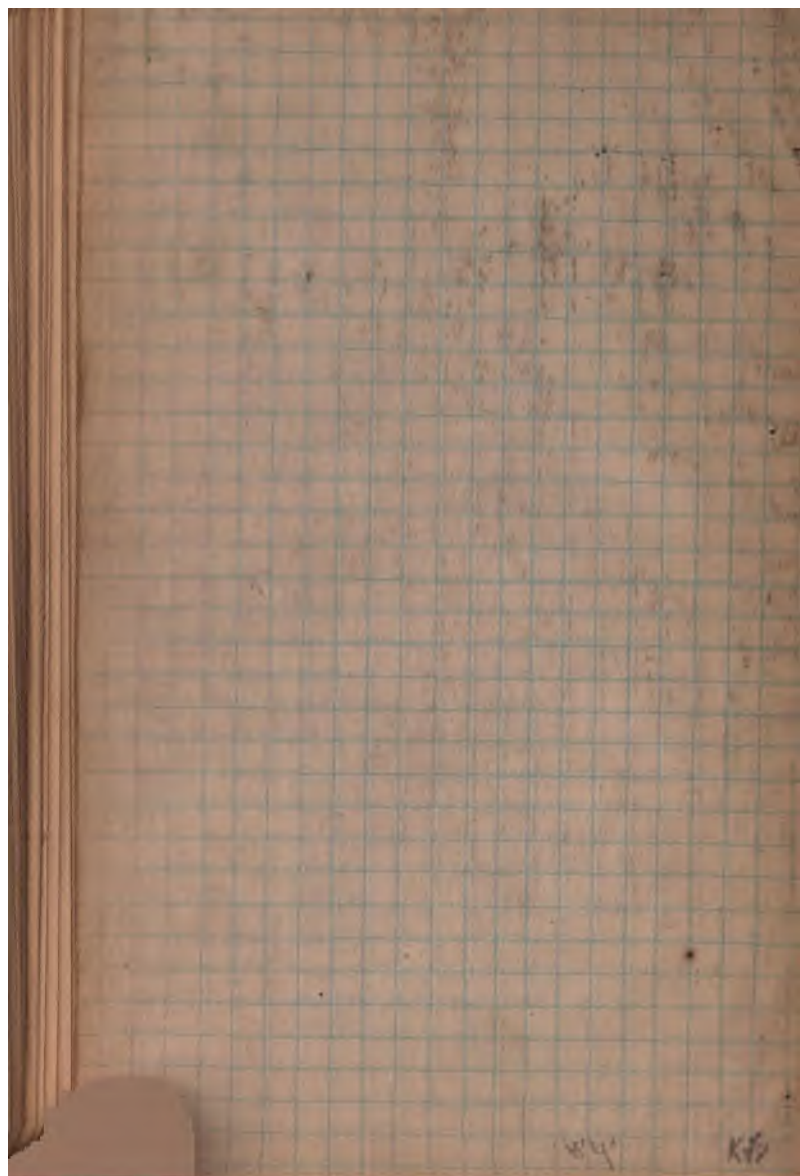


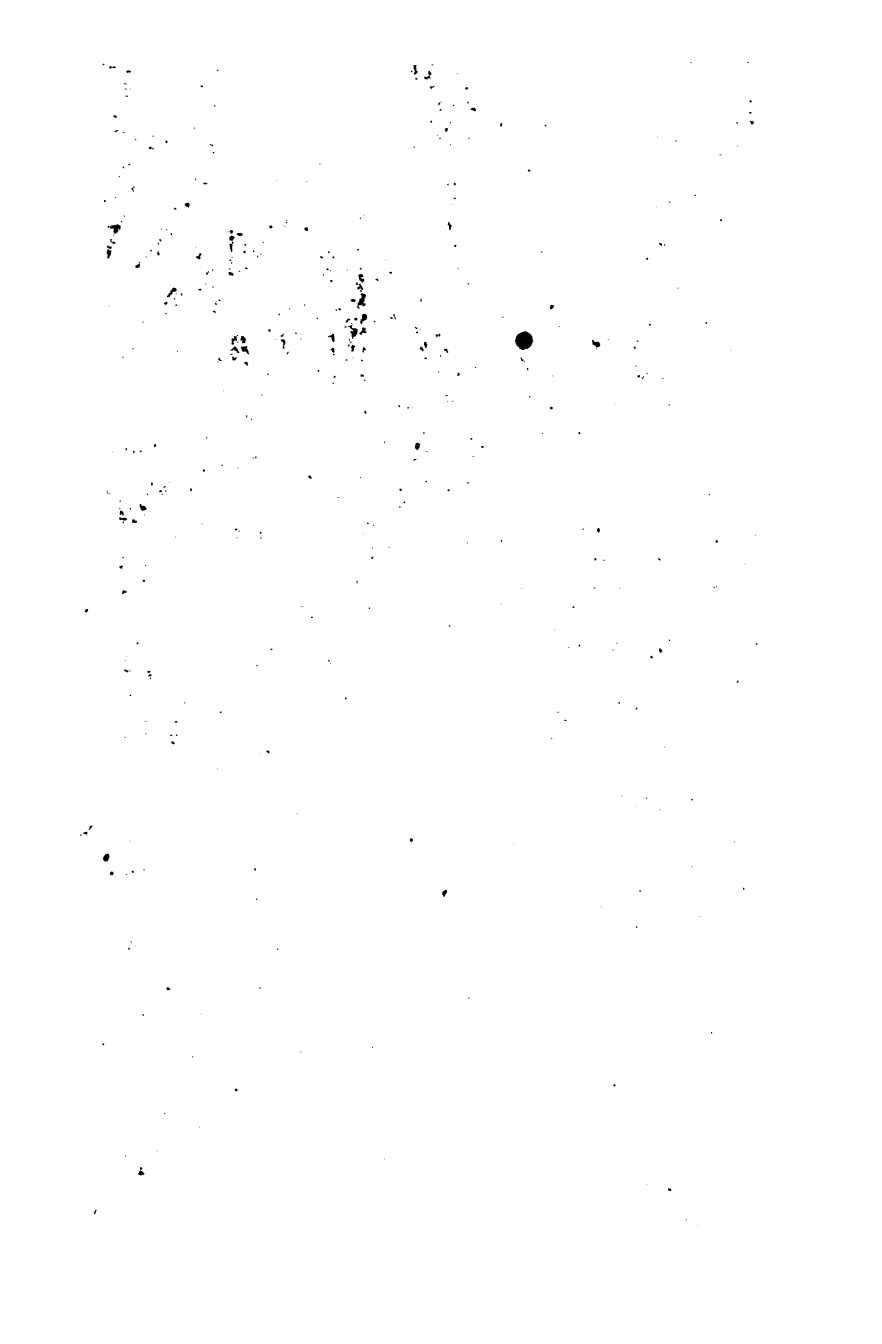












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